

Appendix for “EquiGraspFlow: SE(3)-Equivariant 6-DoF Grasp Pose Generative Flows”

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10 A Proof of SE(3)-Invariant Conditional Distributions

11 In this section, we restate and prove Proposition 1 in section 4.1.

12 **Proposition 1.** *Suppose a prior distribution $p_0(T|\mathcal{P})$ is SE(3)-invariant. If the angular and linear*
13 *velocity fields ω, v are SE(3)-equivariant, then the conditional distribution $p_t(T|\mathcal{P})$ at any time*
14 *$t \geq 0$ defined via the flow of ODE $(\dot{R}, \dot{x}) = ([\omega_\theta(t, \mathcal{P}, T)]R, v_\phi(t, \mathcal{P}, T))$ is SE(3)-invariant.*

15 To this end, we first introduce the concept of a conditional flow derived from the velocity fields
16 and define the SE(3)-equivariance of the conditional flow. Subsequently, we demonstrate that
17 SE(3)-equivariant time-dependent conditional velocity fields induce an SE(3)-equivariant condi-
18 tional flow. Finally, we prove Proposition 1 by establishing that, starting from an SE(3)-invariant
19 prior, an SE(3)-equivariant conditional flow preserves the invariance over time.

20 A.1 SE(3)-Equivariant Conditional Flows

21 Consider a trajectory on the SE(3) manifold, starting from an initial point $T \in \text{SE}(3)$ and guided by
22 the time-dependent angular and linear velocity fields, ω and v , conditioned on a point cloud \mathcal{P} . This
23 trajectory is called an *integral curve* for ω and v conditioned on \mathcal{P} and starting at T , and is denoted by
24 $\gamma : \mathbb{R} \rightarrow \text{SE}(3)$. By decomposing the SO(3) and \mathbb{R}^3 components such that $\gamma(t) = (\gamma_R(t), \gamma_x(t))$,
25 the integral curve is defined via the following ordinary differential equations (ODEs) of the velocity
26 fields:

$$\dot{\gamma}_R(t) = [\omega(t, \mathcal{P}, \gamma(t))] \gamma_R(t), \quad \dot{\gamma}_x(t) = v(t, \mathcal{P}, \gamma(t)), \quad \gamma(0) = T. \quad (1)$$

27 Denoting the space of point clouds by \mathcal{X} , a *conditional flow* of the velocity fields ω and v conditioned
28 on \mathcal{P} is defined as a mapping $f : \mathbb{R} \times \mathcal{X} \times \text{SE}(3) \rightarrow \text{SE}(3)$. Here, $f(t, \mathcal{P}, T) = \gamma(t)$ where γ is the
29 integral curve for ω and v conditioned on \mathcal{P} and starting at T .

30 Now, we define the SE(3)-equivariance of a conditional flow as follows:

31 **Definition 3.** A flow on SE(3) conditioned on a point cloud, denoted by $f(t, \mathcal{P}, T)$, is SE(3)-
 32 equivariant if, for an arbitrary $T' \in \text{SE}(3)$, $f(t, T'\mathcal{P}, T'T) = T'f(t, \mathcal{P}, T)$.

33 Next, We demonstrate that SE(3)-equivariant time-dependent conditional velocity fields induce the
 34 SE(3)-equivariance of their conditional flow through the following Proposition:

35 **Proposition 2.** For any time-dependent conditional angular and linear velocity fields ω and v , their
 36 conditional flow f is SE(3)-equivariant if ω and v are SE(3)-equivariant.

37 *Proof.* Consider an arbitrary point cloud \mathcal{P} and fix $T = (R_0, x_0)$ as an arbitrary element in SE(3).
 38 Then, $f(t, \mathcal{P}, T) = \gamma(t) = (\gamma_R(t), \gamma_x(t))$ represents the integral curve for the velocity fields con-
 39 ditioned on \mathcal{P} and starting at T . The ODEs governing this integral curve are given by the same
 40 equations as (1).

41 For any $T' = (R', x') \in \text{SE}(3)$, $f(t, T'\mathcal{P}, T'T) = \tilde{\gamma}(t) = (\tilde{\gamma}_R(t), \tilde{\gamma}_x(t))$ where $\tilde{\gamma}$ is the integral
 42 curve for the velocity fields conditioned on $T'\mathcal{P}$ and starting at $T'T$. The ODEs for this integral
 43 curve are given by:

$$\dot{\tilde{\gamma}}_R(t) = [\omega(t, T'\mathcal{P}, \tilde{\gamma}(t))] \tilde{\gamma}_R(t), \quad \dot{\tilde{\gamma}}_x(t) = v(t, T'\mathcal{P}, \tilde{\gamma}(t)), \quad \tilde{\gamma}(0) = T'T. \quad (2)$$

44 Now, consider an integral curve $\hat{\gamma}$ defined as $\hat{\gamma}(t) = (\hat{\gamma}_R(t), \hat{\gamma}_x(t)) := (R'\gamma_R(t), R'\gamma_x(t) + x') =$
 45 $T'(\gamma_R(t), \gamma_x(t)) = T'\gamma(t) = T'f(t, \mathcal{P}, T)$. This integral curve results from transforming the inte-
 46 gral curve $(\gamma_R(t), \gamma_x(t))$ by T' .

47 To prove the SE(3)-equivariance of the conditional flow, we need to show that $\tilde{\gamma}$ and $\hat{\gamma}$ are the same
 48 integral curve. Specifically, we need to show that $\tilde{\gamma}(t) = f(t, T'\mathcal{P}, T'T) = T'f(t, \mathcal{P}, T) = \hat{\gamma}(t)$.

49 Noting that $R[a]R^T = [Ra]$ for any $R \in \text{SO}(3)$ and $a \in \mathbb{R}^3$, we analyze $\dot{\hat{\gamma}}_R(t)$ as follows:

$$\begin{aligned} \dot{\hat{\gamma}}_R(t) &= \frac{d}{dt}(R'\gamma_R(t)) = R'\dot{\gamma}_R(t) \\ &= R'[\omega(t, \mathcal{P}, \gamma(t))] \gamma_R(t) \\ &= [R'\omega(t, \mathcal{P}, \gamma(t))] R'\gamma_R(t) \\ &= [\omega(t, T'\mathcal{P}, T'\gamma(t))] R'\gamma_R(t) \\ &= [\omega(t, T'\mathcal{P}, \hat{\gamma}(t))] \hat{\gamma}_R(t). \end{aligned} \quad (3)$$

50 Similarly, for $\hat{\gamma}_x(t)$, we have:

$$\begin{aligned} \dot{\hat{\gamma}}_x(t) &= \frac{d}{dt}(R'\gamma_x(t) + x') \\ &= R'\dot{\gamma}_x(t) \\ &= R'v(t, \mathcal{P}, \gamma(t)) \\ &= v(t, T'\mathcal{P}, T'\gamma(t)) \\ &= v(t, T'\mathcal{P}, \hat{\gamma}(t)). \end{aligned} \quad (4)$$

51 Finally, note that $\hat{\gamma}(0) = T'\gamma(0) = T'T$. Thus, $\tilde{\gamma}(t)$ and $\hat{\gamma}(t)$ satisfy the same ODEs, and the
 52 uniqueness of the solution of the ODE ensures that $\tilde{\gamma}$ and $\hat{\gamma}$ are the same integral curve. Con-
 53 sequently, we have $f(t, T'\mathcal{P}, T'T) = T'f(t, \mathcal{P}, T)$ for any $T' \in \text{SE}(3)$, demonstrating that f is
 54 SE(3)-equivariant. \square

55 A.2 SE(3)-Invariant Conditional Distributions

56 To demonstrate that an SE(3)-equivariant conditional flow preserves the invariance of an SE(3)-
 57 invariant prior, we present the following proposition.

58 **Proposition 3.** Suppose a prior distribution $p_0(T|\mathcal{P})$ is SE(3)-invariant. If the conditional flow f
 59 is SE(3)-equivariant, then the conditional distribution $p_t(T|\mathcal{P})$ at any time $t \geq 0$ defined via the
 60 flow is SE(3)-invariant.

61 *Proof.* To prove this proposition, we first extend Theorem 3 from [1], which involves a general
 62 Riemannian manifold and a general group, to a conditional version.

63 Consider a Riemannian manifold (\mathcal{M}, h) with a group G . Denote the action of an element $g \in G$
 64 on \mathcal{M} by the map $L_g : \mathcal{M} \rightarrow \mathcal{M}$. The map L_g is isometric if, for any tangent vectors u and v
 65 at any point $x \in \mathcal{M}$, the following condition holds: $h(d(L_g)_x(u), d(L_g)_x(v)) = h(u, v)$, where
 66 $d(L_g)_x$ represents the differential of L_g at x . If L_g is isometric, then $|\det J_{L_g}(x)| = 1$ for any
 67 $x \in \mathcal{M}$, where $J_{L_g}(x)$ denotes the Jacobian matrix of the map L_g evaluated at x and expressed in
 68 local coordinates.

69 Let c denote a condition variable. The conditional flow at time t is represented by the map
 70 $f_{t,c} : \mathcal{M} \rightarrow \mathcal{M}$. This flow transforms a prior conditional distribution $p_0(x|c)$ into the condi-
 71 tional distribution $p_t(x|c)$. The likelihood of the transformed conditional distribution is given by the
 72 following change of variables formula:

$$p_t(x|c) = p_0(f_{t,c}^{-1}(x)|c) \left| \det J_{f_{t,c}^{-1}}(x) \right|. \quad (5)$$

73 A conditional distribution $p(x|c)$ is G -invariant if $p(L_g(x)|g \cdot c) = p(x|c)$ for any $g \in G$. Assuming
 74 the action of $g \in G$ on c is well-defined and denoted by $g \cdot c$, the conditional flow $f_{t,c}$ is G -equivariant
 75 if, $f_{t,g \cdot c}(L_g(x)) = L_g(f_{t,c}(x))$ for any $g \in G$, i.e., $f_{t,g \cdot c} \circ L_g = L_g \circ f_{t,c}$ and $L_g^{-1} \circ f_{t,g \cdot c}^{-1} =$
 76 $f_{t,c}^{-1} \circ L_g^{-1}$.

77 Assuming that the map L_g is isometric for any $g \in G$, we can prove Proposition 3 in a general
 78 Riemannian manifold \mathcal{M} and a general group G as follows:

$$\begin{aligned} & p_t(L_g(x)|g \cdot c) \\ &= p_0(f_{t,g \cdot c}^{-1}(L_g(x))|g \cdot c) \left| \det J_{f_{t,g \cdot c}^{-1}}(L_g(x)) \right| \\ &= p_0(L_{g^{-1}}(f_{t,g \cdot c}^{-1}(L_g(x)))|c) \left| \det J_{f_{t,g \cdot c}^{-1}}(L_g(x)) \right| && \text{(invariant prior)} \\ &= p_0((L_{g^{-1}} \circ f_{t,g \cdot c}^{-1} \circ L_g)(x)|c) \\ &\quad \underbrace{\left| \det J_{L_{g^{-1}}}((f_{t,g \cdot c}^{-1} \circ L_g)(x)) \right|}_{=1} \left| \det J_{f_{t,g \cdot c}^{-1}}(L_g(x)) \right| \underbrace{\left| \det J_{L_g}(x) \right|}_{=1} \\ &= p_0((L_{g^{-1}} \circ f_{t,g \cdot c}^{-1} \circ L_g)(x)|c) && (6) \\ &\quad \left| \det J_{L_{g^{-1}}}((f_{t,g \cdot c}^{-1} \circ L_g)(x)) J_{f_{t,g \cdot c}^{-1}}(L_g(x)) J_{L_g}(x) \right| && \text{(multiplicativity)} \\ &= p_0((L_{g^{-1}} \circ f_{t,g \cdot c}^{-1} \circ L_g)(x)|c) \left| \det J_{L_{g^{-1}} \circ f_{t,g \cdot c}^{-1} \circ L_g}(x) \right| && \text{(chain rule)} \\ &= p_0((L_g^{-1} \circ f_{t,g \cdot c}^{-1} \circ L_g)(x)|c) \left| \det J_{L_g^{-1} \circ f_{t,g \cdot c}^{-1} \circ L_g}(x) \right| && (L_{g^{-1}} = L_g^{-1}) \\ &= p_0((f_{t,c}^{-1} \circ L_g^{-1} \circ L_g)(x)|c) \left| \det J_{f_{t,c}^{-1} \circ L_g^{-1} \circ L_g}(x) \right| \\ &= p_0(f_{t,c}^{-1}(x)|c) \left| \det J_{f_{t,c}^{-1}}(x) \right| \\ &= p_t(x|c). \end{aligned}$$

79 Proposition 3 is a special case where $\mathcal{M} = \text{SE}(3)$, $G = \text{SE}(3)$, and $c = \mathcal{P}$, and the group action of
 80 $T' \in \text{SE}(3)$ on $T \in \text{SE}(3)$, denote by $L_{T'}(T) = T'T$, is the left translation map which is isometric.
 81 Hence, Proposition 3 is proved. \square

82 We now prove Proposition 1 by utilizing Proposition 2 and Proposition 3.

83 *Proof of Proposition 1.* Since the angular and linear velocity fields ω_θ and v_ϕ are $\text{SE}(3)$ -equivariant,
 84 it follows from Proposition 2 that their flow f is also $\text{SE}(3)$ -equivariant. Consequently, by Propo-
 85 sition 3, the conditional distribution $p_t(T|\mathcal{P})$, which is defined via the flow of the velocity fields, is
 86 $\text{SE}(3)$ -invariant. \square

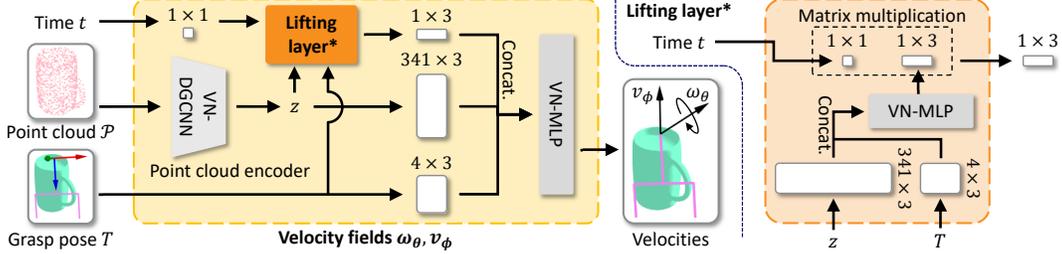


Figure 1: The structure of the velocity fields and lifting layer. The VN-DGCNN encodes the point cloud \mathcal{P} into a representation z consisting of 341 three-dimensional vectors. The VN-MLP in the lifting layer utilizes this representation along with the grasp pose T , to produce a matrix of size 1×3 . This matrix lifts the time variable t (of size 1×1) to a three-dimensional vector. Finally, the VN-MLP takes as input the concatenated list of the lifted time, representation, and grasp pose, and outputs the angular and linear velocities.

87 B Implementation Details

88 B.1 Details for Networks

89 To model the time-dependent conditional velocity fields $\omega_\theta(t, \mathcal{P}, T)$ and $v_\phi(t, \mathcal{P}, T)$ with SO(3)-
 90 equivariance, we employ Vector Neuron (VN) architectures [2], which are specifically designed for
 91 SO(3)-equivariance. The structure of these velocity fields is illustrated in Figure 1.

92 To encode the point cloud \mathcal{P} , we utilize the backbone of the VN-DGCNN designed for classification
 93 tasks. We use the network before the invariant layer, excluding the batch normalization layers. We
 94 add an EdgeConv module with a size of 170 at the sixth module position. Following the backbone,
 95 a mean pooling layer is applied to pool the point dimension, extracting a representation z
 96 of 341 three-dimensional vectors. The grasp pose T is reconfigured into a form that concatenates
 97 the three column vectors of the rotation part and one vector of the translation part, resulting in four
 98 three-dimensional vectors. Time t is converted into a single three-dimensional vector through the
 99 lifting layer. Subsequently, the VN-MLP concatenates these lists of three-dimensional vectors as
 100 input and outputs the angular and linear velocities. The VN-MLP consists of five hidden VN-Linear
 101 layers, each followed by VN-LeakyReLU activation with a negative slope 0.2, and one output VN-
 102 Linear layer. The sizes of the hidden layers are (256, 256, 128, 128, 128), and the output layer size
 103 is 2, as the network’s output is two three-dimensional vectors.

104 The lifting layer uses the representation z and the grasp pose T to convert the scalar time t into
 105 a three-dimensional vector. This process involves a VN-MLP that consists of a single VN-Linear
 106 layer with a size of 1, producing an output matrix of size 1×3 . This output matrix is then multiplied
 107 to the scalar t (size 1×1), resulting in a single three-dimensional vector.

108 B.2 Details for Training and Inference

109 **Dataset Split** We use a dataset of 101 mugs and 83 bowls obtained from the [ACRONYM dataset](#)
 110 [3] to train the networks. The dataset is split as follows: 61 mugs and 51 bowls are randomly selected
 111 for training, 20 mugs and 16 bowl for validation, and the remaining 20 mugs and 16 bowl for testing.

112 **Flow Matching** We employ the Flow Matching (FM) framework [4, 5] to train our continuous
 113 normalizing flow model. The core element of FM involves designing the *per-sample* target vector
 114 field $u_t^*(T|T_1)$ and the corresponding probability path $p_t(T|T_1)$, where $T_1 = (R_1, x_1)$ represents a
 115 particular sample from the target distribution $q(T|\mathcal{P})$. In our approach, we separate the rotation and
 116 translation components in $u_t^*(T|T_1) = (\omega_t^*(R|R_1), v_t^*(x|x_1))$. We then define the target angular
 117 and linear velocity fields $\omega_t^*(R|R_1)$ and $v_t^*(x|x_1)$ as follows:

$$[\omega_t^*(R|R_1)] = \frac{\log(R^T R_1)}{1-t}, \quad v_t^*(x|x_1) = \frac{x_1 - x}{1-t}. \quad (7)$$

118 Consequently, the training objective for EquiGraspFlow is designed as

$$\mathcal{L} = \mathbb{E}_{t, T_1 \sim q(T|\mathcal{P}), T \sim p_t(T|T_1)} \left[\frac{1}{2} \left\| \left[\omega_\theta(t, \mathcal{P}, T) \right] - \frac{\log(R^T R_1)}{1-t} \right\|_F^2 + \left\| v_\phi(t, \mathcal{P}, T) - \frac{x_1 - x}{1-t} \right\|^2 \right] \quad (8)$$

119 where $\|\cdot\|_F$ denotes the Frobenius norm, and $T = (R, x)$ and $T_1 = (R_1, x_1)$.

120 One thing to note is that it might seem natural to design the vector field on the SE(3) manifold
 121 instead of separating the rotation and translation components, similarly to how we design the angular
 122 velocity field on the SO(3) manifold as shown in (7). However, this approach results in screw
 123 motion-shaped paths of grasp poses, where the translation may not follow a straight line toward
 124 the target grasp pose. In the context of our grasp pose generation task, separating the rotation and
 125 translation and ensuring that the translation motion directly heads toward the target grasp pose is a
 126 more intuitive and appropriate vector field formulation.

127 **Guided Flows** Guided Flows [6] is a technique that enhances the sample quality and efficiency of
 128 conditional generative models by integrating classifier-free guidance [7] into Flow Matching mod-
 129 els. This method employs a guided velocity field during sampling, defined as a weighted sum of
 130 unconditional and conditional velocity fields. Using an empty set \emptyset as a null condition for the point
 131 cloud input, we define the guided angular and linear velocity fields $\tilde{\omega}_\theta$ and \tilde{v}_ϕ as follows, utilizing
 132 the weight parameter β :

$$\begin{aligned} \tilde{\omega}_\theta(t, \mathcal{P}, T) &= (1 - \beta)\omega_\theta(t, \emptyset, T) + \beta\omega_\theta(t, \mathcal{P}, T), \\ \tilde{v}_\phi(t, \mathcal{P}, T) &= (1 - \beta)v_\phi(t, \emptyset, T) + \beta v_\phi(t, \mathcal{P}, T). \end{aligned} \quad (9)$$

133 When \emptyset is input, the point cloud encoder outputs a list of zero vectors as z . To train the unconditional
 134 velocity fields, we randomly replace \mathcal{P} with the empty set \emptyset with a probability of 20% during
 135 training. For inference, we use $\beta = 1.25$ to evaluate average performance and $\beta = 2$ to assess the
 136 consistency of performance.

137 **Optimizer** Adam optimizer [8] with learning rate 1×10^{-4} is utilized to train the baselines and our
 138 network. L2 regularization with hyperparameter 1×10^{-5} and 1×10^{-6} are employed for training
 139 6-DOF GraspNet (GAN) [9] and EquiGraspFlow.

140 B.3 Details for Grasping Motion in Real-World Experiments

141 The robot motion for grasping an object in real-world experiment is designed as follows. To prevent
 142 collisions with the object during the movement of the gripper toward the generated grasp pose, we
 143 first move the gripper to a pre-grasp pose. This pre-grasp pose is offset from the grasp pose by a
 144 small distance in the $-z$ direction in the gripper’s frame (the z -axis of the gripper’s frame represents
 145 the direction of gripper’s palm). Next, we move the gripper to the grasp pose and execute the grasp.
 146 Once the object is grasped, the gripper is lifted by 10cm. The success of the grasp is manually
 147 determined based on whether the object is held securely by the gripper. After each grasping attempt,
 148 we manually reset the position and orientation of the object to its initial state.

149 C Additional Results for Grasp Pose Generation

150 Figures 2 to 5 illustrate the additional visualizations of the generated grasp poses. These figures
 151 show the generated grasp poses of two mugs and two bowls for ten object rotations, along with the
 152 Earth Mover’s Distance (EMD) and grasp success rate values. The objects are rotated and input into
 153 each model, but in these figures, both the objects and the generated grasp poses are inversely rotated
 154 to align all scenes. Successful and failed grasp poses are indicated in green and red, respectively.

155 The grasp poses generated by EquiGraspFlow are widely distributed across various parts of the
 156 objects, demonstrating that our model generates more diverse grasp poses compared to the baselines.
 157 The values indicate that EquiGraspFlow generates grasp poses similar to the ground truth with high
 158 success rate. Additionally, the variance in the values indicates that EquiGraspFlow exhibits more
 159 consistent results across different object rotations. Notably, our model maintains identical value
 160 across the ten object rotations, demonstrating the perfect equivariance of our approach.

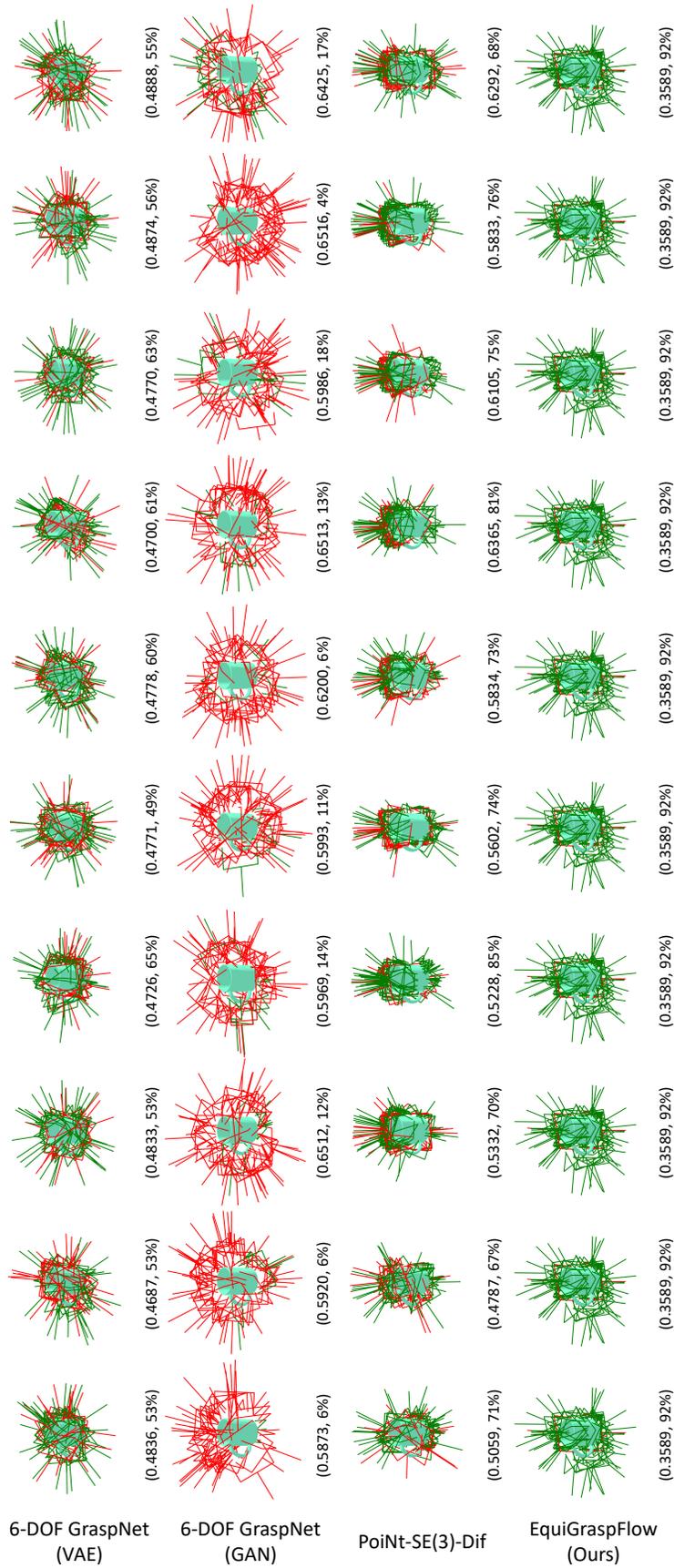


Figure 2: The generated grasp poses for the first mug across ten rotations.

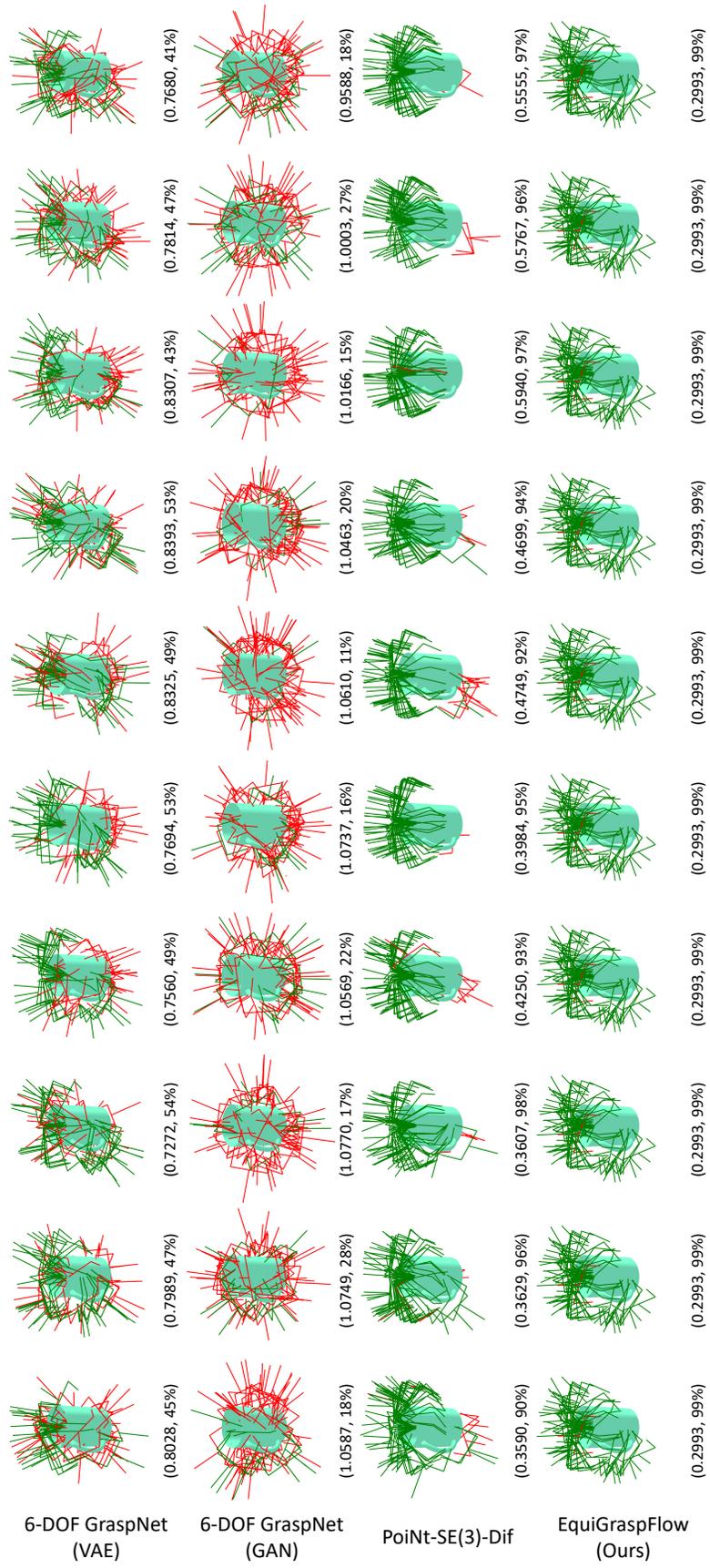


Figure 3: The generated grasp poses for the second mug across ten rotations.

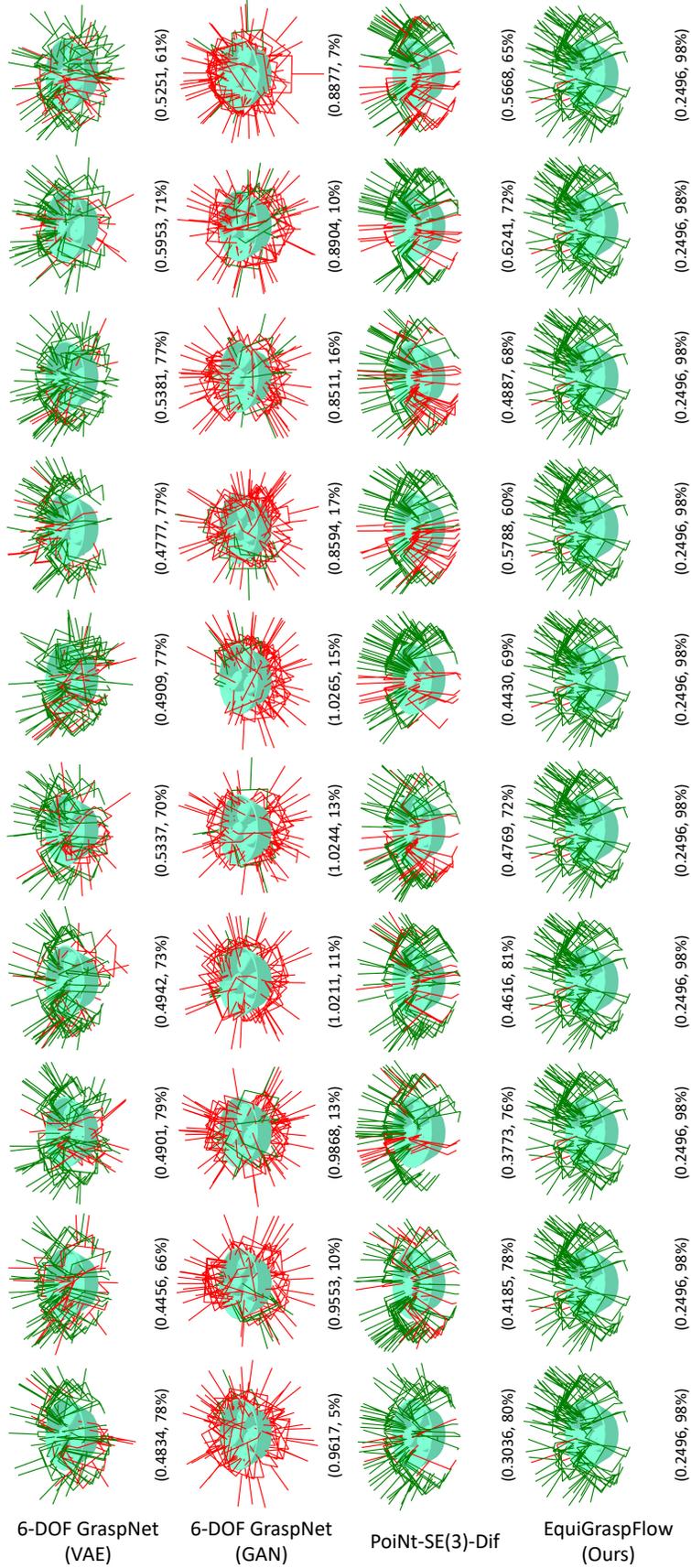


Figure 4: The generated grasp poses for the first bowl across ten rotations.

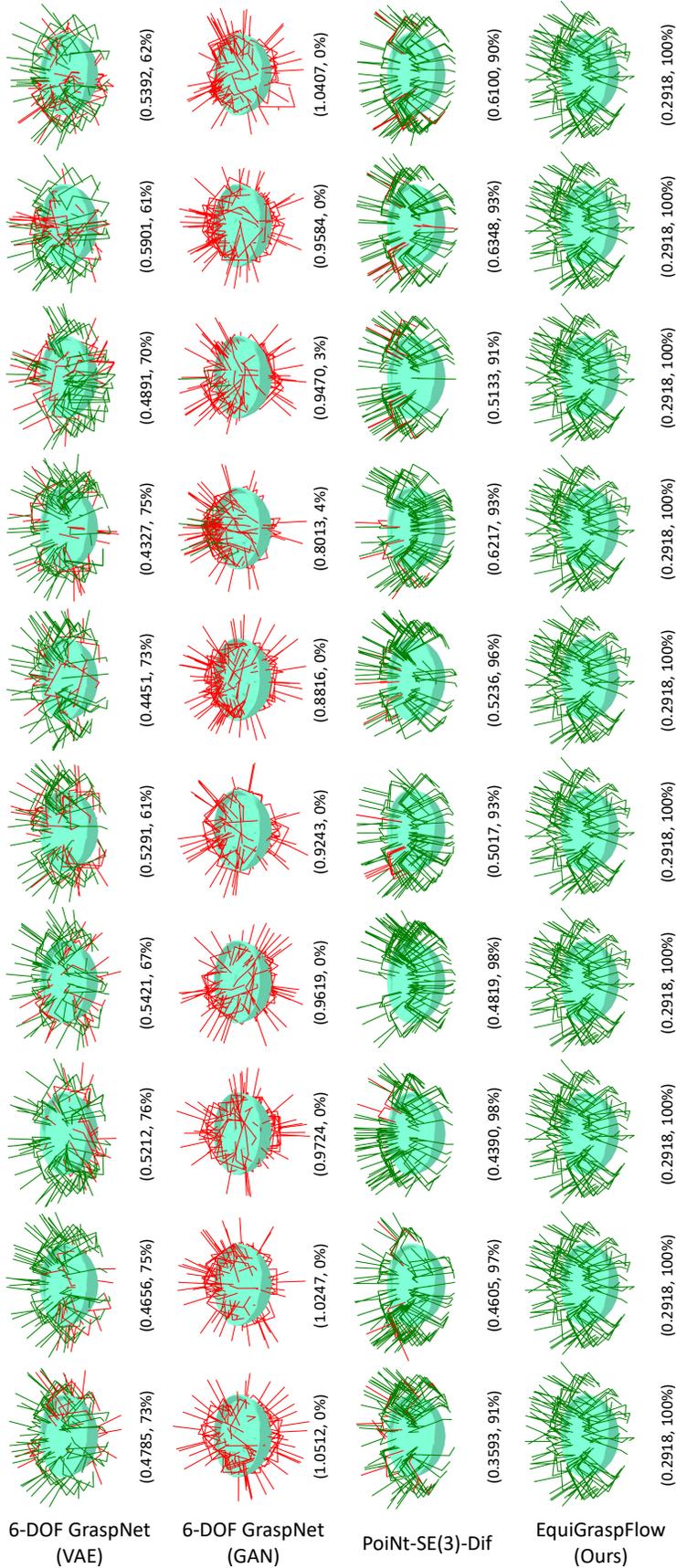


Figure 5: The generated grasp poses for the second bowl across ten rotations.

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