PT^2 -LLM: Post-Training Ternarization for Large Language Models

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Paper under double-blind review

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A FORMULATION AND DERIVATION OF THE ASYMMETRIC TERNARY QUANTIZER

A.1 ASYMETRIC TERNARY INITIALIZATION

We define the ternarization objective as:

$$\alpha^*, \mathbf{T}^* = \arg\min_{\alpha, \mathbf{T}} \|\widetilde{\mathbf{W}} - \alpha \mathbf{T}\|_F^2,$$
 (1)

where the centered weight matrix $\widetilde{\mathbf{W}}$ is computed by subtracting the row-wise mean:

$$\widetilde{\mathbf{W}} = \mathbf{W} - \mu, \quad \mu = \frac{1}{m} \sum_{j=1}^{m} \mathbf{W}_{:,j}.$$
 (2)

Each ternary value \mathbf{T}_{ij} is then determined using a fixed threshold Δ :

$$\mathbf{T}_{ij} = \begin{cases} 1, & \text{if } \widetilde{\mathbf{W}}_{ij} > \Delta, \\ 0, & \text{if } |\widetilde{\mathbf{W}}_{ij}| \le \Delta, \\ -1, & \text{if } \widetilde{\mathbf{W}}_{ij} < -\Delta. \end{cases}$$
(3)

Here, Δ serves as a positive threshold that determines which weights are set to -1, 0, or 1.

With this, the original problem reduces to optimizing over α and Δ :

$$\alpha, \, \Delta = \arg\min_{\alpha \ge 0, \, \Delta \ge 0} \left(|\mathbf{I}_{\Delta}| \cdot \alpha^2 - 2\alpha \sum_{(i,j) \in \mathbf{I}_{\Delta}} |\widetilde{\mathbf{W}}_{ij}| + c_{\Delta} \right), \tag{4}$$

where $\mathbf{I}_{\Delta} = \{(i,j) \mid |\widetilde{\mathbf{W}}_{ij}| > \Delta\}$ is the index set of non-zero ternary entries, and c_{Δ} is a constant independent of α .

The closed-form solution for α under fixed Δ is:

$$\alpha = \frac{1}{|\mathbf{I}_{\Delta}|} \sum_{(i,j) \in \mathbf{I}_{\Delta}} |\widetilde{\mathbf{W}}_{ij}|. \tag{5}$$

The optimal threshold Δ can be approximated by minimizing the squared error:

$$\Delta = \arg\min_{\Delta > 0} \left(\frac{1}{|\mathbf{I}_{\Delta}|} \left(\sum_{(i,j) \in \mathbf{I}_{\Delta}} |\widetilde{\mathbf{W}}_{ij}| \right)^{2} \right). \tag{6}$$

Since exact optimization is computationally expensive, we adopt a rule-of-thumb approximation:

$$\Delta \approx \frac{0.75}{m} \sum_{j=1}^{m} |\widetilde{\mathbf{W}}_{:,j}|. \tag{7}$$

A.2 ITERATIVE TERNARY FITTING

To reduce the discrepancy between the ternarized weights T and the original full-precision weights W, the following optimization problem is formulated:

$$\alpha, \mu = \underset{\alpha, \mu}{\operatorname{arg\,min}} ||(\alpha \mathbf{T} + \mu - \mathbf{W})||_F^2. \tag{8}$$

We rewrite the function as follows:

$$\|\alpha \mathbf{T} + \mu - \mathbf{W}\|_F^2 = \sum_j (\alpha_j \mathbf{t}_j + \mu_j - \mathbf{w}_j)^2$$
(9)

$$=\sum_{j} (\mathcal{E}_w)_j \tag{10}$$

$$=\mathcal{E}_w,\tag{11}$$

where \mathbf{t}_i denotes the j-th row of \mathbf{T} , and \mathbf{w}_i is the corresponding row of \mathbf{W} . Taking the gradient of the inner summand with respect to α_i and μ_i :

$$\frac{\partial \mathcal{E}_w}{\partial \alpha_j} = 2(\alpha_j \mathbf{t}_j + \mu_j \mathbf{1}^\top - \mathbf{w}_j) \mathbf{t}_j^\top, \tag{12}$$

$$\frac{\partial \mathcal{E}_w}{\partial \mu_j} = 2(\alpha_j \mathbf{t}_j + \mu_j \mathbf{1}^\top - \mathbf{w}_j) \mathbf{1}.$$
 (13)

Since the optimal solution is obtained at the stationary point,we set $\frac{\partial \mathcal{E}_w}{\partial \alpha_j} = 0$ and $\frac{\partial \mathcal{E}_w}{\partial \mu_i} = 0$:

$$\begin{bmatrix} \mathbf{t}_{j} \mathbf{t}_{j}^{\top} & \mathbf{1}^{\top} \mathbf{t}_{j}^{\top} \\ \mathbf{t}_{j} \mathbf{1} & \mathbf{1}^{\top} \mathbf{1} \end{bmatrix} \begin{bmatrix} \alpha_{j} \\ \mu_{j} \end{bmatrix} = \begin{bmatrix} \mathbf{w}_{j} \mathbf{t}_{j}^{\top} \\ \mathbf{w}_{j} \mathbf{1} \end{bmatrix}.$$
(14)

Summing over j,we can solve for the

$$\alpha = \frac{1}{ad - bc}(dy_1 - by_2), \quad \mu = \frac{1}{ad - bc}(ay_2 - cy_1), \tag{15}$$

where all operations are taken to be element-wise and

$$a = \operatorname{diag}(\mathbf{T}\mathbf{T}^{\top}), \quad b = c = \mathbf{T}\mathbf{1}, \quad d = \mathbf{1}^{\top}\mathbf{1},$$
 (16)

$$y_1 = \mathbf{diag}(\mathbf{W}\mathbf{T}^\top), \quad y_2 = \mathbf{diag}(\mathbf{W}\mathbf{1}),$$
 (17)

 By substituting a, b, c, d, y_1, y_2 into the above conditions, we obtain the closed-form solutions for α and μ :

$$\alpha = \frac{\mathbf{1}^{\top} \mathbf{1} \cdot \mathbf{diag}(\mathbf{W} \mathbf{T}^{\top}) - (\mathbf{T} \mathbf{1}) \circ \mathbf{diag}(\mathbf{W} \mathbf{1})}{\mathbf{diag}(\mathbf{T} \mathbf{T}^{\top}) \cdot \mathbf{1}^{\top} \mathbf{1} - (\mathbf{T} \mathbf{1})^{2}},$$
(18)

$$\mu = \frac{\left(\operatorname{diag}(\mathbf{T}\mathbf{T}^{\top}) \circ \operatorname{\mathbf{diag}}(\mathbf{W}\mathbf{1}) - (\mathbf{T}\mathbf{1}) \circ \operatorname{\mathbf{diag}}(\mathbf{W}\mathbf{T}^{\top})\right)}{\operatorname{diag}(\mathbf{T}\mathbf{T}^{\top}) \cdot \mathbf{1}^{\top}\mathbf{1} - (\mathbf{T}\mathbf{1})^{2}}.$$
(19)

We define

$$\mathbf{Z} = \frac{\mathbf{W} - \mu}{\alpha},$$

for every element in T, we update it as follows:

$$\mathbf{T}_{ij} = \underset{t \in \{-1,0,1\}}{arg \min} |\mathbf{Z}_{ij} - t|. \tag{21}$$

(20)

ACTIVATION-AWARE GRID ALIGNMENT

To optimize the ternarized weights T based on the calibration data X, we formulate the following problem:

$$\alpha, \mu = \underset{\alpha, \mu}{\operatorname{arg\,min}} ||(\alpha \mathbf{T} + \mu - \mathbf{W}) \mathbf{X}||_F^2, \tag{22}$$

We rewrite the problem as follows:

$$||(\alpha \mathbf{T} + \mu - \mathbf{W})\mathbf{X}||_F^2 = \sum_{b=1} \sum_{i=1} ||(\alpha \mathbf{T} + \mu - \mathbf{W})\mathbf{X}_{b,:,i}||_2^2$$
 (23)

$$= \sum_{j} \sum_{b} \sum_{i} \left[(\alpha_{j} \mathbf{t}_{j} + \mu_{j} \mathbf{1}^{\top} - \mathbf{w}_{j}) \mathbf{X}_{b,:,i} \right]^{2}$$
 (24)

$$=\sum_{j}\sum_{b}\sum_{i}(\mathcal{E}_{x})_{jbi}$$
(25)

$$=\mathcal{E}_x. \tag{26}$$

where \mathbf{t}_j denotes the j-th row of \mathbf{T} , and \mathbf{w}_j is the corresponding row of \mathbf{W} . Taking the gradient of the inner summand with respect to α_j and μ_j :

$$\frac{\partial \mathcal{E}_x}{\partial \alpha_j} = 2[(\alpha_j \mathbf{t}_j + \mu_j \mathbf{1}^\top - \mathbf{w}_j) \mathbf{X}_{bi}] \mathbf{t}_j \mathbf{X}_{bi}, \tag{27}$$

$$\frac{\partial \mathcal{E}_x}{\partial \mu_j} = 2[(\alpha_j \mathbf{t}_j + \mu_j \mathbf{1}^\top - \mathbf{w}_j) \mathbf{X}_{bi}] \mathbf{1}^\top \mathbf{X}_{bi}.$$
(28)

To simplify the problem, we let $\mathbf{S}_j = \alpha_j \mathbf{t}_j + \mu_j \mathbf{1}^\top - \mathbf{w}_j$, then we derive

$$\frac{\partial \mathcal{E}_x}{\partial \alpha_j} = 2 \sum_b \sum_i (\mathbf{S}_j \mathbf{X}_{bi}) (\mathbf{t}_j \mathbf{X}_{bi})$$
(29)

$$=2\sum_{b}\sum_{i}\mathbf{S}_{j}\mathbf{X}_{bi}\mathbf{X}_{bi}^{\mathsf{T}}\mathbf{t}_{j}$$
(30)

$$=2\mathbf{S}_{j}\sum_{b}\sum_{i}\mathbf{X}_{bi}\mathbf{X}_{bi}^{\top}\mathbf{t}_{j}$$
(31)

$$= 2\mathbf{S}_{j}\mathbf{C}\mathbf{t}_{j}, \quad \left(\mathbf{C} = \sum_{b} \sum_{i} \mathbf{X}_{bi} \mathbf{X}_{bi}^{\top}\right)$$
(32)

which leads to:

$$\frac{1}{2} \frac{\partial \mathcal{E}_x}{\partial \alpha_j} = (\mathbf{t}_j \mathbf{C} \mathbf{t}_j^\top) \alpha_j + (\mathbf{1}^\top \mathbf{C} \mathbf{t}_j^\top) \mu_j - \mathbf{w}_j \mathbf{C} \mathbf{t}_j, \tag{33}$$

$$\frac{1}{2} \frac{\partial \mathcal{E}_x}{\partial \mu_j} = (\mathbf{t}_j \mathbf{C} \mathbf{1}) \alpha_j + (\mathbf{1}^\top \mathbf{C} \mathbf{1}) \mu_j - \mathbf{w}_j \mathbf{C} \mathbf{1}.$$
 (34)

Let $\frac{\partial \mathcal{E}_x}{\partial \alpha_j} = 0$ and $\frac{\partial \mathcal{E}_x}{\partial \mu_j} = 0$:

$$\begin{bmatrix} \mathbf{t}_{j} \mathbf{C} \mathbf{t}_{j}^{\top} & \mathbf{1}^{\top} \mathbf{C} \mathbf{t}_{j}^{\top} \\ \mathbf{t}_{j} \mathbf{C} \mathbf{1} & \mathbf{1}^{\top} \mathbf{C} \mathbf{1} \end{bmatrix} \begin{bmatrix} \alpha_{j} \\ \mu_{j} \end{bmatrix} = \begin{bmatrix} \mathbf{w}_{j} \mathbf{C} \mathbf{t}_{j} \\ \mathbf{w}_{j} \mathbf{C} \mathbf{1} \end{bmatrix}.$$
 (35)

The result can be written as follows:

$$\begin{bmatrix} a_j & b_j \\ c_j & d_j \end{bmatrix} \begin{bmatrix} \alpha_j \\ \mu_j \end{bmatrix} = \begin{bmatrix} y_{1j} \\ y_{2j} \end{bmatrix}, \tag{36}$$

Summing over j:

$$\begin{bmatrix} a_{1} & 0 & 0 & \cdots & b_{1} & 0 & 0 & \cdots \\ 0 & a_{2} & 0 & \cdots & 0 & b_{2} & 0 & \cdots \\ \vdots & \vdots \\ 0 & 0 & 0 & a_{n} & 0 & 0 & 0 & b_{n} \\ c_{1} & 0 & 0 & \cdots & d_{1} & 0 & 0 & \cdots \\ 0 & c_{2} & 0 & \cdots & 0 & d_{2} & 0 & \cdots \\ \vdots & \vdots \\ 0 & 0 & 0 & c_{n} & 0 & 0 & 0 & d_{n} \end{bmatrix} \begin{bmatrix} \alpha \\ \mu \end{bmatrix} = \begin{bmatrix} y_{1} \\ y_{2} \end{bmatrix},$$

$$(37)$$

from which the closed-form solutions are obtained:

$$\alpha = \frac{1}{ad - bc}(dy_1 - by_2), \quad \mu = \frac{1}{ad - bc}(ay_2 - cy_1), \tag{38}$$

where all operations are taken to be element-wise and

$$a = \operatorname{diag}(\mathbf{T}\mathbf{C}\mathbf{T}^{\top}), \quad b = c = \mathbf{T}\mathbf{C}\mathbf{1}, \quad d = \mathbf{1}^{\top}\mathbf{C}\mathbf{1},$$
 (39)

$$y_1 = \mathbf{diag}(\mathbf{WCT}^{\mathsf{T}}), \quad y_2 = \mathbf{WC1}.$$
 (40)

We obtain the closed-form solutions:

$$\alpha = \frac{d \cdot (\mathbf{W} \circ \mathbf{T})\mathbf{S}\mathbf{1} - \mathbf{v} \circ (\mathbf{W}\mathbf{S}\mathbf{1})}{d \cdot \mathbf{T}^2\mathbf{S}\mathbf{1} - \mathbf{v}^2}, \quad \mu = \frac{\mathbf{T}^2\mathbf{S}\mathbf{1} \circ (\mathbf{W}\mathbf{S}\mathbf{1}) - \mathbf{v} \circ [(\mathbf{W} \circ \mathbf{T})\mathbf{S}\mathbf{1}]}{d \cdot \mathbf{T}^2\mathbf{S}\mathbf{1} - \mathbf{v}^2}, \quad (41)$$

where $d = \mathbf{1}^{\mathsf{T}} \mathbf{S} \mathbf{1}$ is a scalar, and $\mathbf{v} = \mathbf{T} \mathbf{S} \mathbf{1}$; \mathbf{T}^2 and \mathbf{v}^2 denote element-wise squares.

A.4 OVERFITTING IN ACTIVATION-AWARE GRID ALIGNMENT

To improve the expressiveness and accuracy of ternarized models, we aim to minimize the activation-aware output error \mathcal{E}_x , which measures how well the quantized weights approximate the original full-precision weights when interacting with representative calibration data. Under this objective, we experiment with two strategies for updating the ternary code matrix \mathbf{T} .

Gradient-based Projection. The first approach treats \mathbf{T} as a continuous variable during optimization. After computing the gradient of the loss with respect to \mathbf{T} , the result is projected back to the ternary set -1,0,1 through simple nearest rounding. While this method is conceptually straightforward, we observe that it often yields suboptimal solutions. The mismatch between continuous optimization and discrete rounding makes it difficult to consistently lower the reconstruction error across the entire matrix.

Column-wise Greedy Update. The second approach greedily updates one column of **T** at a time, keeping all other columns fixed. Each column-wise update becomes a low-dimensional subproblem with a closed-form optimal solution over ternary values. Empirically, this method substantially reduces the output more effectively than the projection method.

Overfitting Phenomenon. Surprisingly, we find that aggressive minimization of the reconstruction loss leads to overfitting. While the greedy strategy significantly lowers the error with respect to the calibration set, the final model performs worse on downstream tasks. This indicates that overly aligning ternary weights to calibration data may distort the model's inductive biases and impair generalization—especially in autoregressive or masked settings common in diffusion-based LLMs.

Future Directions. To address this overfitting, future work may explore regularization techniques that limit excessive fitting to calibration samples, curriculum-based updates that gradually refine \mathbf{T} , or multi-objective formulations that combine reconstruction loss with downstream task loss. Another promising direction is to precondition the \mathbf{T} update using meta-learned or task-aware initializations.

Table: Effect of T Optimization on Model Performance

T Update Method	Avg. Output Error $\mathcal{E}_x \downarrow$	Avg. Accuracy ↑		
Without T Update	128.3	0.4507		
Greedy Column-wise Update	24.7	0.4213		

Table 1: Evaluation on LLaMA-7B: While greedy column-wise updates to the ternary matrix T significantly reduce the activation-aware output error \mathcal{E}_x , they also lead to a notable drop in downstream average accuracy. This suggests a trade-off between low-level reconstruction and high-level generalization, highlighting the risk of overfitting under aggressive quantization.

B IMPLEMENTATION DETAILS FOR THROUGHPUT EXPERIMENTS

All throughput experiments are conducted on the llama.cpp platform using NVIDIA A800 GPUs. We leverage the platform's native support for ternary quantization operators as the basis for our extension. Specifically, we integrate our proposed *Asymmetric Ternary Quantizer* into the existing operator framework, ensuring compatibility with the platform's optimized low-bit inference path.

In addition to quantizer integration, we implement a runtime module that performs activation reordering during forward inference, in accordance with the *Structural Similarity-based Reordering (SSR)* strategy. This module dynamically adjusts the layout of activations to match the reordered column structure expected by SSR, enabling compatibility with ternary matrix operations. The entire logic is seamlessly integrated into the forward pass.

Our quantization pipeline targets all linear layers within the model, including projection and feed-forward modules, while the activation values are preserved at 16-bit precision throughout inference. This design choice ensures a fair comparison with prior methods that retain higher-precision activations, and avoids confounding effects introduced by activation quantization. All modifications are implemented in C++ with CUDA acceleration preserved through the original backend.

C MEMORY FOOTPRINT ANALYSIS

To evaluate the storage efficiency of our ternarization scheme, we analyze the memory footprint introduced by each component in the quantized model.

Ternary Weight Encoding. We adopt a compact encoding strategy in which 5 ternarized values (each taking values from $\{-1,0,+1\}$) are packed into a single 8-bit integer. This yields an effective average of 1.6 bits per weight element.

Per-block Quantization Parameters. In addition to the ternary codes, each block of weights shares two 16-bit floating-point parameters: a scaling factor α and a shift μ , which are used to reconstruct the approximate full-precision values. The block size is fixed (e.g., 128), and the overhead introduced by these scalars is amortized across all elements in the block, contributing only a small fraction to the overall storage.

Unquantized Modules. Following common practice in LLM compression, certain modules are kept in full precision to preserve model quality. In our implementation, both the LayerNorm layers and the lm-head (final projection layer) are left unquantized. These components constitute a small portion of the total parameters and do not significantly impact the compression ratio.

D DETAILED PROCEDURE OF THE ASYMMETRIC TERNARY QUANTIZER

Algorithm 1 provides the complete pseudocode for the Asymmetric Ternary Quantizer (ATQ). It elaborates the full ternarization procedure, including initialization, iterative ternary fitting, and the activation-aware grid alignment (AGA) phase. This modular pipeline enables efficient and accurate weight ternarization while adapting to activation statistics from calibration data.

Algorithm 1 Asymmetric Ternary Quantizer (ATQ)

Weight matrix $\mathbf{W} \in \mathbb{R}^{n \times m}$; calibration data $\mathbf{X} \in \mathbb{R}^{B \times L \times m}$ Quantized weight matrix $\widehat{\mathbf{W}} \in \mathbb{R}^{n \times m}$

Step 1: Ternary Initialization

Compute row-wise bias: $\mu \leftarrow \frac{1}{m} \sum_{i=1}^{m} \mathbf{W}_{:,i}$

Center weights: $\mathbf{\tilde{W}} \leftarrow \mathbf{W} - \mu$

Compute threshold: $\Delta \leftarrow \frac{0.75}{m} \sum_{j=1}^{m} |\widetilde{\mathbf{W}}_{:,j}|$

Initialize ternary matrix: $\mathbf{T}_{ij} \leftarrow \begin{cases} 1 & \text{if } \widetilde{\mathbf{W}}_{ij} > \Delta \\ -1 & \text{if } \widetilde{\mathbf{W}}_{ij} < -\Delta \\ 0 & \text{otherwise} \end{cases}$ Initialize scale: $\alpha \leftarrow \frac{\sum_{j=1}^{m} \mathbf{T}_{:,j} \cdot \widetilde{\mathbf{W}}_{:,j}}{\sum_{j=1}^{m} |\mathbf{T}_{:,j}|}$

Step 2: Iterative Ternary Fitting (ITF)

T not converged Update grid parameters (α, μ) using:

$$\alpha^* = \frac{m \cdot (\mathbf{W} \circ \mathbf{T})\mathbf{1} - (\mathbf{T1}) \circ (\mathbf{W1})}{m \cdot (\mathbf{T} \circ \mathbf{T})\mathbf{1} - (\mathbf{T1})^2}$$
$$\mu^* = \frac{(\mathbf{T} \circ \mathbf{T})\mathbf{1} \circ (\mathbf{W1}) - (\mathbf{T1}) \circ [(\mathbf{W} \circ \mathbf{T})\mathbf{1}]}{m \cdot (\mathbf{T} \circ \mathbf{T})\mathbf{1} - (\mathbf{T1})^2}$$

Update ternary matrix:

$$\mathbf{T}_{ij} \leftarrow \arg\min_{t \in \{-1,0,1\}} \left| \frac{\mathbf{W}_{ij} - \mu_i^*}{\alpha_i^*} - t \right|$$

Step 3: Activation-aware Grid Alignment (AGA)

Compute activation covariance: $\mathbf{S} \leftarrow \sum_{b,i} \mathbf{X}_{b,:,i} \mathbf{X}_{b,:,i}^{\top}$

Update (α, μ) using:

$$\alpha^* = \frac{d \cdot (\mathbf{W} \circ \mathbf{T})\mathbf{S}\mathbf{1} - \mathbf{v} \circ (\mathbf{W}\mathbf{S}\mathbf{1})}{d \cdot \mathbf{T}^2\mathbf{S}\mathbf{1} - \mathbf{v}^2} \quad \mu^* = \frac{\mathbf{T}^2\mathbf{S}\mathbf{1} \circ (\mathbf{W}\mathbf{S}\mathbf{1}) - \mathbf{v} \circ [(\mathbf{W} \circ \mathbf{T})\mathbf{S}\mathbf{1}]}{d \cdot \mathbf{T}^2\mathbf{S}\mathbf{1} - \mathbf{v}^2}$$

where $d = \mathbf{1}^{\top} \mathbf{S} \mathbf{1}$, $\mathbf{v} = \mathbf{T} \mathbf{S} \mathbf{1}$

Step 4: Final Quantization

$$\widehat{\mathbf{W}} \leftarrow \alpha \mathbf{T} + \mu$$

E VISUALIZATION

E.1 COLUMN-WISE DEVIATION PATTERNS

We visualize representative weight matrices from LLaMA-3-8B and observe clear column-wise deviation patterns 1. This column-wise asymmetry highlights the rationality of performing column-wise reordering prior to quantization, as it helps to better align the weight distribution and improve representational efficiency.

E.2 ASYMMETRIC WEIGHT DISTRIBUTION VISUALIZATION

As shown in Figure 2, many weight matrices in LLaMA-3-8B exhibit clear asymmetric distributions. Rather than being centered around zero, some layers present skewed profiles where a significant portion of weights deviate toward one side. In particular, we observe long tails or outlier concentrations either on the positive or negative axis, highlighting the existence of asymmetry. This property suggests that symmetric quantization may be suboptimal, and motivates the need for asymmetric or distribution-aware quantization strategies.

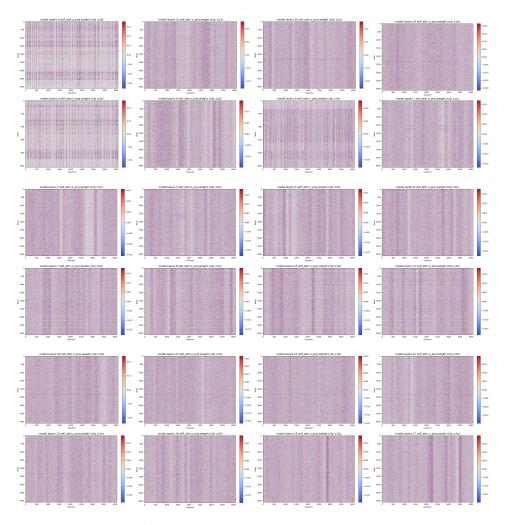


Figure 1: Visualization of column-wise deviation patterns across three representative layers.

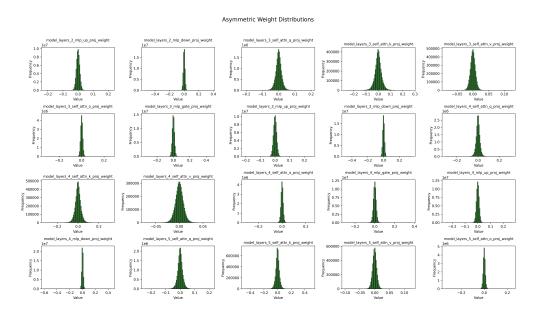


Figure 2: Histogram visualizations of selected weight matrices from LLaMA-3-8B.

432 DIALOG EXAMPLES 433 434 435 **Prompt:** Shakespeare was a famous writer from 436 **Slim-LLM:** Shakespeare was a famous writer from the 19th century. He was a poet and a playwright. 437 He was born in 1809 and died in 1849. **GPTQ**: Shakespeare was a famous writer from a \$100) 438 PT²-LLM: Shakespeare was a famous writer from the 16th century. He wrote many plays and poems. 439 Shakespeare is considered to be the greatest writer in the English language. 440 **Prompt:** Beethoven was a composer from 441 Slim: Beethoven was a composer from the 16th century. He was born in 1560 in Germany. 442 **GPTQ**: Beethoven was a composer from Homomal Homers 443 PT: Beethoven was a composer from the late 18th century. He was born in Bonn, Germany, and died 444 in Vienna, Austria. Beethoven was a composer, pianist, and conductor. He was also a teacher. 445 **Prompt:** The Pyramids are located in 446 **Slim:** The Pyramids are located in the middle of the pyramid. 447 **GPTQ**: The Pyramids are located in the United States. PT²-LLM: The Pyramids are located in the Egyptian desert. 449 **Prompt:** The Great Barrier Reef is in 450 **Slim-LLM**: The Great Barrier Reef is in the Coral Sea, and is the largest single natural feature on **GPTQ**: The Great Barrier Reef is in the LATs. 452 PT²-LLM: The Great Barrier Reef is in the north-east of Australia. It is the largest reef system in the 453 world. It is 1,200 km long and 150 km wide. 454 **Prompt:** the chemical symbol for gold is 455 **Slim-LLM**: The chemical symbol for gold is C. The chemical symbol for silver is Ag. The chemical 456 symbol for copper is Cu. The chemical symbol for lead is Pb. The chemical symbol for mercury 457 is Hg. The chemical symbol for platinum is Pt. The chemical symbol for tin is Sn. The chemical 458 symbol for zinc is Zn. The chemical symbol for iron is Fe. The chemical symbol for nickel is Ni. 459 The chemical symbol for chromium is Cr. The chemical symbol for bismuth is Bi. 460 **GPTQ**: the chemical symbol for gold is not the same as a person 461 **PT**²**-LLM:** The chemical symbol for gold is Au. The symbol for silver is Ag. The symbol for iron 462 is Fe. The symbol for lead is Pb. The symbol for zinc is Zn. The symbol for mercury is Hg. The 463 symbol for copper is Cu. The symbol for nickel is Ni. The symbol for chromium is Cr. **Prompt:** Michael Jordan played most of his career with the 464 Slim-LLM: Michael Jordan played most of his career with the Washington Bullets. He was the first 465 player to win the NBA Most Valuable Player Award. 466 **GPTQ**: Michael Jordan played most of his career with the The FBI 467 PT²-LLM: Michael Jordan played most of his career with the Chicago Bulls, and was a member of 468 the 1996 NBA All-Star team. 469 **Prompt:** The composer of "The Four Seasons" is 470 **Slim-LLM:** The Four Seasons is the composer of "The Four Seasons" is the composer of "The Four 471 472 **GPTQ**: The composer of "The Four Seasons" is the "T" Night. 473 PT²-LLM: The composer of "The Four Seasons" is Antonio Vivaldi, who was born in 1685. He was 474 a composer, and he wrote "The Four Seasons" in 1725. He was born in Venice, Italy. 475 **Prompt:** Water boils at 476 **Slim-LLM**: Water boils at the surface of the water. 477 **GPTO**: Water boils at A 478 **PT**²**-LLM:** Water boils at 100°C.

479 480

Table 2: **Evaluation on Multiple LLM Backbones.** We report perplexity (PPL) on WikiText2 and C4, and accuracy (%) on seven zero-shot tasks. All quantized models use block size 128.

PF16	Model	Method	#W	Wiki2(↓)	C4 (↓)	PiQA	Arc E	Arc C	Hella.	Wino.	OBQA	BoolQ	Avg(↑)
Qwen3-0.6B-base GPTQ culP 2 5.37ca 3 3.57ca 3 5.15ca 4.906 19.62 25.34 49.96 15.20 42.32 32.71 NA Qwen3-0.6B-base QuIP culP 2 N/A		FP16	16	12.70	17.10	70.00	65.60	33.90	41.10	58.50	24.60	69.70	51.91
Qwen3-0.6B-base QuIP 2 N/A													
Slim-LLM		GPTQ	2	5.37e3	3.57e3	51.58	24.96	19.62	25.34	49.96	15.20	42.32	32.71
PB-LLM 1.78	Qwen3-0.6B-base	QuIP		N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
PT ² LLM		Slim-LLM		282.12	1190.46	54.03	27.95	21.25	26.03	49.64	16.80	39.82	
FP16			1.7	1.25e6	1.68e6	51.14	24.75	11.25	25.29	51.10	12.60	34.80	30.13
AWQ 2 1.13e7 1.02e7 52.40 24.00 21.70 25.60 49.40 10.00 48.50 33.09 GPTQ 2 101.69 375.74 52.12 27.23 18.94 26.29 52.96 17.80 44.98 34.33 34.33 34.34 34.		PT ² -LLM	1.58	145.57	617.11	53.21	30.77	18.77	26.33	51.22	13.80	37.83	33.13
Qwen3-1.7B-base GPTQ 2 101.69 375.74 52.12 27.23 18.94 26.29 52.96 17.80 44.98 34.33 Qwen3-1.7B-base QuIP 2 N/A N/A <td></td> <td>FP16</td> <td>16</td> <td>9.39</td> <td>13.40</td> <td>75.70</td> <td>73.20</td> <td>41.50</td> <td>49.20</td> <td>64.20</td> <td>30.20</td> <td>79.20</td> <td>59.03</td>		FP16	16	9.39	13.40	75.70	73.20	41.50	49.20	64.20	30.20	79.20	59.03
Qwen3-1.7B-base QuIP Slim-LLM 2 Slim-LLM 2 PB-LLM 1.7 2 Slim-LLM 2 Slim-LLM 2 PB-LLM 1.7 N/A Slim-LLM 2 Slim-LLM 2 PT-2 LLM 1.58 N/A Slim-LLM 2 PT-2 LLM 1.58 N/A Slim-LLM 2 PT-2 LLM 1.58 N/A Slim-LM 1.7 N/A Slim-LM 1.7 <td></td> <td></td> <td>2</td> <td>1.13e7</td> <td>1.02e7</td> <td></td> <td></td> <td>21.70</td> <td></td> <td></td> <td></td> <td>48.50</td> <td></td>			2	1.13e7	1.02e7			21.70				48.50	
Qwen3-1.7B-base QuIP 2 N/A		GPTQ	2	101.69	375.74	52.12	27.23	18.94	26.29	52.96	17.80	44.98	34.33
PB-LLM	Qwen3-1.7B-base	QuIP	2	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
PT²-LLM				70.14	280.59		31.69	19.45		50.43	12.60	35.66	
FP16			1.7	6.85e5	4.41e5	52.23	24.58	20.99	25.52	50.36	13.60	41.87	32.74
Qwen3-4B-base AWQ GPTQ 2 7.53e6 G5.14 or 193.61 53.40 or 24.70 or 22.20 or 25.80 or 47.50 or 11.10 or 46.80 or 33.07 or 33.07 or 32.07 or		PT ² -LLM	1.58	66.67	338.19	54.68	31.90	20.22	26.79	51.62	11.20	38.81	33.60
Qwen3-4B-base GPTQ QuIP 2 65.17 NA 193.61 NA 52.61 NA 27.53 NA 20.73 NA 27.38 NA 51.46 NA 17.00 NA 45.50 NA 34.60 NA Qwen3-4B-base QuIP 2 N/A 18.60 22.60 25.00 20.00 55.87 37.36 32.24 PB-LLM 1.58 37.54 153.78 54.62 36.78 19.71 27.65 53.67 13.40 55.72 37.36 66.71 13.147 75.00 26.00 22.60 25.00 50.00 12.00 44.60 </td <td></td> <td>FP16</td> <td>16</td> <td>7.90</td> <td>11.60</td> <td>78.10</td> <td>79.00</td> <td>48.40</td> <td>54.60</td> <td>70.00</td> <td>31.40</td> <td>82.90</td> <td>63.49</td>		FP16	16	7.90	11.60	78.10	79.00	48.40	54.60	70.00	31.40	82.90	63.49
Qwen3-4B-base GPTQ QuIP 2 65.17 NA 193.61 NA 52.61 NA 27.53 NA 20.73 NA 27.38 NA 51.46 NA 17.00 NA 45.50 NA 34.60 NA Qwen3-4B-base QuIP 2 N/A 18.60 22.60 25.00 20.00 55.87 37.36 32.24 PB-LLM 1.58 37.54 153.78 54.62 36.78 19.71 27.65 53.67 13.40 55.72 37.36 66.71 13.147 75.00 26.00 22.60 25.00 50.00 12.00 44.60 </td <td></td> <td>AWQ</td> <td>2</td> <td>7.53e6</td> <td>5.94e6</td> <td>53.40</td> <td>24.70</td> <td>22.20</td> <td>25.80</td> <td>47.50</td> <td>11.10</td> <td>46.80</td> <td>33.07</td>		AWQ	2	7.53e6	5.94e6	53.40	24.70	22.20	25.80	47.50	11.10	46.80	33.07
Qwen3-4B-base QuIP 2 N/A N/A <t< td=""><td></td><td>GPTQ</td><td></td><td>65.17</td><td>193.61</td><td>52.61</td><td>27.53</td><td>20.73</td><td>27.38</td><td>51.46</td><td>17.00</td><td>45.50</td><td>34.60</td></t<>		GPTQ		65.17	193.61	52.61	27.53	20.73	27.38	51.46	17.00	45.50	34.60
PB-LLM	Qwen3-4B-base	QuIP	2	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
PT²-LLM		Slim-LLM	2	16.22	36.93	52.57	28.78	22.61	25.38	55.09	20.00	55.87	37.19
FP16			1.7	5.71e5	7.48e5	52.12	25.00	21.33	25.80	48.46	12.80	40.15	32.24
AWQ GPTQ 2 1.66e7 1.31e7 52.60 26.60 22.60 25.50 50.00 12.00 44.60 33.41 Qwen3-8B-base QuIP 2 106.41 347.02 57.40 30.60 20.50 33.40 52.50 16.40 48.70 37.07 Sim-LLM 2 N/A 11.60 4.31 32.96		PT ² -LLM	1.58	37.54	153.78	54.62	36.78	19.71	27.65	53.67	13.40	55.72	37.36
AWQ GPTQ 2 1.66e7 106.41 1.31e7 347.02 52.60 57.40 26.60 30.60 22.50 20.50 25.50 33.40 50.00 52.50 12.00 16.40 44.60 48.70 33.41 37.07 Qwen3-8B-base QuIP Slim-LLM 2 N/A N/A N/A N/A </td <td></td> <td></td> <td>16</td> <td>6.99</td> <td>10.40</td> <td>79.30</td> <td>82.10</td> <td>52.60</td> <td>58.90</td> <td>72.10</td> <td>32.80</td> <td>82.90</td> <td>65.81</td>			16	6.99	10.40	79.30	82.10	52.60	58.90	72.10	32.80	82.90	65.81
Qwen3-8B-base QuIP Slim-LLM 2 37.60 1/43.57 1.91e4 N/A 2.60 N/A 2.60 N/A 3.9.4 N/A		AWQ	2	1.66e7	1.31e7	52.60	26.60	22.60	25.50	50.00	12.00	44.60	33.41
Slim-LLM 2 37.60 143.57 50.59 49.49 17.63 32.96 54.40 16.20 53.30 39.22 PB-LLM 1.7 1.91e4 2.26e4 53.05 26.56 20.73 25.73 49.17 14.60 40.31 32.88 PT²-LLM 1.58 31.82 138.84 56.64 40.53 18.86 30.65 55.09 14.20 58.04 39.14 FP16 16 4.10 6.13 80.96 80.30 52.90 63.37 75.77 36.00 82.69 67.43 AWQ 2 2.40e5 2.40e5 52.77 24.79 23.46 25.37 48.86 16.40 62.17 36.26 GPTQ 2 15.29 14.86 62.84 42.80 22.01 39.74 53.59 19.40 54.80 42.17 L-30B QuIP 2 22.30 19.33 N/A N/A N/A N/A N/A N/A N/A N/A N/A Slim-LLM 2 7.16 13.14 75.52 51.29 39.29 66.10 64.07 15.00 62.01 53.33 PB-LLM 1.7 23.72 25.16 63.87 48.06 23.04 35.13 60.30 17.20 62.69 44.33 PT²-LLM 1.58 7.35 13.23 70.24 64.10 32.94 44.00 68.43 25.40 69.24 53.48 FP16 16 4.88 6.73 79.05 79.42 48.38 60.03 72.22 35.20 80.55 64.98 AWQ 2 1.20e5 9.40e4 53.26 26.09 22.70 25.57 48.93 13.40 62.17 36.02 GPTQ 2 23.63 19.66 60.77 42.85 20.48 34.03 54.06 17.00 58.04 41.03 L2-13B QuIP 2 13.48 16.16 N/A N/A N/A N/A N/A N/A N/A N/A Slim-LLM 2 9.98 22.62 66.54 52.09 26.37 33.83 50.06 21.40 64.74 45.00 PB-LLM 1.7 236.42 184.67 54.68 27.36 18.86 26.58 50.43 13.20 38.20 32.76		GPTQ	2	106.41	347.02	57.40	30.60	20.50	33.40	52.50	16.40	48.70	37.07
PB-LLM	Qwen3-8B-base	QuIP	2	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
PT²-LLM		Slim-LLM	2	37.60	143.57	50.59	49.49	17.63	32.96	54.40	16.20	53.30	39.22
FP16			1.7	1.91e4	2.26e4	53.05	26.56	20.73	25.73	49.17	14.60	40.31	32.88
FP16		PT ² -LLM	1.58	31.82	138.84	56.64	40.53	18.86	30.65	55.09	14.20	58.04	39.14
L-30B			16	4.10	6.13	80.96	80.30	52.90		75.77	36.00	82.69	67.43
L-30B		AWQ	2	2.40e5	2.40e5	52.77	24.79	23.46	25.37	48.86	16.40	62.17	36.26
Slim-LLM 2 7.16 13.14 75.52 51.29 39.29 66.10 64.07 15.00 62.01 53.33 PB-LLM 1.7 23.72 25.16 63.87 48.06 23.04 35.13 60.30 17.20 62.69 44.33 PT^2-LLM 1.58 7.35 13.23 70.24 64.10 32.94 44.00 68.43 25.40 69.24 53.48 FP16 16 4.88 6.73 79.05 79.42 48.38 60.03 72.22 35.20 80.55 64.98 AWQ 2 1.20e5 9.40e4 53.26 26.09 22.70 25.57 48.93 13.40 62.17 36.02 GPTQ 2 23.63 19.66 60.77 42.85 20.48 34.03 54.06 17.00 58.04 41.03 L2-13B QuIP 2 13.48 16.16 N/A N/A N/A N/A N/A N/A N/A N/A Slim-LLM 2 9.98 22.62 66.54 52.09 26.37 33.83 50.06 21.40 64.74 45.00 PB-LLM 1.7 236.42 184.67 54.68 27.36 18.86 26.58 50.43 13.20 38.20 32.76		GPTQ		15.29	14.86	62.84	42.80	22.01	39.74	53.59	19.40	54.80	42.17
PB-LLM	L-30B	QuIP	2	22.30	19.33	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
PT²-LLM 1.58 7.35 13.23 70.24 64.10 32.94 44.00 68.43 25.40 69.24 53.48 FP16 16 4.88 6.73 79.05 79.42 48.38 60.03 72.22 35.20 80.55 64.98 AWQ 2 1.20e5 9.40e4 53.26 26.09 22.70 25.57 48.93 13.40 62.17 36.02 GPTQ 2 23.63 19.66 60.77 42.85 20.48 34.03 54.06 17.00 58.04 41.03 L2-13B QuIP 2 13.48 16.16 N/A N/A N/A N/A N/A N/A N/A Slim-LLM 2 9.98 22.62 66.54 52.09 26.37 33.83 50.06 21.40 64.74 45.00 PB-LLM 1.7 236.42 184.67 54.68 27.36 18.86 26.58 50.43 13.20 38.20 32.76		Slim-LLM	2	7.16	13.14	75.52	51.29	39.29	66.10	64.07	15.00	62.01	53.33
FP16 16 4.88 6.73 79.05 79.42 48.38 60.03 72.22 35.20 80.55 64.98 AWQ 2 1.20e5 9.40e4 53.26 26.09 22.70 25.57 48.93 13.40 62.17 36.02 GPTQ 2 23.63 19.66 60.77 42.85 20.48 34.03 54.06 17.00 58.04 41.03 L2-13B QuIP 2 13.48 16.16 N/A N/A N/A N/A N/A N/A N/A Slim-LLM 2 9.98 22.62 66.54 52.09 26.37 33.83 50.06 21.40 64.74 45.00 PB-LLM 1.7 236.42 184.67 54.68 27.36 18.86 26.58 50.43 13.20 38.20 32.76			1.7	23.72	25.16	63.87	48.06	23.04	35.13	60.30	17.20	62.69	44.33
AWQ 2 1.20e5 9.40e4 53.26 26.09 22.70 25.57 48.93 13.40 62.17 36.02 GPTQ 2 23.63 19.66 60.77 42.85 20.48 34.03 54.06 17.00 58.04 41.03 UL2-13B QuIP 2 13.48 16.16 N/A		PT ² -LLM	1.58	7.35	13.23	70.24	64.10	32.94	44.00	68.43	25.40	69.24	53.48
L2-13B		FP16	16	4.88	6.73	79.05	79.42	48.38	60.03	72.22	35.20	80.55	64.98
L2-13B		AWQ	2	1.20e5	9.40e4	53.26	26.09	22.70	25.57	48.93	13.40	62.17	36.02
L2-13B QuIP 2 13.48 16.16 N/A				23.63	19.66	60.77	42.85	20.48	34.03	54.06	17.00	58.04	41.03
Slim-LLM 2 9.98 22.62 66.54 52.09 26.37 33.83 50.06 21.40 64.74 45.00 PB-LLM 1.7 236.42 184.67 54.68 27.36 18.86 26.58 50.43 13.20 38.20 32.76	L2-13B				16.16		N/A	N/A		N/A			
		PB-LLM	1.7	236.42	184.67	54.68	27.36	18.86	26.58	50.43	13.20	38.20	32.76
PT ² -LLM 1.58 9.93 21.49 63.76 54.38 24.23 34.23 58.01 18.80 62.23 45.09		PT ² -LLM	1.58	9.93	21.49	63.76	54.38	24.23	34.23	58.01	18.80	62.23	45.09

G ADDITIONAL EXPERIMENTAL RESULTS

As shown in Table 2, we provide additional experimental results on other representative models. These experiments are intended to validate the generality and robustness of our method under varying model architectures and parameter scales. Unless otherwise specified, we follow the same quantization configurations and evaluation settings as in the main results.