Optimal Zero-shot Regret Minimization for Selective Classification With Out-of-Distribution Detection

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Abstract

Selective Classification with Out-of-Distribution Detection (SCOD) is a general framework that combines the detection of incorrectly classified indistribution samples and out-of-distribution samples. Previous solutions for SCOD heavily rely on the choice of Selective Classification (SC) and Out-of-Distribution (OOD) detectors selected at test time. Notably, the performance of these detectors varies across different underlying data distributions. Hence, a poor choice can affect the efficacy of the SCOD framework. On the other hand, making an informed choice is impossible without samples from both in- and out-distribution. We propose an optimal zero-shot black-box method for SCOD that aggregates off-the-shelf detectors, is based on the principle of regret minimization, and provides an improvement on the worst-case performance. We demonstrate that our method achieves performance comparable to state-of-the-art methods in several benchmarks while also shielding the user from the burden of blindly selecting the SC and OOD detectors, optimally minimizing the regret and attaining reduced rejection risk.

1 INTRODUCTION

Classification with an abstention option has become a prominent strategy to make Deep Neural Network classifiers more trustworthy. In particular, the need to identify wrong predictions arising from in-distribution (in-d) and out-distribution (out-d) data has been the subject of extensive research in recent years, both in the fields of Selective Classification (SC) [Geifman and El-Yaniv, 2017, 2019, Granese et al., 2021] and Out-of-Distribution (OOD) detection [Liang et al., 2018, Sastry and Oore, 2020, Dadalto et al., 2022, Djurisic et al., 2023]. Selective Classification with Out-of-Distribution Detection (SCOD) [Xia and Bouganis, 2022, Narasimhan et al., 2024] has recently been proposed as a general framework for the detection of misclassified samples drawn from the training in-d \mathbb{P}_{in} , and samples coming from an out-d $\mathbb{P}_{out} \neq \mathbb{P}_{in}$. Narasimhan et al. [2024] introduces a *black-box* solution for SCOD when only samples from \mathbb{P}_{in} are available. It provides a *plugin* framework that allows to combine off-the-shelf SC and OOD detection methods to achieve a Bayes-optimal rejector in the most constraining scenario.

Why do we need a principled solution based on regret minimization? Previous work places the burden on the practitioner to decide which off-the-shelf scores to choose. However, when the user does not have access to samples drawn from both \mathbb{P}_{in} and \mathbb{P}_{out} , no informed decision can be made. Indeed, the problem of binary detection has been shown to be very challenging, especially when a detector is required to perform well on multiple domains, with no side information about the underlying distributions [Lee and Barber, 2021, Fang et al., 2022, Pichler et al., 2024]. As highlighted in Li et al. [2023], worst-case risk minimization is essential for trustworthy systems, as it shields the user from the risk of picking detectors that may fail catastrophically on one or more given domains.

Thus, the questions we address in this paper are:

- **Q1** Can we make a more informed choice instead of blindly selecting a detector from off-the-shelf, achieving good SCOD performance while also reducing the worst-case rejection risk?
- **Q2** Can we accomplish the aforementioned goal with a zero-shot framework that allows us to reject samples in the wild without any additional training?

To illustrate our objective, consider Figure 1, which shows the worst-case, i.e. highest, Area Under the Risk-Coverage Curve (AUC-RC) attained by different OOD detectors when plugged in the framework of Narasimhan et al. [2024] and

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Figure 1: Worst-case performance for SCOD among 20 models, 3 in-d datasets (CIFAR-10, CIFAR-100, and ImageNet), and 18 out-d datasets. It highlights the absence of a singular superior performer in the task, exhibiting unpredictable efficacy depending on factors such as in- and out-domain scenarios and the OOD detection method applied within the SCOD framework. The proposed algorithm (blue line) strategically aggregates the off-the-shelf detectors in this example, do not require training, and mitigate catastrophic performance.

evaluated over 18 out-d domains. Clearly, not all the considered state-of-the-art (SOTA) detectors guarantee the same worst-case risk, e.g. Energy score (Energy) outperforms the others methods when the out-d domains are Gaussian or Uniform Noise [Hendrycks and Gimpel, 2017], but performs worse than the others when the out-d domains are, for instance, coming from curated datasets, such as Ninco [Bitterwolf et al., 2023], Species [Hendrycks et al., 2022], iNaturalist [Horn et al., 2017], or OpenImages [Krasin et al., 2017]. Had access to any out-d domain been granted, it would be possible to pick the most suitable method by, for instance, choosing the one that best performs on a given task. However, this is not possible in many realistic scenarios, where the only known domain is \mathbb{P}_{in} , and the only option is a black-box plugin estimator.

The principled zero-shot score we propose in this paper provides answers to the questions mentioned earlier. Our solution performs comparably to the state-of-the-art out-ofdistribution detectors. Additionally, *it consistently reduces the worst-case AUC-RC across all tasks*, as indicated by the blue line in Figure 1 and in the main results in Section 5. In contrast, all other methods are impacted by the highest rejection risk in one or more cases.

This work makes the following contributions:

- 1. We identify and address a limitation in the existing SOTA black-box framework for SCOD. Without samples from the out-d, practitioners cannot make informed decisions on which off-the-shelf detection method to use (see Figure 1).
- 2. We provide a theoretical framework and derive a prin-

cipled method to combine off-the-shelf OOD detectors in a zero-shot manner, meaning there is no need for any OOD data. Our approach is tailored to each input sample (see Section 3).

3. We compare the proposed method against a wide range of SOTA OOD detection methods on several benchmarks and models within the framework of Narasimhan et al. [2024]. The attained results are consistently comparable with the best-performing methods, while also reducing the worst-case rejection risk, which is crucial for the reliability of AI systems (see Section 5).

2 BACKGROUND

We consider the standard multi-class classification task, where, given a feature space $\mathcal{X} \in \mathbb{R}^d$, and a label space $\mathcal{Y} \doteq \{0, \ldots, C-1\} \subset \mathbb{N}$, a classifier is a function $f : \mathcal{X} \to \mathcal{Y}$ trained on a set of samples $S_n \doteq \{(\boldsymbol{x}_i, y_i)\}_{i=[n]}$ consisting of n i.i.d. training samples drawn according to the in-d \mathbb{P}_{in} defined over the support $\mathcal{X} \times \mathcal{Y}$. In the usual setup, the training and test distribution coincide, i.e., $\mathbb{P}_{te} = \mathbb{P}_{in}$. Then, typically, for $\boldsymbol{x} \in \mathcal{X}$ and $\boldsymbol{y} \in \mathcal{Y}$, $f(\boldsymbol{x}) = \arg \max_{\boldsymbol{y} \in \mathcal{Y}} h_{\boldsymbol{y}}(\boldsymbol{x}, \boldsymbol{\theta})$, where $h(\boldsymbol{x}, \boldsymbol{\theta}) : \mathcal{X} \to \mathbb{R}^C$, $h_{\boldsymbol{y}}(\cdot, \boldsymbol{\theta})$ is the \boldsymbol{y} -th component of $h(\cdot, \boldsymbol{\theta})$, and $\boldsymbol{\theta}$ is the vector of parameters that is fit to the training data by optimizing a loss function over S_n using an iterative algorithm such as Stochastic Gradient Descent (SGD).

Though this is an interesting theoretical setup, in practice, the ability to abstain from classifying a sample when the prediction confidence is expected to be low is a desideratum. This helps reduce the number of misclassifications for samples drawn from \mathbb{P}_{te} that may be close to the learned decision boundary. Moreover, it helps dealing with situations in which $\mathbb{P}_{te} \neq \mathbb{P}_{in}$, e.g. $\mathbb{P}_{te} \doteq \pi_{in} \cdot \mathbb{P}_{in} + (1 - \pi_{in}) \cdot \mathbb{P}_{out}$ for a certain out-d \mathbb{P}_{out} , and a mixture parameter $\pi_{in} \in [0, 1]$.

SC is the problem of abstaining from classifying a sample, typically drawn from \mathbb{P}_{in} , when the classifier is not confident enough about its prediction Geifman and El-Yaniv [2017, 2019], Corbière et al. [2019], Liu et al. [2019], Huang et al. [2020], Granese et al. [2021]. The simplest way to model this goal is to consider a rejector $r: \mathcal{X} \to \{0,1\}$, which is a binary function that outputs 1 when the prediction on $x \in \mathcal{X}$ is rejected, and 0 otherwise. In this case, and for a given rejection budget $b_{\rm rei} \in (0,1)$, the optimal solution to the SC problem is $\min_{h,r} \mathbb{P}_{in}(y \neq h(\boldsymbol{x}), r(\boldsymbol{x}) = 0) : \mathbb{P}_{in}(r(\boldsymbol{x}) = 1) \leq b_{rej},$ where $\mathbb{P}_{in}(y \neq h(x), r(x) = 0)$ is the probability of accepting a prediction that is incorrect, and $\mathbb{P}_{in}(r(\boldsymbol{x}) = 1)$ is the probability of rejecting a prediction. Most of the SC frameworks in the literature consider the rejector to be a function of $h(\cdot, \boldsymbol{\theta})$, e.g. its output, and can be learned jointly with the classifier by adapting the training loss function Corbière et al. [2019], Huang et al. [2020]. In line with Narasimhan et al. [2024], we consider the solution in Geifman and El-Yaniv [2017], where the decision is made by comparing the Max Soft Probability (MSP) of a pre-trained model $h(\cdot, \theta)$ to a threshold.

OOD detection is the problem of detecting samples drawn from a distribution \mathbb{P}_{out} that is different from the training distribution \mathbb{P}_{in} , for instance when $\mathbb{P}_{te} \doteq \pi_{in} \cdot \mathbb{P}_{in} + (1 - \pi_{in}) \cdot \mathbb{P}_{out}$. In this case, the optimal solution to the OOD problem is given by $\min_r \mathbb{P}_{te}(r(\boldsymbol{x}) = 0) : \mathbb{P}_{in}(r(\boldsymbol{x}) = 1) \leq b_{fpr}$, where $b_{fpr} \in (0, 1)$ is the False Positive Rate (FPR) budget, i.e., the fraction of in-d samples incorrectly predicted as out-d. In line with the plugin framework, we consider the most popular SOTA solutions for this problem, i.e. methods that consider the rejector to be a function of the pre-trained classifier, such as Liang et al. [2018], Liu et al. [2020], Feng et al. [2022], among others.

SCOD is the framework that combines SC and OOD. According to Narasimhan et al. [2024], the optimal solution to the SCOD problem is given by

$$\min_{h,r} \left[(1 - c_{\mathrm{fn}}) \cdot \mathbb{P}_{\mathrm{in}}(y \neq h(\boldsymbol{x}), r(\boldsymbol{x}) = 0) + c_{\mathrm{fn}} \cdot \mathbb{P}_{\mathrm{out}}(r(\boldsymbol{x}) = 0) : \mathbb{P}_{\mathrm{te}}(r(\boldsymbol{x}) = 1) \leq b_{\mathrm{rej}} \right], \quad (1)$$

where $c_{\text{fn}} \in [0, 1]$ is a user-specified cost of not rejecting an out-d sample.

A way to deal with it would be to perform hypothesis testing on the true distributions by defining s_{sc}^* and s_{ood}^* where

$$s_{\rm sc}^*(\boldsymbol{x}) \doteq \max_{\boldsymbol{y} \in [C]} \mathbb{P}_{\rm in}(\boldsymbol{y} \mid \boldsymbol{x}), \ s_{\rm ood}^*(\boldsymbol{x}) \doteq \frac{\mathbb{P}_{\rm in}(\boldsymbol{x})}{\mathbb{P}_{\rm out}(\boldsymbol{x})}, \quad (2)$$

and comparing them with a threshold. Clearly, the two quantities above require full knowledge of \mathbb{P}_{in} and \mathbb{P}_{out} . The function *h* and *r* could be optimized for Equation (1) if we had samples from \mathbb{P}_{in} and \mathbb{P}_{out} , or a way to estimate the underlying mixture \mathbb{P}_{te} . However, in this work, and in line with the black-box solution presented in Narasimhan et al. [2024] (cf. Equation (3)), we do not assume access to out-d samples from \mathbb{P}_{out} , and we consider the classifier to be a pre-trained one, and we seek to leverage existing selective classification and OOD detection techniques to estimate the quantities in Equation (2).

Plugin Estimator. Given $s_{sc}(\cdot)$ and $s_{ood}(\cdot)$ scores as an estimate of $s_{sc}^*(\cdot)$, $s_{ood}^*(\cdot)$ respectively, derived from one SC method, and one OOD method among those listed in Section 7, the black-box plugin estimator takes the following form:

$$r_{\rm BB}(\boldsymbol{x}) = \mathbb{1}[((1 - c_{\rm in} - c_{\rm out}) \cdot s_{\rm sc}(\boldsymbol{x}) + c_{\rm out} \cdot \beta(s_{\rm ood}(\boldsymbol{x})) < t_{\rm BB})], \qquad (3)$$

where $c_{\rm in}$, $c_{\rm out} \in [0, 1]$, $\beta(s_{\rm ood}(\cdot)) = -1/s_{\rm ood}(\cdot)$, $t_{\rm BB} = 1-2 \cdot c_{\rm in} - c_{\rm out}$, and Equation (3) coincides with Narasimhan et al. [2024, Lemma 3.1].

3 ZERO-SHOT SCOD WITH MINIMIZED REGRET

The SOTA black-box plugin method in Narasimhan et al. [2024] presents an optimal way to combine SC and OOD detection, using off-the-shelf methods to obtain the needed scores.

Crucially, a limiting aspect is that it does not provide a way to pick which detectors to use. In this work, we propose a way to aggregate multiple SOTA OOD detectors, according to the information theoretical notion of *regret minimization* Barron et al. [1998]. Notably, we propose a framework to combine multiple OOD detection scores into one, in a zeroshot way, without training a new detector.

As we shall see,

- Our solution achieves performance comparable to the best OOD detector in each considered task;
- Most importantly, it allows the user to aggregate multiple detectors from the literature, rather than choose one, which may have varying performance when evaluated on different domains.

3.1 PROBABILISTIC DETECTION SCORE (PDS): FROM A DISTANCE-BASED TO A CONFIDENCE-BASED OOD DETECTION

As defined in Equation (2), OOD detection scores can be summarized as a scalar function that tries

to estimate the quantity $s_{\text{ood}}(\boldsymbol{x}) : \mathcal{X} \to \mathbb{R}^+$ such that $s_{\text{ood}}(\boldsymbol{x}) \approx (\mathbb{P}_{\text{in}}/\mathbb{P}_{\text{out}})(\boldsymbol{x})$, also referred to as likelihood ratio.

Low values of *s* indicate that the example is likely to be sampled from an out-d, while high values indicate otherwise. In the OOD literature, this formulation is also referred to as *confidence-based* scores. On the other hand, a popular interpretation of the OOD detection problem follows a *distance-based* setting, where higher values of the scores would indicate that the sample is far from the in-d, making it incompatible with confidence-based detection frameworks.

To allow any score function to be correctly plugged in our framework, that we shall present in Section 3, we propose a Probabilistic Detection Score (PDS) transformation to ground the scores into a common range and same distribution for in-d samples. This transformation is based on the empirical estimate of the Cumulative Distribution Function (CDF) which converges almost surely to the true CDF. As a result, we define PDS as being the function

$$\bar{s}_{\text{ood}} : \mathcal{X} \to [0, 1],$$
 (4)

which unifies confidence-based and distance-based scores without loss of detection performance.

Algorithm 1 Probabilistic Detection Score (PDS) Transformation

Input: sorted set (ascending order) of confidence-based soft scores of m in-d samples $S_m = \{\delta : s_{\text{ood}}(\boldsymbol{x}_1) = \delta_1 \leq \cdots \leq \delta_m = s_{\text{ood}}(\boldsymbol{x}_m)\}$ and the score to be transformed $s_{\text{ood}}(\boldsymbol{x})$.

// new lower and upper bounds, respectively $\delta_0 \leftarrow \delta_1/m, \quad \delta_{m+1} \leftarrow \delta_m \cdot m$

// concatenate bounds to original scores vector $S \leftarrow \delta_0 \oplus S_m \oplus \delta_{m+1}$ $C \leftarrow [1/(m+2) \ 2/(m+2) \ \dots \ (m+2)/(m+2)]$ // lower and upper query indexes $i \leftarrow \arg\min_{k \in [0...m]} |s_{\text{ood}}(\boldsymbol{x}) - S_k|, \quad j \leftarrow i+1$ // interpolation $\bar{s}_{\text{ood}}(\boldsymbol{x}) \leftarrow C_i + (s_{\text{ood}}(\boldsymbol{x}) - S_i) \frac{C_j - C_i}{S_j - S_i}$ **Return:** $\bar{s}_{\text{ood}}(\boldsymbol{x})$

Algorithm 1 is an implementation of a quantile transformation that shows how to obtain the PDS for a confidencebased score. For a distance-based score, it changes slightly: first, the scores are flipped around the zero-value (i.e., multiplied by -1) to align with confidence-based scores; and finally, the heuristics for the lower and upper bounds changes: the division and multiplication operations in Algorithm 1 are swapped as we are dealing with strict negative values this time (i.e., $\delta_0 = \delta_1 \cdot m$ and $\delta_{m+1} = \delta_m/m$). After this pre-processing, Algorithm 1 can be applied as is.

The output of the PDS algorithm, transforms the s_{ood} scores into the corresponding value on the CDF curve. Intuitively, the empirical CDF, estimated through the sorted scores of samples from \mathbb{P}_{in} , maps a sample to its probability of being in-d. Indeed, considering Figure 2b, a sample will have a matching high \bar{s}_{ood} score if its s_{ood} score is on the in-d side of Figure 2a, i.e. if it is likely in-d, and far from the error area where the histograms of in-d and out-d overlap.

Using this interpretation, the \bar{s}_{ood} score can be regarded as a measure of the likelihood of being in-d, and used to define a detection method based on a distribution $\mathbb{Q}_{Z|x}$ where Z is a binary random variable indicating whether the sample x is likely to be in-d if it takes the value 0 or out-d if it takes the value 1. Usually, a *Hard Rejector* is derived by comparing s to a real-valued hyperparameter γ , i.e., $r'(x) = \mathbb{1}[s(x) \leq \gamma]$. In our case, the PDS can be compared to a confidence value $\alpha \in [0, 1]$ that will indicate the desired False Negative Rate (FNR), or

$$r(\boldsymbol{x}) = \mathbb{1}[\bar{s}_{\text{ood}}(\boldsymbol{x}) \le \alpha].$$
(5)

Figure 2 showcases the PDS transformation for a confidencebased score (energy) and a distance-based score (KNN). We can observe the histograms of s_{ood} in Figure 2a and \bar{s}_{ood} in Figure 2b, which maps any in-distribution to a uniform distribution in the unit range. OOD samples are mapped to low values due to the PDS transformation. The detection capacity is untouched as observed in Figure 2c, where the ROC curves of the PDS do not deviate from the ROC curve of the raw soft-score.

We plot the quantization error with 90% confidence bounds, showing that, with more than 10 in-distribution samples the absolute error between the PDS ROC and the original ROC is virtually zero. Furthermore, the study presented in Table 1 reports the average AURC for the proposed method across the OOD datasets considered in Section 4, using different values of m in Algorithm 1, specifically $\{5, 10, 20, 1000\}$: the values fluctuate slightly, the variance across the four choices of m is small, supporting the analysis of the mparameter shown in Figure 2.

Thus, through PDS, we can represent any score within any range into a score that resembles a distribution, requires few data points, is inexpensive to compute, and will allow the minimum regret principle introduced in Section 3.2 to aggregate multiple scores for the first time in OOD detection, enabling a more reliable SCOD setup. As a matter of fact, the detector provider can take care of this transformation, so that no data is needed to deploy our framework.

| Model (in-d dataset) | Valu | e of the | paramet | er m | Variance |
|--------------------------|-------|----------|---------|-------|----------|
| | 5 | 10 | 20 | 1000 | |
| VGG-16 (Cifar-10) | 0.219 | 0.227 | 0.224 | 0.227 | 1.425E-5 |
| DenseNet-121 (Cifar-100) | 0.321 | 0.320 | 0.322 | 0.326 | 6.917E-6 |
| ResNet-101 (ImageNet) | 0.305 | 0.301 | 0.301 | 0.305 | 5.333E-6 |

Table 1: Ablation study of the parameter m in terms of average AURC.

3.2 Minimum Regret Probabilistic Score Aggregation (MRPSA)

Let us consider a model h as defined above and a score \bar{s}_{ood} as described in Section 3.1, representing a probabilistic score. Usually, in practice, given a sample x, a score is not only a function of the sample but also the underlying classifier model, i.e., we have $\bar{s}_{ood}(x, h)$. Hence, the corresponding probability distribution $\mathbb{Q}_{Z|x,h}$ also depends on it. For the sake of simplicity, and assuming that a given pretrained classifier is fixed, we will omit the dependence on the model in the following, using, without loss of generality, the notation $\bar{s}_{ood}(x)$ and $\mathbb{Q}_{Z|x}$.

Now, consider a set of K soft-rejectors as in Section 3.1 and the set of corresponding distributions $Q \doteq \{\mathbb{Q}_{Z|X}^k\}_{k=1}^K$, and let us assume that each rejector r_k is effective against at least one benchmark, i.e., it can successfully detect samples from \mathbb{P}_{in} and \mathbb{P}_{out}^k with high confidence at least for a given setting of \mathbb{P}_{in} and \mathbb{P}_{out}^k . Notice that this is a mild assumption since all the published literature showcases a set of benchmarks where the proposed detectors are SOTA or close to it. Fixed an input sample x, we would like to formally define $\mathbb{Q}_{Z|x}^{\star}$ that performs well simultaneously over all the possible |K| detection problem settings. This can be framed as the following problem:

$$\mathcal{L}(\mathcal{Q}, \boldsymbol{x}) = \min_{\mathbb{Q}_{Z|\boldsymbol{x}}} \max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{k}} \left[-\log \mathbb{Q}_{Z|\boldsymbol{x}} \right], \qquad (6)$$

which requires solving (6) for Q and for each given input sample x. It is important to note that the minimization is performed over all distributions $\mathbb{Q}_{Z|x}$, including elements that are not part of the set Q. As it turns out, Equation (6) is computationally intractable. In Appendix A.1.1, we show how to obtain the following upper bound for the maximization problem in Equation (6). For any arbitrary choice of $\mathbb{Q}_{Z|x}$, it holds that:

$$\max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{k}} \left[-\log \mathbb{Q}_{Z|\boldsymbol{x}} \right] \leq \underbrace{\max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{k}} \left[-\log \mathbb{Q}_{Z|\boldsymbol{x}}^{k} \right]}_{=\text{constant w.r.t. } \mathbb{Q}_{Z|\boldsymbol{x}}} + \underbrace{\max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{k}} \left[\log \left(\frac{\mathbb{Q}_{Z|\boldsymbol{x}}^{k}}{\mathbb{Q}_{Z|\boldsymbol{x}}} \right) \right]}_{=\text{constant } \mathbf{y}.r.t. } \mathbb{Q}_{Z|\boldsymbol{x}}$$
(7)

=average worst-case regret Barron et al. [1998]

According to the proof in Appendix A.1.2, this upper bound allows us to optimize the objective in Equation (6) by defining the surrogate objective in Equation (8).

$$\tilde{\mathcal{L}}(\mathcal{Q}, \boldsymbol{x}) = \min_{\mathbb{Q}_{Z|\boldsymbol{x}}} \max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{k}} \left[\log \left(\frac{\mathbb{Q}_{Z|\boldsymbol{x}}^{k}}{\mathbb{Q}_{Z|\boldsymbol{x}}} \right) \right] = \min_{\mathbb{Q}_{Z|\boldsymbol{x}}} \max_{P_{\Omega}} \mathbb{E}_{\Omega} \left[D_{\mathrm{KL}} \left(\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)} \| \mathbb{Q}_{Z|\boldsymbol{x}} \right) \right], \quad (8)$$

where the min is taken over all the possible distributions $\mathbb{Q}_{Z|x}$; and Ω is a discrete random variable with P_{Ω} denoting a generic probability distribution whose probabilities are $(\omega_1, \ldots, \omega_{|\mathcal{K}|})$, i.e., $P_{\Omega}(k) = \omega_k$; and $D_{\mathrm{KL}}(\cdot \| \cdot)$ is the Kullback–Leibler divergence (KL divergence), representing the expected value of regret of $\mathbb{Q}_{Z|U}$ w.r.t. the worst-case distribution in Q. Finally, according to the proof in Appendix A.1.3, and utilizing the convex nature of the KL divergence, the solution to Equation (8) provides the optimal distribution P_{Ω}^{\star} , i.e. the collection of weights $\{\omega_k^{\star}\}$, which leads to our soft-detector [Barron et al., 1998, Granese et al., 2024] $\mathbb{Q}_{Z|x}^{\star}$:

$$\mathbb{Q}_{Z|\boldsymbol{x}}^{\star} = \sum_{k \in \mathcal{K}} \omega_k^{\star} \cdot \mathbb{Q}_{Z|\boldsymbol{x}}^k, \ P_{\Omega}^{\star} = \arg \max_{\{\omega_k\}} I_{\boldsymbol{x}}(\Omega; Z).$$
(9)

In Equation (9), $I_{\boldsymbol{x}}(\cdot; \cdot)$ denotes the Shannon mutual information between the random variable Ω , distributed according to $\{\omega_k\}$, and the binary soft-prediction variable Z, distributed according to $\mathbb{Q}_{Z|\boldsymbol{x}}^k$ and conditioned on the particular test example \boldsymbol{x} . The optimal combination of weights can be estimated by means of the Blahut-Arimoto Arimoto [1972] iterative algorithm that maximizes the mutual information in (9), parametrized by the weights $\{\omega_k\}$, with respect to the weights themselves. In line with Section 3.1, we can extract the score $\bar{s}_{\text{ood}}(\boldsymbol{x})$ from $\mathbb{Q}_{Z|\boldsymbol{x}}^*$, i.e.,

$$r(\boldsymbol{x}) = \mathbb{1}\left[\mathbb{Q}_{Z|X}^{\star}(0|\boldsymbol{x}) < \alpha\right], \qquad (10)$$

where Z = 0 indicates the event of detecting x as an in-d sample and use it in the black-box SCOD plugin framework of Narasimhan et al. [2024].

4 EXPERIMENTAL SETUP

Baselines. We consider the following post-hoc detection methods as off-the-shelf baselines: MSP [Hendrycks and



Figure 2: MRPSA allows to move from confidence-based and distance-based soft detection scores to an effective probabilistic detection score with good convergence rate, using a relatively low value for the parameter m in Algorithm 1.

Gimpel, 2017], Energy [Liu et al., 2020], Mahalanobis (Maha) [Lee et al., 2018], Igeood [Dadalto et al., 2022], MaxCosine (MCos) [Techapanurak et al., 2020], ReAct [Sun et al., 2021], ODIN [Liang et al., 2018], Maximum logits (MaxL) [Hendrycks et al., 2022], KL-divergence matching (KL-M) [Hendrycks et al., 2022], Doctor [Granese et al., 2021], Relative Mahalanobis distance (RMaha) [Fort et al., 2021], and KNN [Sun et al., 2022]. Following popular OOD detection settings Fort et al. [2021], we followed the hyperparameter selection procedure suggested in the original papers, we used only the penultimate layer or logits outputs, and they are implemented so that they only have access to in-d data. In so doing, we extend the analysis reported in Figure 1 by considering a larger number of OOD detectors for SCOD, that we aggregate through MRPSA.

Models. We consider both pre-trained models and models trained from scratch with the following architectures: Residual Convolutional Neural Networks (ResNet) [He et al., 2016], Vision Transformers (ViT) [Dosovitskiy et al., 2021], MobileNet [Howard et al., 2017], DenseNet [Huang et al., 2017], and VGG [Simonyan and Zisserman, 2015]. We *do not* include any OOD data during training.

Datasets. The CIFAR-10 (C-10) dataset [Krizhevsky et al., 2009] comprises 32x32 pixel natural images categorized into 10 distinct classes, such as airplanes, ships, birds, and more. Similarly, the CIFAR-100 (C-100) dataset consists of natural images akin to those in CIFAR-10 but spanning 100 categories non-overlapping with C-10. Both datasets feature a training set containing 50,000 images and a test set of 10,000 images. SVHN [Netzer et al., 2011], Tiny-ImageNet (TIN) [Le and Yang, 2015] and LSUN (LS) [Yu et al., 2015] in its (c)roped and (r)seized versions, iSUN [Xu et al., 2015], Textures (Tex.) [Cimpoi et al., 2014], Places365 (Places) [Zhou et al., 2017], Gaussian noise (Gauss), and Uniform noise (Unif.) are used as OOD datasets. The ImageNet [Deng et al., 2009] dataset encompasses ap-

proximately 1.28 million training examples and 50,000 labeled test instances from 1000 classes. For this large-scale benchmark, in addition to Textures and Places365 (Places), Species [Hendrycks et al., 2022], OpenImage-O (OpenIm) [Wang et al., 2022], iNaturalist (iNat) [Huang and Li, 2021], Sun [Huang and Li, 2021], Semantic Shift Benchmark (SSB) [Vaze et al., 2022], and NINCO [Bitterwolf et al., 2023] are considered.

Evaluation Metrics. Following Narasimhan et al. [2024], we define the evaluation dataset as $S_{\rm all} \doteq S_{\rm in} \cup S_{\rm out}$, a combination of in-d and out-d sets such that $\hat{\pi}_{\rm in} = |S_{\rm in}|/(|S_{\rm in}| + |S_{\rm out}|) \approx \pi_{\rm in}$. From this set, we can compute a few key metrics, such as the empirical coverage, risk, and the area under the risk-coverage curve (AUC-RC or AURC), summarizing the SCOD rejector performance. We also plotted these curves for fine-grained analysis and computed the AUROC for the SCOD problem. We fix $\pi_{\rm in} = 0.5$ and $c_{\rm fn} = 0.75$ for all the experiments. All the results are averaged over 10 random seeds.

Empirical Coverage. The empirical coverage counts how many samples are not rejected, i.e.,

$$\hat{\phi}(r) \doteq \frac{1}{|S_{\text{all}}|} \sum_{x \in S_{\text{all}}} \mathbb{1}[r(x) = 0] \approx 1 - b_{\text{rej}}.$$
 (11)

Empirical SCOD Risk. The empirical SCOD risk, or *joint* risk as in Narasimhan et al. [2024], measures the rate of mistakes of the rejector weighted by $c_{\rm fn}$ on in-d and out-d data. It counts how many misclassified samples are accepted and how many OOD samples are accepted compared to the total amount of accepted samples when a rejector is fixed

Table 2: Comparative analysis of AURC in the black-box SCOD framework between 12 existing OOD detection methods and ours (combining the other 12 methods) for three different models and domains. Results are sorted in descending order by average.

| | | C-100 | SVHN | Text. | Places | Unif. | Avg |
|------|---------|-------|-------|-------|--------|--------|-------|
| | ReAct | 0.395 | 0.357 | 0.417 | 0.314 | 0.259 | 0.348 |
| | ODIN | 0.294 | 0.248 | 0.248 | 0.287 | 0.181 | 0.252 |
| | MaxL | 0.294 | 0.248 | 0.248 | 0.287 | 0.180 | 0.251 |
| (0) | Energy | 0.294 | 0.249 | 0.248 | 0.286 | 0.178 | 0.251 |
| 4 | Igeood | 0.286 | 0.230 | 0.256 | 0.294 | 0.180 | 0.249 |
| FA | KL M | 0.280 | 0.228 | 0.239 | 0.285 | 0.185 | 0.243 |
| G | MSP | 0.272 | 0.221 | 0.241 | 0.276 | 0.182 | 0.239 |
| 16 | Doctor | 0.272 | 0.221 | 0.242 | 0.275 | 0.181 | 0.238 |
| 9 | RelMaha | 0.274 | 0.224 | 0.241 | 0.253 | 0.177 | 0.234 |
| Ŋ | Ours | 0.253 | 0.219 | 0.241 | 0.237 | 0.185 | 0.227 |
| • | Maha | 0.244 | 0.215 | 0.219 | 0.241 | 0.188 | 0.222 |
| | MCos | 0.244 | 0.209 | 0.218 | 0.238 | 0.182 | 0.218 |
| | KNN | 0.230 | 0.205 | 0.206 | 0.224 | 0.179 | 0.208 |
| | | C-10 | SVHN | Text. | Places | Unif. | Avg |
| | ReAct | 0.514 | 0.461 | 0.417 | 0.427 | 0.353 | 0.435 |
| | RMaha | 0.367 | 0.334 | 0.465 | 0.364 | 0.337 | 0.373 |
| 0 | Maha | 0.430 | 0.361 | 0.319 | 0.366 | 0.294 | 0.354 |
| | KL M | 0.366 | 0.326 | 0.363 | 0.328 | 0.308 | 0.338 |
| Ϋ́E | Energy | 0.355 | 0.322 | 0.358 | 0.323 | 0.300 | 0.332 |
| G | MaxL | 0.353 | 0.320 | 0.358 | 0.324 | 0.301 | 0.331 |
| - | ODIN | 0.353 | 0.320 | 0.357 | 0.323 | 0.300 | 0.331 |
| -12 | Doctor | 0.342 | 0.322 | 0.351 | 0.322 | 0.309 | 0.329 |
| Vet | MSP | 0.342 | 0.323 | 0.349 | 0.321 | 0.309 | 0.329 |
| sel | Ours | 0.373 | 0.318 | 0.331 | 0.322 | 0.288 | 0.326 |
| Cen | Igeood | 0.346 | 0.315 | 0.350 | 0.318 | 0.294 | 0.325 |
| Ц | KNN | 0.374 | 0.313 | 0.305 | 0.318 | 0.276 | 0.317 |
| | MCos | 0.372 | 0.310 | 0.297 | 0.320 | 0.272 | 0.315 |
| | | NINCO | iNat | Text. | Places | OpenIm | Avg |
| | Maha | 0.390 | 0.341 | 0.310 | 0.373 | 0.346 | 0.352 |
| | Energy | 0.343 | 0.310 | 0.320 | 0.318 | 0.318 | 0.322 |
| ŝ | ODIN | 0.341 | 0.304 | 0.319 | 0.315 | 0.314 | 0.319 |
| Nei | KNN | 0.338 | 0.312 | 0.293 | 0.324 | 0.321 | 0.318 |
| ige | ReAct | 0.352 | 0.304 | 0.310 | 0.306 | 0.314 | 0.317 |
| lm | KL M | 0.339 | 0.315 | 0.304 | 0.295 | 0.317 | 0.314 |
| 10 | MaxL | 0.334 | 0.301 | 0.304 | 0.304 | 0.303 | 0.309 |
| -10 | RMaha | 0.316 | 0.289 | 0.303 | 0.314 | 0.311 | 0.307 |
| let- | Ours | 0.331 | 0.292 | 0.295 | 0.303 | 0.303 | 0.305 |
| esl | Doctor | 0.312 | 0.300 | 0.310 | 0.296 | 0.299 | 0.303 |
| Ч | MSP | 0.306 | 0.281 | 0.300 | 0.291 | 0.299 | 0.296 |
| | MCos | 0.324 | 0.281 | 0.276 | 0.296 | 0.295 | 0.294 |
| | Igeood | 0.312 | 0.286 | 0.286 | 0.282 | 0.287 | 0.291 |

according to a coverage budget. Formally,

$$\hat{R}(f,r) \doteq \frac{(1-c_{\mathrm{fn}})}{A} \underbrace{\sum_{(x,y)\in S_{\mathrm{in}}} \mathbb{1}[f(x) \neq y, r(x) = 0]}_{\text{\# of accepted misclassifications}} + \underbrace{\frac{c_{\mathrm{fn}}}{A} \sum_{\substack{x\in S_{\mathrm{out}}\\ \text{\# of accepted OOD samples}}} \mathbb{1}[r(x) = 0], \qquad (12)$$

where $A = \sum_{\boldsymbol{x} \in S_{\text{all}}} \mathbb{1}[r(\boldsymbol{x}) = 0]$ is the total number of accepted samples.

AUC-RC. The area under the risk-coverage curve is computed using the trapezoidal integration rule by discretizing

the space of thresholds to compute points of the SCOD risk curve. We considered 10% of the testing points uniformly sampled to be the discretizing thresholds to compute the integral, which accelerates the computations considerably. We report the average results over 10 random seeds, where we observed a standard deviation of less than 10^{-3} .

5 RESULTS AND ANALYSIS

Table 2 showcases the detection performance of the baselines and our method on the SCOD benchmark in terms of AURC. We observe that the proposed solution falls within the top 5 best detection methods on average, but most importantly, it keeps a low distance compared to the best performer for the given task. For CIFAR-10, on average, the worst method degrades performance by 67%, while ours degrades best performance by only 9%. For CIFAR-100, the worst method degrades performance by 38%; in contrast, we are merely 3.5% below the best performer. Finally, for ImageNet, the worst method degrades performance by 21%, while we are just 4.8% below the best method. As a result, we reduced the worst case risk by 35%, 25%, and 13% on these three benchmarks, respectively. In addition, we compared our method to baseline aggregation methods in Appendix A.4.

Figure 3 shows the SCOD **risk-coverage curves** for a few tasks on the benchmark. As desired, the proposed method never attains the worst performance, and we show empirically that the performance is much closer to the best method on the specific benchmark than the worst one, confirming the results obtained in Table 2. On ImageNet, results seem more uniform across methods, at least for the benchmark displayed in Figure 3. Extended results are relegated to the Appendix A.6, where you can find all the experimental points, including AURC and AUROC results, used to analyze the results obtained in this paper, which comprises over 20 trained models and further OOD datasets.

We analyzed the **execution time** in Equation (9), as a function of the number of detectors. Notably, the optimization algorithms can be optimized to run in parallel on a GPU, showing no outstanding overhead (cf. Figure 4 in Appendix A.3) with the code available in Listing 1.

Limitations and domain shift scenario. Although the approach introduced in this work guarantees minimal regret and achieves consistent reduction of the worst-case risk across several domains, it is not free from the risk that none of the aggregated detectors is effective against a new given OOD domain. While typically the "robustness to distribution shifts" of OOD detectors is empirically assessed by testing on various benchmarks, *our approach offers the opportunity to establish a formal upper bound on error detection*.

Owing to the probabilistic nature introduced by the PDS framework, we can utilize Ben-David et al. [2010] to obtain



Figure 3: Risk-coverage curves for the SCOD black-box plugin framework for our method and popular OOD detection baselines.

an error bound based on the statistical divergence between the domains where our detector performs well and any new domain. For detailed insights, refer to the proof provided in Appendix A.2. While this might be regarded as a limitation, indicating that no OOD detector can be universally effective across all possible domains Zhang et al. [2021], Fang et al. [2022], it points out that comparing detectors on standard benchmarks often provides a false sense of security.

6 **DISCUSSION**

In Section 3, we introduce a theoretical framework demonstrating that it is possible to construct a detector that minimizes regret across all potential detectors contained in the set Q.

To recall, in information theory, the concept of minimized regret addresses the challenge of designing a detection method from a set of available options to reduce the risk (i.e., detection error) associated with preemptively choosing a single detector, as is common practice. This approach mitigates the worst-case scenario that arises when selecting a single detector for diverse OOD detection tasks (cf. Figure 1). This key advantage sets our method apart from existing state-ofthe-art black-box SCOD plugin methods (cf. Narasimhan et al. [2024]).

We evaluate the proposed framework across a wide range of benchmark datasets (see Sections 4 and 5, and Appendix A.6). While it consistently performs close to the best detector in most cases, every other plugged-in detection method—except ours—inevitably encounters at least one instance where it reaches worst-case detection performance. This finding is supported by the results in Table 2 in Section 4 and Tables 5 to 8 in Appendix A.6.

Additionally, in Appendix A.4, we compare the proposed aggregation method, with less nuanced ones, such as majority voting, and assigning the same weight to all the detectors of the scores. On average, when multiple OOD datasets are considered, our method outperforms these baselines up to two percentage points (cf. right-most colums in Tables 3 and 4), while retaining the theoretical guarantees of minimal regret.

Furthermore, we provide a short analysis of the interpretability features of our method in Appendix A.5, showing in Figure 5 how the scores it assigns differ from those assigned by less nuanced solutions, and how they reflect the nature of the underlying data and the considered detectors.

7 RELATED WORKS

In this section we position our work within the broader context of Selective Classification, Out-of-Distribution detection, and the intersection of these two fields, i.e., Selective Classification with Out-of-Distribution Detection.

7.1 SELECTIVE CLASSIFICATION

A large body of work emphasizes the importance of fitting auxiliary parameters to directly estimate a detection score, aligning with the "learning to reject" paradigm [Chow, 1957, 1970, Geifman and El-Yaniv, 2017, Corbière et al., 2019, Liu et al., 2019, Huang et al., 2020]. Zhu et al. [2023] analyzes how models respond to outliers, aiming to assess the effectiveness of these heuristics in enhancing misclassification performance. In the mathematical framework proposed by Granese et al. [2021], a simple detection method based on the estimated probability of error is introduced.

The investigation by Zhu et al. [2022a] shows that calibration methods often prove counterproductive for failure prediction, offering valuable insights into the underlying reasons. Cen et al. [2023] explores the impact of training settings on misclassification detection performance. Other contributions in this area encompass uncertainty estimation through Bayesian Neural Networks [Gal and Ghahramani, 2016, Lakshminarayanan et al., 2017] and conformal predictions [Gibbs and Candes, 2021]. Zhang et al. [2022] relies on the adaptation to augmented data produced at test time.

7.2 OUT-OF-DISTRIBUTION DETECTION

The taxonomy of post-hoc OOD detection methods delineates three main categories: *confidence-based*, *distance-based*, and *mixed distance-confidence* techniques. Confidence-based methods [Hein et al., 2019, Hendrycks and Gimpel, 2017, Liang et al., 2018, Hsu et al., 2020, Liu et al., 2020, Hendrycks et al., 2022, Sun and Li, 2022], rely on logits or softmax outputs of neural networks. Distancebased methods [Sun et al., 2021, Huang et al., 2021, Zhu et al., 2022b, Colombo et al., 2022, Dong et al., 2021, Dadalto et al., 2022, Song et al., 2022, Lin et al., 2021, Djurisic et al., 2023, Lee et al., 2018, Fort et al., 2021, Sun et al., 2022, Du et al., 2022a, Ming et al., 2023] focus on latent representations by measuring dissimilarities between input samples and training prototypes.

Mixed distance-confidence techniques [Wang et al., 2022, Dadalto et al., 2024, Wu et al., 2023] combine information from both outputs and latent representations. Learning with outlier exposure [Hendrycks et al., 2019, Du et al., 2022b] incorporates outlier samples to regularize shape decision boundaries to be outlier-aware. Benchmarks [Zhang et al., 2023] underscore the absence of a singularly superior method, highlighting the complexity and challenges inherent to OOD detection. The concurrent work [Fan et al., 2024] relies on the idea that an online detector can be trained at test time batches using the linear separability between scores for in-distribution and out-of-distribution data points.

7.3 SELECTIVE CLASSIFICATION WITH OUT-OF-DISTRIBUTION DETECTION

Narasimhan et al. [2024], Katz-Samuels et al. [2022], Xia and Bouganis [2022], simultaneously identifying misclassified samples and samples from outside the training distribution. Xia and Bouganis [2022] empirically observes that softmax-based scores are superior in misclassification on a few benchmarks, and combining it with class agnostic features such as the norm of the output features of the penultimate layer or the residual score introduced in Wang et al. [2022] could improve SCOD detection. Narasimhan et al. [2024] provides a plugin framework to combine off-theshelf SC and OOD detection methods to achieve a Bayesoptimal black-box rejector, from which this work extends to introduce our combined SCOD rejector that minimizes regret on the target task.

A different approach, distinct from the one presented in this work and based on orthogonal assumptions, is proposed in Franc et al. [2024]. It aligns with the white-box scenarios outlined in Narasimhan et al. [2024], and in analogy with Gomes et al. [2024] aims to define a data-driven Bayesian SCOD detector that requires a training algorithm, in-d, and notably multiple out-d data shots. Katz-Samuels et al. [2022] also leverages learning the optimization of a surrogate constrained optimization problem using unlabeled in-the-wild data, but in a framework that fits the white-box approach in Narasimhan et al. [2024]. The concurrent work [Vishwakarma et al., 2024] incorporates expert human feedback to safely update the OOD detection threshold.

8 CONCLUSION

We proposed a regret minimization-based framework to aggregate several off-the-shelf OOD detection methods with the SCOD paradigm. Crucially, this method is zero-shot, easy to implement, cost-effective, and can be applied to several OOD methods. We show that our framework can consistently reduce the worst-case detection risk across several domains while also attaining performance comparable to SOTA solution when they are plugged in the black-box SCOD framework Narasimhan et al. [2024].

SCOD presents a particularly challenging detection problem in Machine Learning, as it involves detecting both misclassified samples and those originating from outside the training distribution. The novel approach we proposed in this work aligns distance-based and confidence-based detectors, and formally aggregates their decisions, providing a principled way to combine off-the-shelf detectors, and providing a new perspective on the cat-and-mouse game of developing new ones—an endeavor often driven solely by empirical comparisons and lacking theoretical guarantees.

We are hopeful that this work will stimulate further research in the field of SCOD, particularly toward a more rigorous assessment of the worst-case risk of newly proposed methods. By providing a principled baseline through the MRPSA solution, our framework offers a modular and flexible design fostering cumulative progress rather than isolated advancements.

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Optimal Zero-shot Regret Minimization for Selective Classification With Out-of-Distribution Detection

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A APPENDIX

A.1 PROOFS

A.1.1 Proof of Equation (7)

Proof.

$$\max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}} \left[-\log \mathbb{Q}_{Z|\boldsymbol{x}} \right] = \max_{k \in \mathcal{K}} \left[\mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}} \left[-\log \mathbb{Q}_{Z|\boldsymbol{x}}^{(k)} \right] + \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}} \left[\log \left(\frac{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}}{\mathbb{Q}_{Z|\boldsymbol{x}}} \right) \right] \right] \right]$$
$$\leq \max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}} \left[-\log \mathbb{Q}_{Z|\boldsymbol{x}}^{(k)} \right] + \max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}} \left[\log \left(\frac{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}}{\mathbb{Q}_{Z|\boldsymbol{x}}} \right) \right].$$

| - | - | - | |
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A.1.2 Proof of Equation (8)

Proof. The equality holds by noticing that

$$\max_{P_{\Omega}} \mathbb{E}_{\Omega} \left[D_{\mathsf{KL}} \left(\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)} \| \mathbb{Q}_{Z|\boldsymbol{x}} \right) \right] \leq \max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}} \left[\log \left(\frac{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}}{\mathbb{Q}_{Z|\boldsymbol{x}}} \right) \right],$$

and moreover,

$$\max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}} \left[\log \left(\frac{\mathbb{Q}_{Z|\boldsymbol{x}}^{(k)}}{\mathbb{Q}_{Z|\boldsymbol{x}}} \right) \right] = \mathbb{E}_{\bar{\Omega}} \left[D_{\mathrm{KL}} \left(\mathbb{Q}_{Z|\boldsymbol{x}}^{(\bar{\Omega})} \| \mathbb{Q}_{Z|\boldsymbol{x}} \right) \right],$$

for a uniformly distributed random variable $\overline{\Omega}$ for the set of maximizers $\overline{\mathcal{K}} = \arg \max_{k \in \mathcal{K}} \mathbb{E}_{\mathbb{Q}_{Z|\mathbf{x}}^{(k)}} \left[\log \left(\frac{\mathbb{Q}_{Z|\mathbf{x}}^{(k)}}{\mathbb{Q}_{Z|\mathbf{x}}} \right) \right]$, zero otherwise.

^{*}Work done while working at Université Paris-Saclay CNRS CentraleSupélec.

A.1.3 **Proof of Equation (9)**

Proof. Let us consider a zero-sum game with a concave-convex mapping defined on a product of convex sets. The sets of all probability distributions $\mathbb{Q}_{Z|x}$ and P_{Ω} are two nonempty convex sets, bounded and finite-dimensional. On the other hand, $(P_{\Omega}, \mathbb{Q}_{Z|x}) \to \mathbb{E}_{\Omega} \left[D_{\mathrm{KL}} \left(\mathbb{Q}_{Z|x}^{(\Omega)} \| \mathbb{Q}_{Z|x} \right) \right]$ is a concave-convex mapping, i.e., $P_{\Omega} \to \mathbb{E}_{\Omega} \left[D_{\mathrm{KL}} \left(\mathbb{Q}_{Z|x}^{(\Omega)} \| \mathbb{Q}_{Z|x} \right) \right]$ is concave and $\mathbb{Q}_{Z|x} \to \mathbb{E}_{\Omega} \left[D_{\mathrm{KL}} \left(\mathbb{Q}_{Z|x}^{(\Omega)} \| \mathbb{Q}_{Z|x} \right) \right]$ is convex for every $(P_{\Omega}, \mathbb{Q}_{Z|x})$. Then, by classical min-max theorem von Neumann [1928] we have

$$\min_{\mathbb{Q}_{Z|\boldsymbol{x}}} \max_{P_{\Omega}} \mathbb{E}_{\Omega} \left[D_{\mathrm{KL}} \left(\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)} \| \mathbb{Q}_{Z|\boldsymbol{x}} \right) \right] = \max_{P_{\Omega}} \min_{\widehat{\mathbb{Q}}_{Z|\boldsymbol{x}}} \mathbb{E}_{\Omega} \left[D_{\mathrm{KL}} \left(\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)} \| \mathbb{Q}_{Z|\boldsymbol{x}} \right) \right].$$

For the next result, it is enough to show that

$$\min_{\widehat{\mathbb{Q}}_{Z|\boldsymbol{x}}} \mathbb{E}_{\Omega} \left[D_{\mathrm{KL}} \left(\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)} \| \mathbb{Q}_{Z|\boldsymbol{x}} \right) \right] = I_{\boldsymbol{x}}(\Omega; Z),$$
(13)

for every random variable Ω distributed according to an arbitrary probability distribution P_{Ω} and each distribution $\mathbb{Q}_{Z|\mathbf{x}}^{(\Omega)}$. We begin by showing that

$$\mathbb{E}_{\Omega}\left[D_{\mathrm{KL}}\left(\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)} \| \mathbb{Q}_{Z|\boldsymbol{x}}\right)\right] \geq I_{\boldsymbol{x}}(\Omega; Z),$$

for any arbitrary distributions P_{Ω} and $\mathbb{Q}_{Z|\mathbf{z}}^{(\Omega)}$. To this end, we use the following identities:

$$\mathbb{E}_{\Omega}\left[D_{\mathrm{KL}}\left(\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)} \| \mathbb{Q}_{Z|\boldsymbol{x}}\right)\right] = \mathbb{E}_{\Omega}\mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)}}\left(\log\frac{\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)}}{\mathbb{Q}_{Z|\boldsymbol{x}}}\right)$$
$$= \mathbb{E}_{\Omega}\mathbb{E}_{\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)}}\left(\log\frac{\mathbb{Q}_{Z|\boldsymbol{x}}^{(\Omega)}}{P_{Z}}\right) + D_{\mathrm{KL}}\left(P_{Z}\|\mathbb{Q}_{Z|\boldsymbol{x}}\right)$$
$$= I_{\boldsymbol{x}}(\Omega; Z) + D_{\mathrm{KL}}\left(P_{Z}\|\mathbb{Q}_{Z|\boldsymbol{x}}\right) \ge I_{\boldsymbol{x}}(\Omega; Z), \tag{14}$$

where P_Z represents the marginal distribution of $\mathbb{Q}_{Z|x}^{(\Omega)}$ w.r.t. P_Ω and the last inequality holds for the fact that the KL divergence is non-negative. Finally, it is easy to check that by for $\mathbb{Q}_{Z|x} = P_Z$ the lower bound in (14) holds. As a consequence, this proves the identity in expression (13). By taking the maximum overall probability distributions P_Ω at both sides of expression (13) the claim follows.

A.2 ON THE CONSEQUENCES OF DOMAIN SHIFT

So far we have described an optimal solution to aggregate $|\mathcal{K}|$ detectors (cf. Equation (10)) such that each of them has is assumed to effectively detect in-d samples and out-d samples drawn from a certain $\mathbb{P}_{out}^{(k)}$, i.e. the *source domain*. Let us now suppose that a new $k^* \notin \mathcal{K}$ is introduced. Clearly, it may be the case that none of the detectors we aggregated is effectively deployable for this task, thus one may wonder whether the aggregated detector will be able to work on k^* , i.e. the *new domain*. In this section, we consider this problem and provide an upper bound on detection error for the new domain as a function of the detection error for the previous domain.

Let us consider a detector r, like the one defined in Equation (10). Let us also assume a function $f^S : \mathbb{R}^d \to \{0, 1\}$, i.e. the source label function (oracle) which assigns a label to any input sample distributed according to the source domain. Let us define P_X^S , the distribution of the input variable X (in-d or out-d) over the input space \mathbb{R}^d , where the out-d samples are generated according to the possible $|\mathcal{K}|$ out-d of which our aggregated detector is aware.

Similarly, we define $f^T : \mathbb{R}^d \to \{0, 1\}$, i.e. the label function relative to the new domain. The new (testing) domain, defined as P_X^T is the distribution of the input X (in-d or out-d), where the OOD samples are generated and indexed with k^* , which are new to our detector.

We can now define the source error:

$$P_e^S(r) \doteq \mathbb{E}_{\boldsymbol{x} \sim P_X^S} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^S(\boldsymbol{x}) \right] \right], \tag{15}$$

and the error on the new domain:

$$P_e^T(r) \doteq \mathbb{E}_{\boldsymbol{x} \sim P_X^T} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^T(\boldsymbol{x}) \right] \right].$$
(16)

Let

$$d\left(P_{X|Z=1}^{S}, P_{X|Z=1}^{T}\right) \doteq 2\sup_{B\in\beta} \left|\Pr_{S}(B) - \Pr_{T}(B)\right|,\tag{17}$$

where β is the set of measurable subsets under the noise distributions $P_{X|Z=1}^{S}$, and $P_{X|Z=1}^{T}$. Then, according to Ben-David et al. [2010],

$$P_{e}^{T}(r) \leq P_{e}^{S}(r) + d\left(P_{X|Z=1}^{S}, P_{X|Z=1}^{T}\right) + \min\left\{\mathbb{E}_{\boldsymbol{x}\sim P_{X}^{S}}[|f^{S}(\boldsymbol{x}) - f^{T}(\boldsymbol{x})|], \\ \mathbb{E}_{\boldsymbol{x}\sim P_{X}^{T}}[|f^{S}(\boldsymbol{x}) - f^{T}(\boldsymbol{x})|]\right\}.$$
(18)

Intuitively, as the detector has never seen samples from the new domain, it is expected to perform worse on it. Conversely, the above bound indicates that the loss in terms of performance is expected to be low proportionally to a small $d\left(P_{X|Z=1}^{S}, P_{X|Z=1}^{T}\right)$ of the noises between the domains. This proof is adapted from Ben-David et al. [2010].

Proof.

$$P_{e}^{T}(r) = P_{e}^{T}(r) + P_{e}^{S}(r) - P_{e}^{S}(r) + \mathbb{E}_{\boldsymbol{x} \sim P_{X}^{S}} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^{T}(\boldsymbol{x}) \right] \right] - \mathbb{E}_{\boldsymbol{x} \sim P_{X}^{S}} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^{T}(\boldsymbol{x}) \right] \right]$$

$$(19)$$

$$\leq P_e^S(r) + \left| \mathbb{E}_{\boldsymbol{x} \sim P_X^S} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^T(\boldsymbol{x}) \right] \right] - P_e^S(r) \right| +$$

$$P_e^T(r) - \mathbb{E}_{\boldsymbol{x} \sim P_X^S} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^T(\boldsymbol{x}) \right] \right]$$
(20)

$$\leq P_e^S(r) + \mathbb{E}_{\boldsymbol{x} \sim P_X^S} \left| \mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^T(\boldsymbol{x}) \right] - \mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^S(\boldsymbol{x}) \right] \right| + \left| P_x^T(r) - \mathbb{E}_{\boldsymbol{x} \sim P_X} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^T(\boldsymbol{x}) \right] \right] \right|$$
(21)

$$\frac{P_e^{T}(r) - \mathbb{E}_{\boldsymbol{x} \sim P_X^S}\left[\mathbb{I}\left[r\left(\boldsymbol{x}\right) \neq f^{T}\left(\boldsymbol{x}\right)\right]\right]$$
(21)

$$\leq P_e^S(r) + \mathbb{E}_{\boldsymbol{x} \sim P_X^S} \left| f^T(\boldsymbol{x}) - f^S(\boldsymbol{x}) \right| + \left| P_e^T(r) - \mathbb{E}_{\boldsymbol{x} \sim P_X^S} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^T(\boldsymbol{x}) \right] \right] \right|$$
(22)

$$\leq P_e^S(r) + \mathbb{E}_{\boldsymbol{x} \sim P_X^S} \left| f^T(\boldsymbol{x}) - f^S(\boldsymbol{x}) \right| + d \left(P_{X|Z=1}^S, P_{X|Z=1}^T \right).$$
(23)

Notice that by choosing to add and subtract $\mathbb{E}_{\boldsymbol{x}\sim P_X^T} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^T(\boldsymbol{x}) \right] \right]$ instead of $\mathbb{E}_{\boldsymbol{x}\sim P_X^S} \left[\mathbb{1} \left[r\left(\boldsymbol{x} \right) \neq f^T(\boldsymbol{x}) \right] \right]$, we would get the term $\mathbb{E}_{\boldsymbol{x}\sim P_X^T} \left| f^T(\boldsymbol{x}) - f^S(\boldsymbol{x}) \right|$, instead of $\mathbb{E}_{\boldsymbol{x}\sim P_X^S} \left| f^T(\boldsymbol{x}) - f^S(\boldsymbol{x}) \right|$. Therefore, the final result holds true:

$$P_{e}^{T}(r) \leq P_{e}^{S}(r) + d\left(P_{X|Z=1}^{S}, P_{X|Z=1}^{T}\right) + \min\left\{\mathbb{E}_{\boldsymbol{x}\sim P_{X}^{S}}[|f^{S}(\boldsymbol{x}) - f^{T}(\boldsymbol{x})|], \\ \mathbb{E}_{\boldsymbol{x}\sim P_{X}^{T}}[|f^{S}(\boldsymbol{x}) - f^{T}(\boldsymbol{x})|]\right\}.$$

$$(24)$$

A.3 BLAHUT-ARIMOTO ALGORITHM TIME ANALYSIS

The Blahut-Arimoto algorithm can be accelerated with parallelized computing. Notably, we observe in Figure 4 that the processing times are negligible when implemented on a GPU when compared to the inference time of a deep neural network in classic tasks. Thus, our algorithm does not represent a bottleneck in computation when deployed.



Figure 4: Time analysis for the Blahut-Arimoto algorithm, where dimension is the hypothetical number of detectors to combine.

```
import torch
  def blahut_arimoto(probs: torch.Tensor, max_iter: int = int(le6), tol: float = le-6):
4
      num_samples, num_detectors, _ = scores.shape
5
      weights = torch.ones(num_samples, num_detectors, 1) / num_detectors
      for _ in range(max_iter):
          q = torch.mul(weights, probs)
9
          q = q / torch.sum(q, dim=1, keepdim=True)
10
          w = torch.prod(torch.pow(q, probs), dim=2, keepdim=True)
          w = w / torch.sum(w, dim=1, keepdim=True)
14
          tolerance = torch.linalg.norm(w - weights) / torch.linalg.norm(weights)
15
          weights = w
16
          if tolerance < tol:
18
              break
19
20
      return weights
```

Listing 1: Blahut-Arimoto algorithm implementation with PyTorch [Paszke et al., 2019].

A.4 COMPARISON WITH BASELINE AGGREGATION ALGORITHMS

We ran experiments with baseline aggregation algorithms and compared their performance to our MRPSA framework on CIFAR-10 and ImageNet benchmarks in Tables 3 and 4, respectively. The *Average* baseline is a simple mean between PDS transformed scores from the same 12 off-the-shelf detectors as in the main experiments in Table 2. The two majority vote methods are based on an evaluation of the detectors' individual decisions on each sample. The aggregation is based on the majority vote, i.e. a weight of 1 is assigned to a detector in agreement with the majority of the detectors, and 0 otherwise. In particular, we consider two variants: in one case we pick a *random* detector within the majority group, in the other case we pick the most *confident* detectors. Even though average and majority vote paradigm's might achieves comparable performance in our benchmarks and others, it is important to stress that these solutions, in stark contrast with ours aggregation, do not guarantee optimality within the regret minimization framework. Thus, despite comparable performance w.r.t. our solution, they do not come with a theoretical guarantee of robustness.

Table 3: Comparative analysis of AURC in the black-box SCOD framework between three baseline aggregation methods (combining 12 off-the-shelf methods) for ResNet-34 trained on CIFAR-10. Results are sorted in descending order by average.

| | C-100 | SVHN | iSUN | LS (c) | LS (r) | TIN (c) | TIN (r) | Tex. | Places | Unif. | Gauss | Avg |
|----------------------|-------|-------|-------|--------|--------|---------|---------|-------|--------|--------------|--------------|-------|
| Majority (confident) | 0.283 | 0.206 | 0.214 | 0.187 | 0.205 | 0.193 | 0.241 | 0.299 | 0.273 | 0.189 | 0.222 | 0.229 |
| Majority (random) | 0.272 | 0.202 | 0.207 | 0.182 | 0.201 | 0.190 | 0.231 | 0.291 | 0.262 | <u>0.183</u> | 0.205 | 0.221 |
| Average | 0.254 | 0.197 | 0.201 | 0.182 | 0.195 | 0.188 | 0.221 | 0.252 | 0.248 | 0.184 | 0.209 | 0.212 |
| Ours | 0.242 | 0.203 | 0.201 | 0.187 | 0.196 | 0.196 | 0.213 | 0.232 | 0.235 | 0.188 | <u>0.204</u> | 0.209 |

Table 4: Comparative analysis of AURC in the black-box SCOD framework between three baseline aggregation methods (combining 12 off-the-shelf methods) for ResNet-50 trained on ImageNet. Results are sorted in descending order by average.

| | iNat. | Species | Places | OpenIm. | SSB (e) | Tex. | NINCO | SSB (h) | Avg |
|----------------------|-------|---------|--------------|---------|--------------|-------|-------|---------|--------------|
| Majority (confident) | 0.307 | 0.330 | 0.327 | 0.325 | 0.321 | 0.329 | 0.347 | 0.388 | 0.336 |
| Majority (random) | 0.295 | 0.327 | 0.319 | 0.322 | 0.315 | 0.315 | 0.342 | 0.384 | 0.328 |
| Average | 0.291 | 0.319 | <u>0.315</u> | 0.310 | <u>0.308</u> | 0.310 | 0.332 | 0.374 | <u>0.321</u> |
| Ours | 0.293 | 0.315 | <u>0.314</u> | 0.306 | <u>0.308</u> | 0.302 | 0.335 | 0.388 | 0.321 |

A.5 INTERPRETABILITY OF OUR FRAMEWORK

Figure 5 sheds a light on the interpretability of our method. Due to its inherent design, it aims to perform robust detection across all potential tasks captured by the available pool of detectors. As a result, the method may assign non-zero weights to detectors that are suboptimal for the specific task.

In particular, in Figure 5a we consider a DenseNet121 model trained on CIFAR-100 and focus on the SCOD detection task, with out-of-distribution (OOD) samples from the SVHN dataset. Crucially, the best stand-alone detector is MCos (Maximum Cosine Similarity), and we observe that our aggregation successfully highlights this by assigning it the highest weight—most importantly, without requiring any training or side information about the specific out-distribution used during evaluation.

Figure 5b shows that the weight assignment reflects an intrinsic characteristic of the underlying pool of detectors. These detectors, while trained to recognize specific OOD misclassified samples, are all exposed to the same in-distribution samples once the target DenseNet121 model trained on CIFAR-100 is used. This is evidenced by the low entropy observed for in-distribution samples (blue boxplot), where different detectors tend to agree and can therefore be assigned similar weights. In contrast, entropy is higher for OOD samples (purple boxplot), where detectors are more likely to disagree—necessitating a more nuanced weight assignment. This is an important interpretability feature that is inherent to our proposed solution, that would be lost in less nuanced aggregation methods, such as the average one.

Finally, Figure 5c compares the weights distribution for the average aggregation (dashed line) and our method (blue histogram). The average aggregation assigns the same weight to any of the 12 considered detectors, while our aggregation provides a more nuanced weight assignment, which is able to highlight the best performing detectors, as shown in Figure 5a. Though in terms of hard decision the two methods may exhibit similar performance in some cases, our method provides not only a theoretically grounded approach, but also a more interpretable one, as it allows us to understand the behavior of the detectors and their agreement on the samples.



(a) Average maximum weight histogram attributed to each of the individual detectors with CIFAR100 as in-distribution and SVHN as out-of-distribution.





(b) Shannon Entropy values computed from the weights of our MRPSA framework.

(c) Histogram of individual weight values of the MRPSA framework.

Figure 5: Interpretability plots of MRPSA showcasing interesting properties of the aggregation weights.

A.6 ADDITIONAL RESULTS

Table 5: Comparative analysis of AURC in the black-box SCOD framework between 12 existing OOD detection methods and our method (combining the other 12 methods) for CIFAR-10 models. Results are sorted in descending order by average AURC.

| | | A | /G | C- | 100 | GA | USS | IS | UN | LS | (C) | LS | (R) | PLA | CES | sv | HN | TI | x. | TIN | (C) | TIN | (R) | UN | UF. |
|-----------------|-----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC |
| | RMAHA | 0.387 | 0.713 | 0.386 | 0.721 | 0.595 | 0.374 | 0.252 | 0.891 | 0.520 | 0.570 | 0.250 | 0.902 | 0.359 | 0.773 | 0.586 | 0.428 | 0.428 | 0.704 | 0.264 | 0.902 | 0.287 | 0.851 | 0.327 | 0.724 |
| 10 | REACT KL M | 0.282 | 0.797 | 0.314 | 0.770 | 0.315 | 0.690 | 0.237 | 0.885 | 0.273 | 0.824 | 0.234 | 0.889 | 0.245 | 0.874 | 0.280 | 0.797 | 0.339 | 0.709 | 0.274 | 0.810 | 0.270 | 0.824 | 0.316 | 0.692 |
| ÅR- | ENERGY | 0.228 | 0.918 | 0.270 | 0.860 | 0.220 | 0.905 | 0.201 | 0.956 | 0.227 | 0.923 | 0.198 | 0.961 | 0.254 | 0.890 | 0.214 | 0.937 | 0.307 | 0.823 | 0.213 | 0.937 | 0.212 | 0.937 | 0.191 | 0.970 |
| CIE | MAXL | 0.228 | 0.919 | 0.269 | 0.862 | 0.220 | 0.907 | 0.201 | 0.956 | 0.227 | 0.924 | 0.198 | 0.961 | 0.256 | 0.888 | 0.214 | 0.938 | 0.306 | 0.825 | 0.213 | 0.938 | 0.212 | 0.938 | 0.190 | 0.973 |
| 5 | OURS | 0.228 | 0.919 | 0.269 | 0.862 | 0.219 | 0.907 | 0.201 | 0.956 | 0.227 | 0.924 | 0.198 | 0.961 | 0.255 | 0.889 | 0.214 | 0.938 | 0.305 | 0.825 | 0.214 | 0.937 | 0.212 | 0.937 | 0.189 | 0.972 |
| E. | IGEOOD | 0.217 | 0.929 | 0.248 | 0.884 | 0.221 | 0.905 | 0.199 | 0.958 | 0.214 | 0.935 | 0.196 | 0.962 | 0.239 | 0.904 | 0.205 | 0.949 | 0.262 | 0.863 | 0.208 | 0.940 | 0.210 | 0.940 | 0.186 | 0.979 |
| ENE | MSP | 0.215 | 0.928 | 0.243 | 0.890 | 0.207 | 0.931 | 0.204 | 0.945 | 0.217 | 0.929 | 0.200 | 0.951 | 0.233 | 0.906 | 0.205 | 0.944 | 0.249 | 0.883 | 0.211 | 0.931 | 0.212 | 0.931 | 0.189 | 0.972 |
| ENS | DOCTOR | 0.215 | 0.925 | 0.243 | 0.891 | 0.180 | 0.931 | 0.224 | 0.904 | 0.211 | 0.929 | 0.220 | 0.912 | 0.237 | 0.890 | 0.205 | 0.937 | 0.201 | 0.884 | 0.205 | 0.941 | 0.211 | 0.933 | 0.180 | 0.988 |
| Ω | MCos | 0.201 | 0.954 | 0.241 | 0.895 | 0.194 | 0.962 | 0.200 | 0.955 | 0.196 | 0.961 | 0.196 | 0.962 | 0.221 | 0.926 | 0.188 | 0.977 | 0.197 | 0.960 | 0.193 | 0.967 | 0.210 | 0.937 | 0.177 | 0.993 |
| | KNN | 0.192 | 0.967 | 0.227 | 0.912 | 0.185 | 0.980 | 0.191 | 0.970 | 0.188 | 0.975 | 0.189 | 0.974 | 0.209 | 0.943 | 0.184 | 0.983 | 0.191 | 0.969 | 0.185 | 0.981 | 0.198 | 0.956 | 0.169 | 0.994 |
| | KL M | 0.238 | 0.882 | 0.203 | 0.832 | 0.181 | 0.982 | 0.235 | 0.880 | 0.229 | 0.882 | 0.233 | 0.883 | 0.282 | 0.848 | 0.302 | 0.898 | 0.232 | 0.894 | 0.234 | 0.847 | 0.239 | 0.875 | 0.188 | 0.988 |
| 0 | REACT | 0.214 | 0.935 | 0.254 | 0.883 | 0.185 | 0.971 | 0.206 | 0.946 | 0.180 | 0.983 | 0.200 | 0.954 | 0.238 | 0.902 | 0.249 | 0.881 | 0.245 | 0.894 | 0.193 | 0.965 | 0.222 | 0.926 | 0.183 | 0.976 |
| -R- | MAXL | 0.205 | 0.944 | 0.239 | 0.897 | 0.203 | 0.936 | 0.193 | 0.961 | 0.177 | 0.989 | 0.191 | 0.965 | 0.228 | 0.915 | 0.210 | 0.931 | 0.245 | 0.896 | 0.183 | 0.979 | 0.202 | 0.946 | 0.189 | 0.966 |
| CIF/ | ENERGY | 0.205 | 0.944 | 0.239 | 0.897 | 0.203 | 0.934 | 0.193 | 0.961 | 0.176 | 0.990 | 0.190 | 0.966 | 0.227 | 0.914 | 0.210 | 0.932 | 0.244 | 0.896 | 0.182 | 0.980 | 0.202 | 0.947 | 0.189 | 0.963 |
| 8 | RMAHA | 0.205 | 0.938 | 0.231 | 0.900 | 0.196 | 0.945 | 0.199 | 0.947 | 0.180 | 0.982 | 0.196 | 0.952 | 0.228 | 0.909 | 0.219 | 0.911 | 0.219 | 0.910 | 0.192 | 0.963 | 0.205 | 0.937 | 0.187 | 0.965 |
| ET-1 | MSP | 0.204 | 0.939 | 0.230 | 0.902 | 0.182 | 0.977 | 0.200 | 0.944 | 0.188 | 0.965 | 0.198 | 0.949 | 0.232 | 0.904 | 0.221 | 0.902 | 0.212 | 0.923 | 0.198 | 0.947 | 0.206 | 0.934 | 0.180 | 0.981 |
| SN | MCos | 0.203 | 0.942 | 0.226 | 0.907 | 0.183 | 0.976 | 0.200 | 0.946 | 0.192 | 0.961 | 0.197 | 0.952 | 0.226 | 0.913 | 0.208 | 0.924 | 0.213 | 0.925 | 0.203 | 0.941 | 0.209 | 0.930 | 0.180 | 0.982 |
| Ri | DOCTOR | 0.203 | 0.941 | 0.228 | 0.904 | 0.191 | 0.957 | 0.199 | 0.946 | 0.181 | 0.979 | 0.197 | 0.950 | 0.225 | 0.909 | 0.208 | 0.928 | 0.228 | 0.909 | 0.189 | 0.964 | 0.205 | 0.936 | 0.184 | 0.973 |
| | KNN | 0.198 | 0.948 | 0.218 | 0.905 | 0.195 | 0.955 | 0.195 | 0.961 | 0.183 | 0.989 | 0.190 | 0.966 | 0.220 | 0.913 | 0.208 | 0.934 | 0.205 | 0.936 | 0.185 | 0.979 | 0.198 | 0.947 | 0.184 | 0.975 |
| | RMAHA | 0.297 | 0.860 | 0.342 | 0.811 | 0.343 | 0.786 | 0.290 | 0.873 | 0.222 | 0.940 | 0.271 | 0.892 | 0.321 | 0.837 | 0.285 | 0.881 | 0.372 | 0.789 | 0.258 | 0.906 | 0.312 | 0.844 | 0.252 | 0.897 |
| _ | ODIN | 0.242 | 0.908 | 0.308 | 0.839 | 0.266 | 0.851 | 0.223 | 0.928 | 0.180 | 0.984 | 0.211 | 0.943 | 0.294 | 0.861 | 0.208 | 0.949 | 0.333 | 0.826 | 0.186 | 0.974 | 0.260 | 0.887 | 0.198 | 0.952 |
| -10 | MAXL | 0.242 | 0.909 | 0.308 | 0.839 | 0.265 | 0.851 | 0.222 | 0.928 | 0.180 | 0.984 | 0.211 | 0.943 | 0.294 | 0.861 | 0.208 | 0.949 | 0.333 | 0.826 | 0.186 | 0.974 | 0.260 | 0.887 | 0.197 | 0.952 |
| ² AR | Igeood | 0.234 | 0.917 | 0.291 | 0.852 | 0.257 | 0.872 | 0.220 | 0.933 | 0.179 | 0.985 | 0.208 | 0.946 | 0.293 | 0.864 | 0.201 | 0.955 | 0.299 | 0.851 | 0.184 | 0.975 | 0.254 | 0.895 | 0.190 | 0.965 |
| G | REACT | 0.231 | 0.922 | 0.300 | 0.848 | 0.204 | 0.939 | 0.216 | 0.936 | 0.189 | 0.974 | 0.206 | 0.949 | 0.250 | 0.894 | 0.223 | 0.933 | 0.315 | 0.841 | 0.198 | 0.960 | 0.248 | 0.899 | 0.187 | 0.970 |
| 34 | DOCTOR | 0.225 | 0.924 | 0.275 | 0.870 | 0.213 | 0.922 | 0.213 | 0.934 | 0.185 | 0.972 | 0.205 | 0.944 | 0.274 | 0.879 | 0.200 | 0.952 | 0.295 | 0.863 | 0.191 | 0.960 | 0.238 | 0.908 | 0.186 | 0.968 |
| NET | KL M | 0.212 | 0.931 | 0.245 | 0.885 | 0.206 | 0.929 | 0.209 | 0.935 | 0.188 | 0.968 | 0.203 | 0.944 | 0.246 | 0.889 | 0.199 | 0.950 | 0.227 | 0.900 | 0.203 | 0.951 | 0.216 | 0.921 | 0.187 | 0.966 |
| RES | MAHA OURS | 0.210 | 0.929 | 0.241 | 0.885 | 0.186 | 0.965 | 0.197 | 0.947 | 0.208 | 0.927 | 0.196 | 0.952 | 0.227 | 0.904 | 0.220 | 0.910 | 0.212 | 0.925 | 0.222 | 0.913 | 0.207 | 0.933 | 0.192 | 0.955 |
| _ | MCos | 0.197 | 0.949 | 0.219 | 0.914 | 0.186 | 0.964 | 0.191 | 0.958 | 0.192 | 0.957 | 0.188 | 0.964 | 0.217 | 0.922 | 0.193 | 0.954 | 0.204 | 0.936 | 0.199 | 0.946 | 0.200 | 0.944 | 0.178 | 0.984 |
| | KNN | 0.193 | 0.955 | 0.214 | 0.921 | 0.187 | 0.962 | 0.187 | 0.965 | 0.187 | 0.966 | 0.185 | 0.970 | 0.212 | 0.929 | 0.190 | 0.960 | 0.198 | 0.944 | 0.193 | 0.955 | 0.195 | 0.951 | 0.177 | 0.984 |
| | REACT | 0.334 | 0.732 | 0.395 | 0.654 | 0.363 | 0.648 | 0.300 | 0.794 | 0.287 | 0.797 | 0.300 | 0.793 | 0.314 | 0.759 | 0.357 | 0.665 | 0.417 | 0.643 | 0.322 | 0.758 | 0.354 | 0.726 | 0.260 | 0.814 |
| ~ | ODIN | 0.234 | 0.925 | 0.294 | 0.849 | 0.190 | 0.978 | 0.216 | 0.946 | 0.215 | 0.950 | 0.217 | 0.945 | 0.287 | 0.863 | 0.248 | 0.905 | 0.235 | 0.903 | 0.246 | 0.916 | 0.230 | 0.928 | 0.181 | 0.991 |
| -10 | MAXL | 0.233 | 0.925 | 0.294 | 0.849 | 0.190 | 0.978 | 0.216 | 0.946 | 0.215 | 0.950 | 0.217 | 0.945 | 0.286 | 0.863 | 0.249 | 0.904 | 0.248 | 0.903 | 0.245 | 0.916 | 0.230 | 0.928 | 0.179 | 0.991 |
| AR | ENERGY KL M | 0.233 | 0.926 | 0.294 | 0.849 | 0.190 | 0.979 | 0.216 | 0.947 | 0.215 | 0.951 | 0.217 | 0.946 | 0.286 | 0.865 | 0.249 | 0.904 | 0.248 | 0.903 | 0.246 | 0.917 | 0.230 | 0.929 | 0.178 | 0.991 |
| Ð | MSP | 0.228 | 0.926 | 0.272 | 0.868 | 0.194 | 0.964 | 0.215 | 0.940 | 0.215 | 0.942 | 0.217 | 0.939 | 0.277 | 0.868 | 0.221 | 0.929 | 0.242 | 0.905 | 0.239 | 0.917 | 0.228 | 0.923 | 0.183 | 0.989 |
| -16 | DOCTOR RMAHA | 0.227 | 0.927 | 0.272 | 0.868 | 0.194 | 0.966 | 0.215 | 0.941 | 0.214 | 0.944 | 0.216 | 0.940 | 0.274 | 0.872 | 0.221 | 0.929 | 0.242 | 0.906 | 0.239 | 0.917 | 0.227 | 0.924 | 0.181 | 0.991 |
| 99 | OURS | 0.217 | 0.933 | 0.253 | 0.878 | 0.204 | 0.944 | 0.204 | 0.953 | 0.200 | 0.960 | 0.204 | 0.953 | 0.236 | 0.908 | 0.219 | 0.924 | 0.241 | 0.900 | 0.215 | 0.937 | 0.221 | 0.927 | 0.186 | 0.983 |
| > | MAHA | 0.212 | 0.936 | 0.244 | 0.890 | 0.193 | 0.967 | 0.206 | 0.948 | 0.203 | 0.947 | 0.203 | 0.951 | 0.241 | 0.900 | 0.216 | 0.923 | 0.219 | 0.921 | 0.211 | 0.936 | 0.212 | 0.935 | 0.188 | 0.976 |
| | MCOS KNN | 0.209 | 0.944 | 0.244 | 0.895 | 0.192 | 0.970 | 0.200 | 0.957 | 0.200 | 0.955 | 0.200 | 0.957 | 0.238 | 0.905 | 0.209 | 0.938 | 0.218 | 0.928 | 0.207 | 0.945 | 0.207 | 0.945 | 0.183 | 0.990 |
| | KL M | 0.179 | 0.975 | 0.185 | 0.970 | 0.154 | 0.997 | 0.190 | 0.966 | 0.174 | 0.981 | 0.191 | 0.965 | 0.194 | 0.964 | 0.166 | 0.986 | 0.153 | 0.997 | 0.198 | 0.958 | 0.213 | 0.944 | 0.155 | 0.997 |
| | RMAHA | 0.165 | 0.982 | 0.167 | 0.980 | 0.161 | 0.981 | 0.164 | 0.985 | 0.163 | 0.987 | 0.165 | 0.983 | 0.168 | 0.978 | 0.163 | 0.986 | 0.161 | 0.988 | 0.168 | 0.978 | 0.171 | 0.974 | 0.162 | 0.981 |
| 6 | MSP | 0.163 | 0.987 | 0.167 | 0.983 | 0.154 | 0.998 | 0.166 | 0.984 | 0.162 | 0.989 | 0.167 | 0.982 | 0.163 | 0.985 | 0.161 | 0.991 | 0.150 | 0.998 | 0.169 | 0.979 | 0.175 | 0.971 | 0.155 | 0.998 |
| LR-1 | IGEOOD | 0.159 | 0.988 | 0.167 | 0.983 | 0.137 | 0.999 | 0.166 | 0.984 | 0.162 | 0.990 | 0.167 | 0.983 | 0.163 | 0.985 | 0.155 | 0.991 | 0.130 | 0.998 | 0.169 | 0.979 | 0.175 | 0.972 | 0.143 | 0.999 |
| CIFA | OURS | 0.158 | 0.990 | 0.164 | 0.987 | 0.138 | 0.997 | 0.162 | 0.989 | 0.159 | 0.993 | 0.162 | 0.989 | 0.162 | 0.987 | 0.158 | 0.996 | 0.154 | 0.998 | 0.166 | 0.984 | 0.171 | 0.977 | 0.141 | 0.997 |
| 6 (C | ODIN MAXL | 0.157 | 0.990 | 0.166 | 0.985 | 0.133 | 0.999 | 0.165 | 0.986 | 0.158 | 0.993 | 0.166 | 0.985 | 0.160 | 0.989 | 0.155 | 0.997 | 0.149 | 0.999 | 0.167 | 0.983 | 0.175 | 0.973 | 0.135 | 0.999 |
| B/1 | ENERGY | 0.155 | 0.990 | 0.166 | 0.984 | 0.129 | 0.999 | 0.165 | 0.986 | 0.159 | 0.994 | 0.166 | 0.985 | 0.155 | 0.990 | 0.157 | 0.997 | 0.138 | 0.999 | 0.167 | 0.983 | 0.175 | 0.974 | 0.130 | 0.999 |
| ΥT- | MAHA | 0.155 | 0.992 | 0.162 | 0.988 | 0.133 | 0.999 | 0.159 | 0.993 | 0.161 | 0.990 | 0.159 | 0.993 | 0.157 | 0.993 | 0.160 | 0.991 | 0.149 | 0.999 | 0.163 | 0.987 | 0.167 | 0.981 | 0.135 | 0.999 |
| - | MCOS REACT | 0.154 | 0.988 | 0.164 | 0.983 | 0.129 | 0.999 | 0.163 | 0.985 | 0.159 | 0.991 | 0.163 | 0.986 | 0.153 | 0.989 0.991 | 0.157 | 0.995 | 0.136 | 0.999 | 0.169 | 0.978 | 0.177 | 0.967 | 0.130 | 0.999 |
| | KNN | 0.153 | 0.994 | 0.161 | 0.990 | 0.133 | 0.999 | 0.157 | 0.995 | 0.155 | 0.997 | 0.157 | 0.995 | 0.159 | 0.991 | 0.150 | 0.998 | 0.149 | 0.999 | 0.161 | 0.990 | 0.164 | 0.985 | 0.135 | 0.999 |

| REACT Q.27 Q.23 Q.23 Q.23 Q.23 | | | A A | VG | C- | 10 | GA | USS | 1S U | UN | LS | (C) | LS | (R) | PLA | CES | SV | HN | TE | EX. | TIN | (C) | TIN | (R) | UN | NIF. |
|--|----------|------------|-------|-------|-------|-------|---------|-------|-------|--------|-------|-------|-------|--------|---------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| Teach 1.49 0.53 0.43 0.26 0.041 0.26 0.25 < | | | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC | RC | ROC |
| Rest 0.20 0.21 0.240 0. | | | | | | | | | | | | | | | | | | | | | | | | | | |
| Bit Bit <td></td> <td>REACT</td> <td>0.409</td> <td>0.755</td> <td>0.513</td> <td>0.596</td> <td>0.360</td> <td>0.825</td> <td>0.405</td> <td>0.761</td> <td>0.411</td> <td>0.750</td> <td>0.404</td> <td>0.768</td> <td>0.425</td> <td>0.729</td> <td>0.460</td> <td>0.651</td> <td>0.417</td> <td>0.746</td> <td>0.343</td> <td>0.880</td> <td>0.407</td> <td>0.757</td> <td>0.353</td> <td>0.841</td> | | REACT | 0.409 | 0.755 | 0.513 | 0.596 | 0.360 | 0.825 | 0.405 | 0.761 | 0.411 | 0.750 | 0.404 | 0.768 | 0.425 | 0.729 | 0.460 | 0.651 | 0.417 | 0.746 | 0.343 | 0.880 | 0.407 | 0.757 | 0.353 | 0.841 |
| Max 0.12 0.12 0.12 0.14 | - | RMAHA | 0.375 | 0.801 | 0.367 | 0.826 | 0.297 | 0.920 | 0.406 | 0.752 | 0.371 | 0.805 | 0.396 | 0.765 | 0.364 | 0.819 | 0.334 | 0.861 | 0.464 | 0.703 | 0.377 | 0.787 | 0.411 | 0.745 | 0.337 | 0.831 |
| Part No.3.29 0.3.30 0.3.20 </td <td>8</td> <td>MAILA</td> <td>0.341</td> <td>0.860</td> <td>0.420</td> <td>0.727</td> <td>0.204</td> <td>0.020</td> <td>0.246</td> <td>0.847</td> <td>0.250</td> <td>0.840</td> <td>0.242</td> <td>0.951</td> <td>0.266</td> <td>0.812</td> <td>0.262</td> <td>0.916</td> <td>0.219</td> <td>0.806</td> <td>0.211</td> <td>0.010</td> <td>0.226</td> <td>0.863</td> <td>0.202</td> <td>0.044</td> | 8 | MAILA | 0.341 | 0.860 | 0.420 | 0.727 | 0.204 | 0.020 | 0.246 | 0.847 | 0.250 | 0.840 | 0.242 | 0.951 | 0.266 | 0.812 | 0.262 | 0.916 | 0.219 | 0.806 | 0.211 | 0.010 | 0.226 | 0.863 | 0.202 | 0.044 |
| No. No. <td></td> <td>MARA</td> <td>0.341</td> <td>0.800</td> <td>0.429</td> <td>0.757</td> <td>0.294</td> <td>0.939</td> <td>0.340</td> <td>0.047</td> <td>0.550</td> <td>0.840</td> <td>0.342</td> <td>0.851</td> <td>0.500</td> <td>0.012</td> <td>0.302</td> <td>0.810</td> <td>0.518</td> <td>0.890</td> <td>0.511</td> <td>0.910</td> <td>0.550</td> <td>0.805</td> <td>0.295</td> <td>0.944</td> | | MARA | 0.341 | 0.800 | 0.429 | 0.757 | 0.294 | 0.939 | 0.340 | 0.047 | 0.550 | 0.840 | 0.342 | 0.851 | 0.500 | 0.012 | 0.302 | 0.810 | 0.518 | 0.890 | 0.511 | 0.910 | 0.550 | 0.805 | 0.295 | 0.944 |
| Dest Dist Dist <th< td=""><td>Ř</td><td>KL M</td><td>0.329</td><td>0.883</td><td>0.366</td><td>0.848</td><td>0.295</td><td>0.917</td><td>0.338</td><td>0.872</td><td>0.322</td><td>0.896</td><td>0.335</td><td>0.875</td><td>0.328</td><td>0.885</td><td>0.326</td><td>0.882</td><td>0.362</td><td>0.853</td><td>0.299</td><td>0.930</td><td>0.337</td><td>0.870</td><td>0.308</td><td>0.888</td></th<> | Ř | KL M | 0.329 | 0.883 | 0.366 | 0.848 | 0.295 | 0.917 | 0.338 | 0.872 | 0.322 | 0.896 | 0.335 | 0.875 | 0.328 | 0.885 | 0.326 | 0.882 | 0.362 | 0.853 | 0.299 | 0.930 | 0.337 | 0.870 | 0.308 | 0.888 |
| D | F/ | ENERGY | 0.325 | 0.885 | 0.355 | 0.842 | 0.307 | 0.902 | 0.329 | 0.880 | 0.316 | 0.900 | 0.325 | 0.887 | 0.327 | 0.889 | 0.321 | 0.889 | 0.360 | 0.841 | 0.300 | 0.926 | 0.336 | 0.868 | 0.301 | 0.916 |
| Ten t | D | ODIN | 0.324 | 0.888 | 0.353 | 0.847 | 0.305 | 0.905 | 0.328 | 0.882 | 0.314 | 0.902 | 0.324 | 0.888 | 0.324 | 0.892 | 0.320 | 0.890 | 0.358 | 0.845 | 0.298 | 0.930 | 0.335 | 0.871 | 0.302 | 0.913 |
| Int Map 0.122 0.88 0.342 0.88 0.310 0.871 0.31 0.897 | ੁ | MAXI | 0.324 | 0.000 | 0.252 | 0.847 | 0.205 | 0.006 | 0.228 | 0.882 | 0.214 | 0.002 | 0.224 | 0.000 | 0.224 | 0.802 | 0.220 | 0.901 | 0.259 | 0.846 | 0.208 | 0.020 | 0 225 | 0.871 | 0.201 | 0.014 |
| Total Liss U.S. U.S. <thu.s.< th=""> U.S. U.S. <th< td=""><td>5</td><td>MAAL</td><td>0.324</td><td>0.888</td><td>0.555</td><td>0.047</td><td>0.305</td><td>0.900</td><td>0.328</td><td>0.882</td><td>0.514</td><td>0.902</td><td>0.324</td><td>0.000</td><td>0.524</td><td>0.092</td><td>0.520</td><td>0.891</td><td>0.558</td><td>0.840</td><td>0.298</td><td>0.950</td><td>0.555</td><td>0.871</td><td>0.301</td><td>0.914</td></th<></thu.s.<> | 5 | MAAL | 0.324 | 0.888 | 0.555 | 0.047 | 0.305 | 0.900 | 0.328 | 0.882 | 0.514 | 0.902 | 0.324 | 0.000 | 0.524 | 0.092 | 0.520 | 0.891 | 0.558 | 0.840 | 0.298 | 0.950 | 0.555 | 0.871 | 0.301 | 0.914 |
| B B C | - 2 | MSP | 0.323 | 0.880 | 0.342 | 0.856 | 0.302 | 0.900 | 0.332 | 0.871 | 0.315 | 0.895 | 0.330 | 0.873 | 0.322 | 0.886 | 0.324 | 0.878 | 0.351 | 0.847 | 0.295 | 0.928 | 0.334 | 0.866 | 0.311 | 0.879 |
| B C | - 5 | DOCTOR | 0.322 | 0.883 | 0.342 | 0.858 | 0.301 | 0.900 | 0.331 | 0.874 | 0.313 | 0.899 | 0.328 | 0.877 | 0.320 | 0.889 | 0.323 | 0.881 | 0.350 | 0.849 | 0.293 | 0.933 | 0.333 | 0.869 | 0.308 | 0.885 |
| 000000000000000000000000000000000000 | Z | IGEOOD | 0.317 | 0.894 | 0.346 | 0.854 | 0.300 | 0.910 | 0.322 | 0.888 | 0.310 | 0.907 | 0.318 | 0.894 | 0.318 | 0.897 | 0.316 | 0.894 | 0.350 | 0.854 | 0.292 | 0.935 | 0.326 | 0.881 | 0.295 | 0.923 |
| 0 | S | Oune | 0.317 | 0.808 | 0.275 | 0.814 | 0.284 | 0.057 | 0.210 | 0.801 | 0.215 | 0.001 | 0.216 | 0.807 | 0 2 2 2 | 0.802 | 0.221 | 0.996 | 0.220 | 0.872 | 0.208 | 0.027 | 0.220 | 0.801 | 0.297 | 0.051 |
| a N.S. 0.10 0.11 0. | ÷. | UNIN | 0.517 | 0.898 | 0.575 | 0.014 | 0.284 | 0.957 | 0.319 | 0.091 | 0.515 | 0.901 | 0.510 | 0.097 | 0.322 | 0.092 | 0.521 | 0.880 | 0.550 | 0.872 | 0.298 | 0.927 | 0.520 | 0.091 | 0.287 | 0.951 |
| MCS 0.36 0.91 0.37 0.91 0.39 0.91 0.39 0.93 0.38 0.93 0.38 0.93 0.39 0.31 0.39 0.91 0.39 0.295 0.93 0.39 0.295 0.93 0.33 0.83 0.39 0.33 0.35 <th< td=""><td>р</td><td>KNN</td><td>0.310</td><td>0.912</td><td>0.374</td><td>0.828</td><td>0.279</td><td>0.963</td><td>0.317</td><td>0.899</td><td>0.313</td><td>0.907</td><td>0.311</td><td>0.908</td><td>0.320</td><td>0.895</td><td>0.313</td><td>0.901</td><td>0.307</td><td>0.915</td><td>0.285</td><td>0.952</td><td>0.314</td><td>0.901</td><td>0.277</td><td>0.963</td></th<> | р | KNN | 0.310 | 0.912 | 0.374 | 0.828 | 0.279 | 0.963 | 0.317 | 0.899 | 0.313 | 0.907 | 0.311 | 0.908 | 0.320 | 0.895 | 0.313 | 0.901 | 0.307 | 0.915 | 0.285 | 0.952 | 0.314 | 0.901 | 0.277 | 0.963 |
| Net Old Ord Old Ord Old Ord Old Old <thold< th=""> <thold< th=""> <thold< th=""></thold<></thold<></thold<> | | MCos | 0.306 | 0.919 | 0.372 | 0.831 | 0.278 | 0.963 | 0.313 | 0.908 | 0.307 | 0.918 | 0.309 | 0.912 | 0.319 | 0.899 | 0.310 | 0.909 | 0.296 | 0.934 | 0.284 | 0.954 | 0.308 | 0.913 | 0.271 | 0.964 |
| Ex D <thd< th=""> D D D</thd<> | | D 1 | 0.067 | 0.000 | | 0.040 | 0.404 | 0.600 | 0.057 | 0.010 | 0.040 | 0.001 | 0.057 | 0.04.0 | 0.040 | 0.007 | 0.007 | 0.844 | 0.050 | 0.000 | 0.064 | 0.000 | 0.054 | 0.010 | 0.000 | |
| Cont Cont <th< td=""><td></td><td>REACT</td><td>0.367</td><td>0.785</td><td>0.338</td><td>0.840</td><td>0.431</td><td>0.630</td><td>0.357</td><td>0.812</td><td>0.342</td><td>0.821</td><td>0.357</td><td>0.812</td><td>0.363</td><td>0.806</td><td>0.397</td><td>0.756</td><td>0.353</td><td>0.820</td><td>0.364</td><td>0.797</td><td>0.356</td><td>0.813</td><td>0.380</td><td>0.724</td></th<> | | REACT | 0.367 | 0.785 | 0.338 | 0.840 | 0.431 | 0.630 | 0.357 | 0.812 | 0.342 | 0.821 | 0.357 | 0.812 | 0.363 | 0.806 | 0.397 | 0.756 | 0.353 | 0.820 | 0.364 | 0.797 | 0.356 | 0.813 | 0.380 | 0.724 |
| B RAMU 0.32 0.838 0.390 0.876 0.314 0.866 0.314 0.860 0.314 0.870 0.314 0.870 0.314 0.870 0.314 0.870 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.330 0.887 0.330 0.887 0.330 0.887 0.310 0.887 0.330 0.887 0.320 0.887 0.320 0.887 0.310 0.887 0.330 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 0.887 0.310 | | KL M | 0.326 | 0.854 | 0.313 | 0.877 | 0.384 | 0.698 | 0.317 | 0.880 | 0.313 | 0.878 | 0.316 | 0.882 | 0.340 | 0.854 | 0.334 | 0.864 | 0.332 | 0.860 | 0.293 | 0.907 | 0.313 | 0.889 | 0.329 | 0.807 |
| D | 6 | RMAHA | 0.325 | 0.838 | 0.309 | 0.872 | 0.390 | 0.676 | 0.314 | 0.865 | 0.309 | 0.868 | 0.312 | 0.866 | 0.334 | 0.854 | 0.329 | 0.860 | 0.325 | 0.848 | 0.298 | 0.883 | 0.310 | 0.870 | 0.347 | 0.762 |
| Part R. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. | 2 | ENERGY | 0.321 | 0.852 | 0 303 | 0.885 | 0.386 | 0.696 | 0.305 | 0.887 | 0.310 | 0.867 | 0.303 | 0.888 | 0.337 | 0.849 | 0.323 | 0.862 | 0.326 | 0.858 | 0.295 | 0.898 | 0.299 | 0.897 | 0.340 | 0 784 |
| VE ODAL C.330 O.830 O.830 O.837 O.340 O.830 O.837 O.340 O.830 O.837 O.340 O.830 O.837 O.340 O.830 O.330 O.8 | ÷ | MaxI | 0.220 | 0.052 | 0.202 | 0.005 | 0.296 | 0.605 | 0.205 | 0.007 | 0.207 | 0.007 | 0.204 | 0.000 | 0.226 | 0.052 | 0.222 | 0.062 | 0.225 | 0.050 | 0.202 | 0.000 | 0.200 | 0.007 | 0.220 | 0.707 |
| D DDIN 0.320 0.330 0.830 0.847 0.340 0.847 0.340 0.848 0.340 0.848 0.340 0.848 0.340 0.848 0.340 0.845 0.330 0.850 0.330 0.850 0.330 0.850 0.330 0.850 0.330 0.850 0.330 0.850 0.330 0.850 0.330 0.850 0.330 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.330 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 0.850 0.350 <t< td=""><td>A</td><td>MAXL</td><td>0.520</td><td>0.855</td><td>0.303</td><td>0.885</td><td>0.580</td><td>0.095</td><td>0.505</td><td>0.880</td><td>0.507</td><td>0.875</td><td>0.504</td><td>0.887</td><td>0.550</td><td>0.832</td><td>0.322</td><td>0.804</td><td>0.525</td><td>0.800</td><td>0.295</td><td>0.902</td><td>0.299</td><td>0.890</td><td>0.339</td><td>0.787</td></t<> | A | MAXL | 0.520 | 0.855 | 0.303 | 0.885 | 0.580 | 0.095 | 0.505 | 0.880 | 0.507 | 0.875 | 0.504 | 0.887 | 0.550 | 0.832 | 0.322 | 0.804 | 0.525 | 0.800 | 0.295 | 0.902 | 0.299 | 0.890 | 0.339 | 0.787 |
| Strep Old Old </td <td>Ξ.</td> <td>ODIN</td> <td>0.320</td> <td>0.853</td> <td>0.303</td> <td>0.885</td> <td>0.385</td> <td>0.694</td> <td>0.305</td> <td>0.886</td> <td>0.308</td> <td>0.872</td> <td>0.304</td> <td>0.887</td> <td>0.334</td> <td>0.852</td> <td>0.322</td> <td>0.864</td> <td>0.324</td> <td>0.859</td> <td>0.293</td> <td>0.902</td> <td>0.299</td> <td>0.896</td> <td>0.338</td> <td>0.786</td> | Ξ. | ODIN | 0.320 | 0.853 | 0.303 | 0.885 | 0.385 | 0.694 | 0.305 | 0.886 | 0.308 | 0.872 | 0.304 | 0.887 | 0.334 | 0.852 | 0.322 | 0.864 | 0.324 | 0.859 | 0.293 | 0.902 | 0.299 | 0.896 | 0.338 | 0.786 |
| VE U0.3200.3540.3600.8580.3690.3070.8820.3700.8820.3200.8670.3200.8670.3000.8300.3810.3510.3700.8820.3200.8670.3200.8670.3000.8810.3500.8780.3000.8840.3300.8810.3500.8780.3000.8860.3300.8840.330.8840.3300.8840.3300.8840.3300.8840.3300.8840.3300.8840.3300.8850.3850.3840.3400.8840.3300.8840.3300.8840.3300.8840.3300.8840.3300.8840.3300.8840.3300.8840.3300.8840.3300.8840.330 <th< td=""><td><u> </u></td><td>IGEOOD</td><td>0.320</td><td>0.854</td><td>0.303</td><td>0.885</td><td>0.383</td><td>0.701</td><td>0.305</td><td>0.887</td><td>0.308</td><td>0.871</td><td>0.304</td><td>0.888</td><td>0.336</td><td>0.851</td><td>0.322</td><td>0.863</td><td>0.326</td><td>0.859</td><td>0.293</td><td>0.901</td><td>0.299</td><td>0.897</td><td>0.337</td><td>0.789</td></th<> | <u> </u> | IGEOOD | 0.320 | 0.854 | 0.303 | 0.885 | 0.383 | 0.701 | 0.305 | 0.887 | 0.308 | 0.871 | 0.304 | 0.888 | 0.336 | 0.851 | 0.322 | 0.863 | 0.326 | 0.859 | 0.293 | 0.901 | 0.299 | 0.897 | 0.337 | 0.789 |
| E DOUCTOR 0.319 0.854 0.308 0.858 0.306 0.879 0.306 0.877 0.307 0.827 0.307 0.827 0.308 0.877 0.308 0.877 0.308 0.877 0.308 0.877 0.308 0.878 0.308 0.887 0.308 0.887 0.308 0.887 0.308 0.887 0.308 0.887 0.30 0.887 0.318 0.887 0.308 0.887 0.308 0.887 0.338 0.887 0.308 0.888 0.308 0.889 0.308 0.887 0.318 0.887 0.308 0.887 0.308 0.887 0.308 0.888 0.318 0.888 0.318 0.888 0.318 0.888 0.318 0.888 0.318 0.888 0.318 0.838 0.318 0.388 0.338 0.388 0.338 0.388 0.338 0.388 0.338 0.388 0.338 0.388 0.338 0.348 0.338 0.348 0.338 0.348 0. | × | MSP | 0.320 | 0.854 | 0.306 | 0.880 | 0.386 | 0.693 | 0.309 | 0.880 | 0.305 | 0.878 | 0.307 | 0.882 | 0 333 | 0.856 | 0.320 | 0.867 | 0 324 | 0.860 | 0.291 | 0.906 | 0.303 | 0.889 | 0 334 | 0 797 |
| 1000 WC 0.388 0.389 0.389 0.389 0.390 0.886 0.329 0.842 0.310 0.886 0.328 0.844 0.310 0.884 0.310 0.884 0.310 0.884 0.310 0.886 0.328 0.884 0.310 0.886 0.328 0.884 0.310 0.884 0.310 0.886 0.331 0.864 0.310 0.887 0.288 0.887 0.388 0.887 0.388 0.887 0.388 0.887 0.388 0.887 0.380 0.887 0.380 0.887 0.388 0.887 0.388 0.388 0.336 0.886 0.338 0.856 0.336 0.856 0.336 0.886 0.338 0.856 0.336 0.886 0.388 0.338 0.888 0.338 0.888 0.338 0.888 0.338 0.888 0.338 0.888 0.338 0.888 0.338 0.888 0.338 0.348 0.338 0.368 0.338 0.338 0.338 0.338 < | 2 | DOCTOR | 0.210 | 0.854 | 0.205 | 0.882 | 0.285 | 0.604 | 0.209 | 0.991 | 0.205 | 0.979 | 0.306 | 0.993 | 0.222 | 0.857 | 0.320 | 0.867 | 0.324 | 0.861 | 0.201 | 0.006 | 0.202 | 0.801 | 0.334 | 0.707 |
| 2 0000 0.387 0.340 0.887 0.340 0.886 0.349 0.845 0.330 0.886 0.330 0.885 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.88 | Ë. | DOCTOR | 0.517 | 0.054 | 0.505 | 0.002 | 0.505 | 0.074 | 0.500 | 0.001 | 0.505 | 0.070 | 0.500 | 0.005 | 0.332 | 0.057 | 0.520 | 0.007 | 0.524 | 0.001 | 0.271 | 0.900 | 0.302 | 0.071 | 0.554 | 0.777 |
| E MCos 0.308 0.378 0.349 0.384 0.321 0.884 0.301 0.897 0.323 0.856 0.331 0.876 0.281 0.295 0.344 0.877 0.281 0.895 0.288 0.893 0.332 0.856 0.336 0.857 0.281 0.295 0.344 0.871 0.285 0.887 0.288 0.893 0.332 0.856 0.348 0.777 0.282 0.891 0.32 0.856 0.348 0.777 0.280 0.891 0.323 0.856 0.348 0.777 0.358 0.872 0.388 0.331 0.857 0.348 0.345 0.856 0.296 0.981 0.331 0.857 0.348 0.345 0.356 0.296 0.380 0.331 0.857 0.348 0.351 0.847 0.348 0.851 0.344 0.456 0.297 0.308 0.331 0.855 0.246 0.345 0.356 0.236 0.857 0.330 0.857 0.338 0.857 | S | OURS | 0.308 | 0.879 | 0.300 | 0.893 | 0.319 | 0.823 | 0.312 | 0.885 | 0.294 | 0.899 | 0.309 | 0.886 | 0.328 | 0.864 | 0.330 | 0.851 | 0.306 | 0.883 | 0.295 | 0.902 | 0.310 | 0.886 | 0.288 | 0.894 |
| E Nu 0.306 0.880 0.302 0.887 0.312 0.887 0.315 0.875 0.279 0.276 0.301 0.887 0.279 0.286 0.330 0.886 0.333 0.886 0.335 0.887 0.310 0.887 0.279 0.296 0.301 0.888 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.886 0.330 0.346 0.485 0.340 0.486 0.400 0.320 0.886 0.390 0.340 0.885 0.330 0.887 0.340 0.880 0.340 0.885 0.340 0.484 0.440 0.852 0.341 0.849 0.345 0.855 0.296 0.990 0.346 0.855 0.346 0.845 0.346 0.855 0.346 0.845 0.346 0.855 0.296 0.990 0.301 0.880 0.330 0.857 0.330 0.855 0.330 0.855 0.336 0.855< | 2 | MCos | 0.308 | 0.878 | 0.304 | 0.884 | 0.321 | 0.816 | 0.306 | 0.882 | 0.301 | 0.894 | 0.301 | 0.890 | 0.332 | 0.859 | 0.334 | 0.860 | 0.313 | 0.876 | 0.281 | 0.925 | 0.304 | 0.887 | 0.289 | 0.890 |
| Mint 0.301 0.314 0.311 0.317 0.300 0.387 0.330 0.383 0.335 0.346 0.845 0.310 0.885 0.282 0.210 0.817 0.420 0.420 0.420 0.420 0.420 0.420 0.420 0.430 0.831 0.331 0.831 0.331 0.831 0.340 0.831 0.340 0.831 0.340 0.831 0.345 0.834 0.346 0.850 0.290 0.900 0.801 0.810 0.310 0.831 0.320 0.831 0.320 0.831 0.320 0.831 0.320 0.831 0.320 0.831 0.331 0.857 0.330 0.855 0.344 0.850 0.320 0.832 0.310 0.831 0.331 0.857 0.330 0.855 0.344 0.850 0.320 0.832 0.310 0.831 0.310 0.831 0.330 0.831 0.331 0.857 0.330 0.851 0.341 0.851 0.310 0.831 | _ | KNN | 0.306 | 0.880 | 0.302 | 0.887 | 0.317 | 0.824 | 0.304 | 0.886 | 0.302 | 0.893 | 0.298 | 0.893 | 0.332 | 0.856 | 0.335 | 0.857 | 0.315 | 0.875 | 0.279 | 0.926 | 0.301 | 0.891 | 0.287 | 0.895 |
| BRACT 0.337 0.337 0.337 0.330 <th< td=""><td></td><td>MAHA</td><td>0.305</td><td>0.801</td><td>0.314</td><td>0.871</td><td>0.280</td><td>0.917</td><td>0.310</td><td>0.877</td><td>0.302</td><td>0.905</td><td>0.304</td><td>0.886</td><td>0.338</td><td>0.853</td><td>0.346</td><td>0.845</td><td>0.310</td><td>0.885</td><td>0.282</td><td>0.926</td><td>0.310</td><td>0.877</td><td>0.262</td><td>0.960</td></th<> | | MAHA | 0.305 | 0.801 | 0.314 | 0.871 | 0.280 | 0.917 | 0.310 | 0.877 | 0.302 | 0.905 | 0.304 | 0.886 | 0.338 | 0.853 | 0.346 | 0.845 | 0.310 | 0.885 | 0.282 | 0.926 | 0.310 | 0.877 | 0.262 | 0.960 |
| Fight Act 0.411 0.117 0.344 0.834 0.572 0.486 0.320 0.835 0.330 0.837 0.426 0.70 0.400 0.370 0.448 0.346 0.848 0.346 0.856 0.390 0.830 | | MANA | 0.505 | 0.071 | 0.514 | 0.071 | 0.200 | 0.917 | 0.510 | 0.077 | 0.502 | 0.705 | 0.504 | 0.000 | 0.550 | 0.055 | 0.540 | 0.045 | 0.510 | 0.005 | 0.202 | 0.720 | 0.510 | 0.077 | 0.202 | 0.700 |
| ENROY 0.328 0.855 0.036 0.887 0.422 0.301 0.890 0.327 0.856 0.296 0.901 0.346 0.852 0.341 0.848 0.355 0.297 0.908 0.305 0.891 0.320 0.831 UBDO 0.326 0.855 0.356 0.857 0.426 0.852 0.341 0.849 0.345 0.856 0.296 0.908 0.305 0.891 0.320 0.838 UBDO 0.326 0.855 0.346 0.855 0.346 0.855 0.346 0.856 0.349 0.350 0.881 0.310 0.881 0.321 0.837 0.338 0.855 0.346 0.856 0.346 0.856 0.349 0.310 0.881 0.321 0.831 0.310 0.881 0.321 0.831 0.310 0.881 0.321 0.831 0.310 0.881 0.310 0.881 0.321 0.831 0.310 0.881 0.310 0.831 0.310 0.831 <td></td> <td>REACT</td> <td>0.411</td> <td>0.717</td> <td>0.344</td> <td>0.834</td> <td>0.532</td> <td>0.468</td> <td>0.400</td> <td>0.740</td> <td>0.352</td> <td>0.826</td> <td>0.398</td> <td>0.742</td> <td>0.402</td> <td>0.737</td> <td>0.455</td> <td>0.662</td> <td>0.384</td> <td>0.777</td> <td>0.409</td> <td>0.739</td> <td>0.418</td> <td>0.714</td> <td>0.429</td> <td>0.648</td> | | REACT | 0.411 | 0.717 | 0.344 | 0.834 | 0.532 | 0.468 | 0.400 | 0.740 | 0.352 | 0.826 | 0.398 | 0.742 | 0.402 | 0.737 | 0.455 | 0.662 | 0.384 | 0.777 | 0.409 | 0.739 | 0.418 | 0.714 | 0.429 | 0.648 |
| 000000 MaxL 0.328 0.885 0.386 0.326 0.887 0.296 0.340 0.882 0.341 0.849 0.345 0.856 0.396 0.989 0.310 0.839 0.320 0.855 0.346 0.856 0.396 0.891 0.310 0.839 0.326 0.857 0.336 0.857 0.336 0.857 0.336 0.851 0.316 0.830 0.325 0.851 0.344 0.854 0.399 0.910 0.316 0.881 0.316 0.881 0.317 0.874 0.301 0.887 0.336 0.855 0.344 0.854 0.399 0.911 0.307 0.881 0.325 0.821 0.322 0.851 0.346 0.851 0.324 0.881 0.321 0.822 0.316 0.881 0.321 0.821 0.821 0.821 0.821 0.831 0.881 0.321 0.831 0.321 0.831 0.321 0.831 0.321 0.831 0.321 0.331 0.841 0.851 | | ENERGY | 0.328 | 0.856 | 0.305 | 0.887 | 0.426 | 0.672 | 0.300 | 0.896 | 0.327 | 0.866 | 0.295 | 0.904 | 0.347 | 0.851 | 0.342 | 0.848 | 0.346 | 0.856 | 0 207 | 0.008 | 0.305 | 0.894 | 0.320 | 0.831 |
| DIN 0.232 0.233 0.235 0.236 0.246 0.246 0.246 0.247 0.248 0.248 0.248 0.248 0.248 0.248 0.248 0.248 0.248 0.248 0.246 0.256 0.246 0.248 0.246 0.247 0.286 0.217 0 | - | ODDI | 0.320 | 0.050 | 0.305 | 0.007 | 0.420 | 0.072 | 0.300 | 0.070 | 0.327 | 0.000 | 0.275 | 0.001 | 0.347 | 0.051 | 0.341 | 0.040 | 0.246 | 0.050 | 0.201 | 0.000 | 0.305 | 0.001 | 0.320 | 0.001 |
| T MaxL 0.328 0.885 0.305 0.887 0.426 0.890 0.326 0.886 0.303 0.888 0.419 0.526 0.880 0.325 0.880 0.887 0.326 0.886 0.303 0.888 0.310 0.888 0.323 0.870 0.335 0.885 0.344 0.855 0.344 0.856 0.844 0.856 0.888 0.838 0.858 0.344 0.855 0.344 0.856 0.844 0.856 0.844 0.856 0.844 0.856 0.848 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.888 0.330 0.880 0.330 0.880 0.330 0.880 0.330 0.880 0.34 | 8 | ODIN | 0.328 | 0.855 | 0.305 | 0.887 | 0.426 | 0.670 | 0.301 | 0.893 | 0.326 | 0.867 | 0.296 | 0.901 | 0.540 | 0.852 | 0.541 | 0.849 | 0.345 | 0.850 | 0.296 | 0.908 | 0.305 | 0.891 | 0.320 | 0.828 |
| Every MSP 0.326 0.856 0.30 0.888 0.499 0.67 0.30 0.89 0.32 0.85 0.30 0.85 0.30 0.88 0.30 0.88 0.30 0.85 0.31 0.85 0.32 0.85 0.30 0.8 0.30 0.8 0.3 0.8 0.3 | | MAXL | 0.328 | 0.855 | 0.305 | 0.887 | 0.426 | 0.670 | 0.301 | 0.893 | 0.326 | 0.867 | 0.295 | 0.901 | 0.346 | 0.852 | 0.341 | 0.849 | 0.345 | 0.856 | 0.296 | 0.909 | 0.305 | 0.891 | 0.321 | 0.827 |
| L MSP 0.326 0.852 0.340 0.857 0.335 0.855 0.344 0.854 0.293 0.910 0.310 0.880 0.322 0.887 0.335 0.855 0.344 0.856 0.293 0.911 0.310 0.880 0.324 0.813 0.355 0.844 0.556 0.293 0.911 0.310 0.880 0.324 0.813 0.355 0.344 0.856 0.290 0.911 0.310 0.882 0.324 0.813 0.310 0.882 0.320 0.884 0.310 0.884 0.320 0.884 0.310 0.884 0.310 0.884 0.310 0.884 0.310 0.884 0.310 0.884 0.310 0.884 0.310 0.887 0.331 0.861 0.310 0.881 0.317 0.871 0.311 0.871 0.324 0.813 0.360 0.377 0.276 0.277 0.290 0.880 0.370 0.310 0.861 0.317 0.871 0.371 0.88 | Ř | IGEOOD | 0.326 | 0.856 | 0.303 | 0.888 | 0.419 | 0.675 | 0.300 | 0.894 | 0.323 | 0.870 | 0.295 | 0.902 | 0.344 | 0.852 | 0.340 | 0.850 | 0.345 | 0.856 | 0.294 | 0.911 | 0.305 | 0.893 | 0.320 | 0.828 |
| U Docrose 0.325 0.835 0.346 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.344 0.855 0.346 0.852 0.320 0.856 0.344 0.855 0.344 0.855 0.344 0.855 0.340 0.855 0.345 0.855 0.340 0.857 0.226 0.856 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.320 0.850 0.310 0.350 0 | F/ | MSP | 0.326 | 0.852 | 0.306 | 0.882 | 0.409 | 0.678 | 0.305 | 0.881 | 0.317 | 0.874 | 0.301 | 0.887 | 0.338 | 0.857 | 0.335 | 0.855 | 0.344 | 0.854 | 0.293 | 0.910 | 0.310 | 0.880 | 0.325 | 0.810 |
| KLM 0.33 0.84 0.30 0.84 0.33 0.84 0.33 0.84 0.33 0.84 0.25 0.31 0.84 0.25 0.31 0.84 0.25 0.31 0.84 0.25 0.31 0.84 0.25 0.31 0.84 0.25 0.31 0.84 0.25 0.31 0.84 0.25 0.31 0.84 0.25 0.31 0.84 0.25 0.34 0.85 0.32 0.85 0.32 0.85 0.32 0.85 0.32 0.85 0.32 0.85 0.32 0.85 0.32 0.85 0.32 0.85 0.32 0.85 0.32 0.32 0.35 | 5 | DOCTOR | 0.325 | 0.852 | 0.205 | 0.993 | 0.408 | 0.692 | 0.205 | 0.882 | 0.217 | 0.874 | 0.201 | 0.880 | 0.220 | 0.959 | 0.224 | 0.855 | 0.244 | 0.856 | 0.202 | 0.011 | 0.210 | 0.991 | 0.224 | 0.912 |
| A: LAM 0.316 0.881 0.391 0.882 0.322 0.872 0.379 0.888 0.343 0.838 0.340 0.838 0.300 0.881 0.301 0.882 0.300 0.871 0.310 0.882 0.300 0.871 0.310 0.884 0.301 0.884 0.303 0.836 0.330 0.836 0.330 0.836 0.322 0.871 0.330 0.861 0.322 0.871 0.322 0.871 0.322 0.871 0.330 0.861 0.322 0.870 0.330 0.864 0.311 0.874 0.294 0.888 0.390 0.831 0.831 0.831 0.331 0.864 0.310 0.831 0.330 0.865 0.372 0.898 0.299 0.888 0.360 0.330 0.861 0.330 0.861 0.330 0.861 0.330 0.861 0.330 0.861 0.330 0.861 0.330 0.861 0.330 0.861 0.330 0.861 0.330 0.861 < | ¥ | DUCTOR | 0.323 | 0.855 | 0.505 | 0.885 | 0.408 | 0.082 | 0.305 | 0.882 | 0.317 | 0.074 | 0.501 | 0.009 | 0.559 | 0.858 | 0.554 | 0.855 | 0.344 | 0.850 | 0.295 | 0.911 | 0.510 | 0.001 | 0.324 | 0.815 |
| L OURSE 0.315 0.854 0.327 0.299 0.881 0.294 0.900 0.302 0.885 0.328 0.465 0.312 0.882 0.300 0.885 0.317 0.870 0.300 0.889 0.320 0.885 0.327 0.856 0.282 0.870 0.320 0.880 0.300 0.885 0.322 0.870 0.330 0.880 0.300 0.885 0.228 0.880 0.320 0.889 0.320 0.880 0.320 0.881 0.321 0.871 0.336 0.864 0.314 0.878 0.276 0.290 0.880 0.290 0.880 0.290 0.881 0.320 0.831 0.361 0.837 0.321 0.831 0.864 0.311 0.832 0.391 0.333 0.840 0.432 0.440 0.836 0.447 0.882 0.361 0.347 0.832 0.391 0.333 0.840 0.337 0.840 0.341 0.341 0.341 0.341 0.341 0.3 | ě | KL M | 0.323 | 0.854 | 0.307 | 0.881 | 0.391 | 0.692 | 0.306 | 0.882 | 0.322 | 0.872 | 0.299 | 0.888 | 0.333 | 0.858 | 0.344 | 0.853 | 0.332 | 0.858 | 0.290 | 0.911 | 0.307 | 0.882 | 0.322 | 0.814 |
| V Marka 0.315 0.884 0.300 0.887 0.302 0.897 0.302 0.875 0.324 0.867 0.329 0.862 0.320 0.878 0.288 0.910 0.305 0.877 0.278 0.299 0.886 0.201 0.881 0.361 0.371 0.335 0.861 0.310 0.871 0.335 0.861 0.371 0.835 0.278 0.282 0.373 0.850 0.299 0.880 0.261 0.371 0.335 0.361 0.347 0.880 0.283 0.361 0.347 0.880 0.361 0.347 0.880 0.331 0.841 0.361 0.347 0.880 0.361 0.341 0.8 | É | OURS | 0.316 | 0.865 | 0.289 | 0.913 | 0.367 | 0.729 | 0.309 | 0.881 | 0.294 | 0.906 | 0.305 | 0.885 | 0.328 | 0.865 | 0.342 | 0.838 | 0.310 | 0.882 | 0.302 | 0.895 | 0.317 | 0.871 | 0.310 | 0.848 |
| B Core 0.336 0.877 0.296 0.893 0.322 0.870 0.336 0.871 0.296 0.893 0.322 0.870 0.336 0.871 0.278 0.277 0.297 0.880 0.297 0.882 0.237 0.835 0.347 0.881 0.337 0.884 0.317 0.310 0.336 0.336 0.337 0.885 0.317 0.336 0.84 | z | RMAHA | 0.315 | 0.854 | 0.300 | 0.883 | 0.367 | 0.714 | 0.305 | 0.870 | 0.302 | 0.890 | 0.302 | 0.875 | 0.324 | 0.867 | 0.329 | 0.862 | 0.320 | 0.856 | 0.285 | 0.910 | 0.305 | 0.871 | 0.327 | 0.798 |
| KUSS 0.000 0.877 0.238 0.896 0.228 0.894 0.294 0.895 0.221 0.894 0.297 0.889 0.297 0.889 0.297 0.889 0.297 0.889 0.297 0.889 0.297 0.889 0.297 0.889 0.298 0.889 0.210 0.871 0.315 0.864 0.214 0.878 0.237 0.885 0.228 0.889 0.290 0.885 0.212 0.871 0.315 0.864 0.214 0.878 0.237 0.885 0.228 0.885 0.212 0.885 0.321 0.871 0.335 0.841 0.885 0.422 0.885 0.421 0.885 0.421 0.885 0.421 0.885 0.421 0.885 0.421 0.885 0.421 0.885 0.421 0.880 0.370 0.841 0.381 0.380 0.831 0.380 0.381 0.381 0.381 0.381 0.381 0.381 0.381 0.381 0.373 0.884 | ES | MCos | 0.306 | 0.877 | 0.206 | 0.803 | 0.329 | 0.700 | 0.200 | 0.886 | 0.202 | 0.803 | 0.206 | 0.901 | 0 2 2 2 | 0.870 | 0.226 | 0.863 | 0.212 | 0.979 | 0.278 | 0.027 | 0.208 | 0.880 | 0.207 | 0.862 |
| KNN 0.304 0.879 0.294 0.896 0.327 0.929 0.290 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.294 0.884 0.373 0.884 0.284 0.894 0.399 0.832 0.391 0.836 0.347 0.891 0.373 0.848 0.766 0.884 0.414 0.810 0.375 0.836 0.347 0.891 0.373 0.848 0.764 0.324 0DIN 0.452 0.746 0.484 0.341 0.883 0.366 0.884 0.419 0.810 0.373 0.848 0.467 0.373 0.844 0.441 0.883 0.366 0.884 0.373 0.844< | К | MCOS | 0.300 | 0.077 | 0.290 | 0.895 | 0.328 | 0.790 | 0.299 | 0.880 | 0.302 | 0.895 | 0.290 | 0.091 | 0.322 | 0.870 | 0.550 | 0.805 | 0.512 | 0.878 | 0.278 | 0.927 | 0.298 | 0.009 | 0.297 | 0.802 |
| MARA 0.302 0.884 0.294 0.885 0.292 0.885 0.228 0.889 0.220 0.881 0.335 0.863 0.306 0.885 0.278 0.925 0.299 0.886 0.283 0.891 0.335 0.832 0.392 0.836 0.347 0.892 0.373 0.850 0.764 0.325 MAXL 0.452 0.746 0.466 0.819 0.803 0.252 0.372 0.852 0.354 0.883 0.366 0.855 0.422 0.800 0.332 0.392 0.836 0.347 0.891 0.373 0.849 0.763 0.324 MAXL 0.452 0.746 0.466 0.817 0.830 0.353 0.494 0.404 0.330 0.357 0.484 0.423 0.366 0.837 0.335 0.337 0.847 0.339 0.891 0.373 0.847 0.330 0.871 0.336 0.870 0.336 0.870 0.336 0.837 0.343 0.868 | | KNN | 0.304 | 0.879 | 0.294 | 0.896 | 0.327 | 0.792 | 0.298 | 0.890 | 0.300 | 0.894 | 0.294 | 0.895 | 0.321 | 0.870 | 0.331 | 0.864 | 0.314 | 0.878 | 0.276 | 0.929 | 0.297 | 0.892 | 0.296 | 0.864 |
| ENERGY 0.453 0.746 0.466 0.818 0.803 0.252 0.372 0.834 0.354 0.884 0.366 0.855 0.422 0.808 0.379 0.832 0.392 0.836 0.347 0.892 0.373 0.849 0.764 0.325 ODIN 0.452 0.746 0.466 0.819 0.810 0.379 0.832 0.390 0.836 0.347 0.891 0.373 0.849 0.763 0.324 ODIN 0.452 0.746 0.464 0.810 0.379 0.832 0.390 0.836 0.347 0.891 0.373 0.848 0.763 0.324 US 0.441 0.756 0.344 0.346 0.830 0.357 0.830 0.373 0.848 0.366 0.830 0.373 0.848 0.366 0.831 0.366 0.830 0.373 0.830 0.373 0.830 0.373 0.838 0.364 0.830 0.373 0.838 0.361 0.361 | | MAHA | 0.302 | 0.884 | 0.294 | 0.897 | 0.307 | 0.834 | 0.299 | 0.885 | 0.298 | 0.898 | 0.296 | 0.889 | 0.321 | 0.871 | 0.335 | 0.863 | 0.306 | 0.885 | 0.278 | 0.925 | 0.299 | 0.886 | 0.283 | 0.894 |
| ENERGY 0.435 0.446 0.440 0.819 0.803 0.222 0.835 0.422 0.836 0.347 0.839 0.72 0.835 0.224 0.351 0.836 0.347 0.833 0.353 0.347 0.830 0.353 0.347 0.337 0.836 0.347 0.336 0.347 0.337 0.836 0.347 0.833 0.357 0.836 0.440 0.837 0.337 0.833 0.377 0.833 0.377 0.833 0.337 0.838 0.367 0.833 0.336 <th< td=""><td></td><td>E.m.</td><td>0.452</td><td>0.746</td><td>0.400</td><td>0.010</td><td>0.002</td><td>0.050</td><td>0.272</td><td>0.054</td><td>0.254</td><td>0.004</td><td>0.244</td><td>0.055</td><td>0.400</td><td>0.000</td><td>0.270</td><td>0.022</td><td>0.202</td><td>0.027</td><td>0.247</td><td>0.000</td><td>0.272</td><td>0.050</td><td>0.764</td><td>0.225</td></th<> | | E.m. | 0.452 | 0.746 | 0.400 | 0.010 | 0.002 | 0.050 | 0.272 | 0.054 | 0.254 | 0.004 | 0.244 | 0.055 | 0.400 | 0.000 | 0.270 | 0.022 | 0.202 | 0.027 | 0.247 | 0.000 | 0.272 | 0.050 | 0.764 | 0.225 |
| MAXL 0.452 0.746 0.406 0.819 0.837 0.833 0.374 0.419 0.810 0.379 0.832 0.391 0.837 0.849 0.733 0.848 0.746 0.845 0.441 0.845 0.340 0.733 0.848 0.733 0.848 0.733 0.848 0.733 0.848 0.747 0.849 0.733 0.848 0.747 0.849 0.733 0.848 0.733 0.848 0.733 0.848 0.733 0.848 0.733 0.848 0.733 0.848 | | ENERGY | 0.453 | 0.746 | 0.406 | 0.818 | 0.803 | 0.252 | 0.372 | 0.854 | 0.354 | 0.884 | 0.300 | 0.855 | 0.422 | 0.808 | 0.379 | 0.832 | 0.392 | 0.830 | 0.347 | 0.892 | 0.373 | 0.850 | 0.764 | 0.325 |
| ODIN 0.452 0.746 0.406 0.810 0.372 0.831 0.379 0.832 0.370 0.832 0.370 0.832 0.370 0.832 0.370 0.832 0.371 0.831 0.373 0.848 0.745 0.324 IGEODD 0.441 0.756 0.394 0.830 0.733 0.844 0.741 0.830 0.535 0.837 0.844 0.339 0.897 0.335 0.837 0.844 0.333 0.745 0.855 0.833 0.740 0.844 0.733 0.833 0.744 0.400 DOCTOR 0.431 0.773 0.846 0.357 0.346 0.840 0.337 0.833 0.740 0.846 0.335 0.833 0.370 0.844 0.441 0.650 0.357 0.846 0.336 0.831 0.370 0.846 0.336 0.831 0.370 0.846 0.336 0.834 0.361 0.841 0.414 0.655 0.444 0.414 0.655 0.454< | | MAXL | 0.452 | 0.746 | 0.406 | 0.819 | 0.803 | 0.251 | 0.372 | 0.853 | 0.354 | 0.883 | 0.366 | 0.854 | 0.419 | 0.810 | 0.379 | 0.832 | 0.391 | 0.836 | 0.347 | 0.891 | 0.373 | 0.849 | 0.763 | 0.324 |
| 0 REACT 0.451 0.740 0.384 0.826 0.447 0.801 0.367 0.840 0.753 0.533 0.540 0.378 0.837 0.425 0.737 0.838 0.467 0.441 0.755 0.389 0.830 0.533 0.540 0.378 0.847 0.335 0.873 0.425 0.373 0.841 0.373 0.841 0.373 0.841 0.373 0.841 0.373 0.833 0.703 0.835 0.871 0.845 0.430 0.773 0.838 0.733 0.831 0.733 0.831 0.733 0.835 0.733 0.835 0.871 0.385 0.864 0.387 0.834 0.369 0.833 0.370 0.846 0.335 0.857 0.464 0.350 0.557 0.464 0.350 0.557 0.464 0.350 0.357 0.356 0.851 0.366 0.845 0.341 0.853 0.366 0.830 0.357 0.833 0.356 0.837 0.835 0.3 | | ODIN | 0.452 | 0.746 | 0.406 | 0.819 | 0.801 | 0.252 | 0.372 | 0.852 | 0.354 | 0.883 | 0.366 | 0.854 | 0.419 | 0.810 | 0.379 | 0.832 | 0.390 | 0.836 | 0.347 | 0.891 | 0.373 | 0.848 | 0.763 | 0.324 |
| IGEODD 0.441 0.756 0.394 0.830 0.792 0.267 0.363 0.859 0.346 0.859 0.402 0.825 0.370 0.840 0.378 0.847 0.339 0.897 0.365 0.854 0.745 0.351 DOCTOR 0.431 0.770 0.843 0.370 0.844 0.337 0.833 0.373 0.838 0.744 0.400 DOCTOR 0.431 0.773 0.846 0.346 0.844 0.341 0.858 0.857 0.366 0.844 0.387 0.833 0.370 0.846 0.335 0.833 0.373 0.838 0.744 0.400 UERS 0.311 0.751 0.346 0.357 0.846 0.336 0.835 0.355 0.858 0.342 0.890 0.335 0.856 0.344 0.857 0.346 0.856 0.346 0.356 0.856 0.344 0.857 0.343 0.360 0.341 0.460 0.355 0.355 0.356 <td>8</td> <td>REACT</td> <td>0.451</td> <td>0.740</td> <td>0.384</td> <td>0.826</td> <td>0.649</td> <td>0.369</td> <td>0.417</td> <td>0.801</td> <td>0.367</td> <td>0.864</td> <td>0.421</td> <td>0.795</td> <td>0.389</td> <td>0.830</td> <td>0.553</td> <td>0.694</td> <td>0.404</td> <td>0.830</td> <td>0.358</td> <td>0.873</td> <td>0.425</td> <td>0.795</td> <td>0.588</td> <td>0.467</td> | 8 | REACT | 0.451 | 0.740 | 0.384 | 0.826 | 0.649 | 0.369 | 0.417 | 0.801 | 0.367 | 0.864 | 0.421 | 0.795 | 0.389 | 0.830 | 0.553 | 0.694 | 0.404 | 0.830 | 0.358 | 0.873 | 0.425 | 0.795 | 0.588 | 0.467 |
| MSP 0.432 0.574 0.536 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.537 0.538 0.527 0.538 0.527 0.538 0.527 0.537 0 | | ICEOOD | 0.441 | 0.756 | 0.204 | 0.830 | 0.702 | 0.267 | 0.262 | 0.850 | 0.246 | 0.000 | 0.360 | 0.850 | 0.402 | 0.825 | 0.270 | 0.840 | 0.279 | 0.847 | 0.220 | 0.807 | 0.265 | 0.854 | 0.745 | 0.251 |
| Mart U-32 0.700 0.379 0.373 0.831 0.366 0.844 0.341 0.885 0.368 0.840 0.833 0.309 0.833 0.370 0.849 0.373 0.839 0.774 0.400 DOCTOR 0.431 0.776 0.357 0.836 0.341 0.885 0.366 0.844 0.337 0.838 0.373 0.839 0.774 0.401 UERS 0.391 0.793 0.836 0.851 0.566 0.844 0.371 0.839 0.774 0.401 0.460 VER 0.376 0.845 0.367 0.846 0.361 0.844 0.375 0.888 0.336 0.830 0.373 0.889 0.373 0.889 0.373 0.889 0.313 0.900 0.341 0.860 0.356 0.846 0.341 0.860 0.356 0.846 0.341 0.860 0.356 0.342 0.861 0.341 0.855 0.446 0.355 0.446 0.355 | Å | MOD | 0.441 | 0.750 | 0.354 | 0.030 | 0.192 | 0.207 | 0.303 | 0.0.19 | 0.340 | 0.000 | 0.300 | 0.019 | 0.402 | 0.023 | 0.370 | 0.040 | 0.378 | 0.047 | 0.339 | 0.07/ | 0.303 | 0.004 | 0.743 | 0.351 |
| UCTOR 0.431 0.761 0.379 0.834 0.737 0.177 0.367 0.845 0.341 0.384 0.369 0.833 0.370 0.846 0.335 0.893 0.733 0.839 0.704 0.401 OURS 0.374 0.376 0.816 0.570 0.455 0.857 0.356 0.854 0.846 0.315 0.857 0.838 0.327 0.835 0.852 0.514 0.555 0.858 0.322 0.990 0.338 0.822 0.990 0.338 0.852 0.541 0.556 0.841 0.440 0.556 0.845 0.341 0.855 0.488 0.321 0.990 0.337 0.880 0.322 0.887 0.337 0.885 0.343 0.855 0.343 0.857 0.341 0.846 0.341 0.846 0.342 0.855 0.343 0.857 0.341 0.848 0.341 0.857 0.341 0.846 0.342 0.857 0.343 0.870 0.313 0.90 | F/ | MSP | 0.432 | 0.760 | 0.379 | 0.839 | 0.753 | 0.315 | 0.367 | 0.844 | 0.341 | 0.883 | 0.368 | 0.840 | 0.387 | 0.833 | 0.369 | 0.832 | 0.370 | 0.845 | 0.336 | 0.891 | 0.373 | 0.838 | 0.704 | 0.400 |
| 5 0 UR8 0.391 0.793 0.358 0.857 0.464 0.357 0.864 0.372 0.846 0.415 0.795 0.355 0.888 0.322 0.902 0.388 0.822 0.910 0.381 0.841 0.414 0.655 KLM 0.367 0.846 0.336 0.881 0.336 0.881 0.336 0.848 0.335 0.835 0.635 0.848 0.341 0.840 0.841 0.414 0.662 MCos 0.358 0.828 0.361 0.840 0.331 0.886 0.332 0.887 0.337 0.886 0.342 0.885 0.342 0.881 0.331 0.908 0.334 0.846 0.420 0.855 0.344 0.840 0.341 0.866 0.355 0.342 0.831 0.330 0.334 0.887 0.332 0.877 0.332 0.887 0.333 0.887 0.333 0.887 0.343 0.880 0.331 0.908 0.332 0.871 | IJ | DOCTOR | 0.431 | 0.761 | 0.379 | 0.840 | 0.753 | 0.317 | 0.367 | 0.845 | 0.341 | 0.885 | 0.368 | 0.841 | 0.387 | 0.834 | 0.369 | 0.833 | 0.370 | 0.846 | 0.335 | 0.893 | 0.373 | 0.839 | 0.704 | 0.401 |
| T KLM 0.367 0.816 0.374 0.841 0.419 0.650 0.357 0.846 0.336 0.883 0.361 0.841 0.375 0.837 0.357 0.835 0.363 0.848 0.324 0.844 0.366 0.844 0.414 0.666 MCos 0.356 0.824 0.366 0.855 0.468 0.336 0.836 0.341 0.855 0.434 0.858 0.444 0.656 MABA 0.356 0.831 0.358 0.458 0.434 0.856 0.342 0.886 0.344 0.856 0.444 0.666 MABA 0.356 0.831 0.358 0.636 0.342 0.857 0.343 0.864 0.390 0.344 0.414 0.665 MABA 0.350 0.858 0.438 0.865 0.342 0.855 0.343 0.851 0.340 0.811 0.313 0.907 0.313 0.909 0.342 0.846 0.325 0.331 0. | Š | OURS | 0.391 | 0.793 | 0.358 | 0.851 | 0.567 | 0.464 | 0.355 | 0.857 | 0.336 | 0.890 | 0.354 | 0.854 | 0.372 | 0.846 | 0.415 | 0.795 | 0.355 | 0.858 | 0.322 | 0.902 | 0.358 | 0.852 | 0.514 | 0.555 |
| 0 | ÷ | KL M | 0.367 | 0.816 | 0 374 | 0.841 | 0 4 1 0 | 0.650 | 0 357 | 0.846 | 0 336 | 0.883 | 0.361 | 0.841 | 0 375 | 0.837 | 0 357 | 0.835 | 0 363 | 0.848 | 0.324 | 0.804 | 0.361 | 0.841 | 0.414 | 0.662 |
| SMARK UNDUG 0.320 0.320 0.340 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.340 0.341 0.355 0.340 0.341 0.857 0.343 0.858 0.441 0.350 0.857 0.343 0.858 0.446 0.350 0.350 0.851 0.344 0.851 0.444 0.855 0.342 0.857 0.343 0.858 0.448 0.861 0.340 0.851 0.340 0.811 0.340 0.811 0.340 0.811 0.340 0.811 0.340 0.811 0.340 0.811 0.340 0.811 0.341 0.810 0.341 0.810 0.341 0.810 0.341 0.810 0.341 0.810 0.341 0.810 0.811 0.341 0.810 0.811 <th< td=""><td>Ó</td><td>DM</td><td>0.260</td><td>0.010</td><td>0.240</td><td>0.041</td><td>0.440</td><td>0.502</td><td>0.241</td><td>0.840</td><td>0.221</td><td>0.003</td><td>0.242</td><td>0.041</td><td>0.254</td><td>0.021</td><td>0.240</td><td>0.033</td><td>0.241</td><td>0.070</td><td>0.212</td><td>0.007</td><td>0.244</td><td>0.041</td><td>0.424</td><td>0.657</td></th<> | Ó | DM | 0.260 | 0.010 | 0.240 | 0.041 | 0.440 | 0.502 | 0.241 | 0.840 | 0.221 | 0.003 | 0.242 | 0.041 | 0.254 | 0.021 | 0.240 | 0.033 | 0.241 | 0.070 | 0.212 | 0.007 | 0.244 | 0.041 | 0.424 | 0.657 |
| MACS U.SS U.SS <thu.ss< th=""> U.SS U.SS <thu< td=""><td>õ</td><td>KWIAHA</td><td>0.500</td><td>0.624</td><td>0.500</td><td>0.833</td><td>0.408</td><td>0.380</td><td>0.341</td><td>0.803</td><td>0.321</td><td>0.904</td><td>0.342</td><td>0.838</td><td>0.554</td><td>0.801</td><td>0.549</td><td>0.645</td><td>0.541</td><td>0.870</td><td>0.515</td><td>0.907</td><td>0.544</td><td>0.838</td><td>0.420</td><td>0.057</td></thu<></thu.ss<> | õ | KWIAHA | 0.500 | 0.624 | 0.500 | 0.833 | 0.408 | 0.380 | 0.341 | 0.803 | 0.321 | 0.904 | 0.342 | 0.838 | 0.554 | 0.801 | 0.549 | 0.645 | 0.541 | 0.870 | 0.515 | 0.907 | 0.544 | 0.838 | 0.420 | 0.057 |
| MARA 0.356 0.831 0.360 0.888 0.438 0.631 0.341 0.865 0.342 0.855 0.343 0.855 0.343 0.870 0.315 0.901 0.342 0.864 0.399 0.709 KNN 0.353 0.838 0.857 0.447 0.614 0.332 0.877 0.325 0.876 0.353 0.855 0.340 0.861 0.340 0.871 0.315 0.901 0.342 0.874 0.415 0.673 KLM 0.226 0.921 0.944 0.185 0.987 0.230 0.918 0.222 0.924 0.210 0.961 0.223 0.911 0.225 0.926 0.229 0.916 0.226 0.917 0.193 0.223 0.927 0.709 Doctron 0.212 0.944 0.212 0.947 0.170 0.990 0.235 0.911 0.225 0.926 0.226 0.916 0.226 0.914 0.422 0.937 0.188 0.922 | ^ | MCos | 0.358 | 0.828 | 0.361 | 0.856 | 0.459 | 0.599 | 0.337 | 0.870 | 0.329 | 0.887 | 0.337 | 0.868 | 0.356 | 0.856 | 0.342 | 0.857 | 0.343 | 0.869 | 0.313 | 0.908 | 0.338 | 0.868 | 0.419 | 0.669 |
| KNN 0.353 0.833 0.358 0.857 0.447 0.614 0.332 0.871 0.332 0.876 0.333 0.856 0.340 0.861 0.340 0.871 0.310 0.912 0.334 0.874 0.415 0.673 KL M 0.226 0.932 0.243 0.931 0.185 0.987 0.213 0.918 0.226 0.916 0.227 0.918 0.226 0.917 0.919 0.913 0.922 0.914 0.212 0.947 0.213 0.911 0.133 0.877 0.213 0.910 0.223 0.910 0.225 0.926 0.229 0.915 0.217 0.990 0.237 0.910 0.225 0.926 0.229 0.916 0.226 0.918 0.226 0.918 0.210 0.971 0.193 0.223 0.916 0.237 0.916 0.226 0.918 0.212 0.937 0.188 0.882 0.221 0.930 0.223 0.916 0.237 0.920 0.221< | | MAHA | 0.356 | 0.831 | 0.360 | 0.858 | 0.438 | 0.631 | 0.341 | 0.865 | 0.332 | 0.879 | 0.342 | 0.861 | 0.357 | 0.855 | 0.345 | 0.853 | 0.343 | 0.870 | 0.315 | 0.901 | 0.342 | 0.864 | 0.395 | 0.709 |
| KLM 0.226 0.931 0.185 0.887 0.231 0.887 0.231 0.918 0.224 0.904 0.222 0.924 0.201 0.967 0.237 0.918 0.245 0.911 0.181 0.992 MSP 0.213 0.941 0.212 0.944 0.212 0.944 0.212 0.944 0.212 0.941 0.223 0.911 0.181 0.992 Doctron 0.212 0.944 0.212 0.944 0.221 0.941 0.223 0.927 0.70 0.938 0.220 0.931 0.223 0.927 0.70 0.990 0.223 0.911 0.225 0.926 0.226 0.916 0.226 0.916 0.226 0.916 0.221 0.937 0.188 0.982 0.221 0.940 0.224 0.936 0.164 0.990 VE Exercery 0.210 0.957 0.170 0.990 0.238 0.916 0.237 0.926 0.214 0.945 0.221 | | KNN | 0.353 | 0.833 | 0.358 | 0.857 | 0.447 | 0.614 | 0.332 | 0.877 | 0.325 | 0.891 | 0.332 | 0.876 | 0.353 | 0.856 | 0.340 | 0.861 | 0.340 | 0.871 | 0.310 | 0.912 | 0.334 | 0.874 | 0.415 | 0.673 |
| KLM 0.226 0.932 0.243 0.931 0.185 0.897 0.216 0.918 0.224 0.904 0.222 0.924 0.201 0.937 0.237 0.918 0.243 0.911 0.113 0.992 MSP 0.213 0.941 0.212 0.944 0.212 0.941 0.212 0.947 0.139 0.237 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.226 0.918 0.210 0.918 0.228 0.916 0.226 0.918 0.226 0.918 0.929 0.973 0.188 0.882 0.210 0.930 0.223 0.916 0.237 0.927 0.214 0.945 0.221 0.937 0.188 0.882 0.221 0.930 0.223 0.916 0.238 0.927 0.217 0.937 0.188 </td <td></td> <td>H</td> <td>0.555</td> <td>0.055</td> <td>0.550</td> <td>0.057</td> <td>0.117</td> <td>0.011</td> <td>0.552</td> <td>0.077</td> <td>0.525</td> <td>0.071</td> <td>0.552</td> <td>0.070</td> <td>0.555</td> <td>0.050</td> <td>0.510</td> <td>0.001</td> <td>0.510</td> <td>0.071</td> <td>0.510</td> <td>0.712</td> <td>0.551</td> <td>0.071</td> <td>0.115</td> <td>0.015</td> | | H | 0.555 | 0.055 | 0.550 | 0.057 | 0.117 | 0.011 | 0.552 | 0.077 | 0.525 | 0.071 | 0.552 | 0.070 | 0.555 | 0.050 | 0.510 | 0.001 | 0.510 | 0.071 | 0.510 | 0.712 | 0.551 | 0.071 | 0.115 | 0.015 |
| MSP 0.213 0.941 0.212 0.946 0.182 0.992 0.236 0.910 0.225 0.926 0.212 0.918 0.220 0.918 0.226 0.918 0.120 0.913 0.220 0.931 0.220 0.931 0.220 0.924 0.994 MAXL 0.211 0.944 0.121 0.994 0.121 0.994 0.121 0.994 0.121 0.994 0.121 0.994 0.124 0.946 0.211 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.946 0.221 0.947 0.220 0.948 0.820 0.210 0.940 0.224 0.340 0.224 0.340< | | KL M | 0.226 | 0.932 | 0.243 | 0.931 | 0.185 | 0.987 | 0.251 | 0.897 | 0.230 | 0.918 | 0.254 | 0.897 | 0.242 | 0.904 | 0.222 | 0.924 | 0.201 | 0.967 | 0.237 | 0.918 | 0.245 | 0.911 | 0.181 | 0.992 |
| OCTOR 0.212 0.942 0.212 0.947 0.179 0.993 0.235 0.911 0.225 0.926 0.919 0.226 0.918 0.192 0.974 0.219 0.933 0.222 0.934 0.229 0.914 0.926 0.919 0.226 0.918 0.192 0.974 0.219 0.933 0.222 0.936 0.164 0.994 ODIN 0.210 0.950 0.209 0.957 0.170 0.990 0.239 0.916 0.237 0.912 0.937 0.188 0.982 0.221 0.930 0.223 0.936 0.164 0.990 VE DIN 0.950 0.209 0.957 0.170 0.990 0.239 0.916 0.237 0.927 0.214 0.945 0.221 0.937 0.188 0.982 0.221 0.930 0.233 0.916 0.237 0.927 0.227 0.224 0.945 0.221 0.933 0.123 0.936 0.227 0.927 0.214 | | MSP | 0.213 | 0.941 | 0.212 | 0.946 | 0.182 | 0.992 | 0.236 | 0.910 | 0.225 | 0.926 | 0.229 | 0.915 | 0.227 | 0.918 | 0.226 | 0.917 | 0.193 | 0.973 | 0.220 | 0.931 | 0.223 | 0.927 | 0.170 | 0.994 |
| Dectors 0.112 0.742 0.117 0.753 0.123 0.911 0.223 0.926 0.124 0.915 0.112 0.937 0.129 0.914 0.119 0.937 0.124 0.941 0.119 0.937 0.124 0.941 0.119 0.937 0.124 0.936 0.124 0.936 0.124 0.936 0.124 0.936 0.124 0.936 0.124 0.937 0.188 0.982 0.221 0.940 0.224 0.936 0.164 0.990 K N 0.210 0.950 0.209 0.957 0.170 0.990 0.238 0.929 0.227 0.926 0.214 0.946 0.221 0.937 0.188 0.982 0.221 0.940 0.223 0.936 0.162 0.990 K R N <td>~</td> <td>DOCTOR</td> <td>0.212</td> <td>0.042</td> <td>0.212</td> <td>0.947</td> <td>0.170</td> <td>0.002</td> <td>0.235</td> <td>0.011</td> <td>0.225</td> <td>0.026</td> <td>0.220</td> <td>0.016</td> <td>0.226</td> <td>0.010</td> <td>0.226</td> <td>0.019</td> <td>0.102</td> <td>0.074</td> <td>0.210</td> <td>0.032</td> <td>0.222</td> <td>0.028</td> <td>0.164</td> <td>0.004</td> | ~ | DOCTOR | 0.212 | 0.042 | 0.212 | 0.947 | 0.170 | 0.002 | 0.235 | 0.011 | 0.225 | 0.026 | 0.220 | 0.016 | 0.226 | 0.010 | 0.226 | 0.019 | 0.102 | 0.074 | 0.210 | 0.032 | 0.222 | 0.028 | 0.164 | 0.004 |
| → MAXL 0.211 0.950 0.209 0.957 0.172 0.990 0.239 0.916 0.237 0.929 0.212 0.946 0.221 0.937 0.188 0.882 0.221 0.940 0.223 0.936 0.167 0.990 ≤ OLIN 0.250 0.290 0.957 0.170 0.990 0.237 0.928 0.227 0.226 0.214 0.945 0.221 0.937 0.188 0.982 0.221 0.930 0.223 0.936 0.164 0.990 ≤ DERGY 0.210 0.950 0.209 0.957 0.170 0.990 0.237 0.916 0.237 0.925 0.929 0.212 0.947 0.218 0.940 0.188 0.982 0.221 0.930 0.233 0.916 0.237 0.926 0.227 0.926 0.211 0.937 0.188 0.980 0.211 0.936 0.163 0.917 0.103 0.916 0.223 0.936 0.161 < | õ | DOCTOR | 0.212 | 0.942 | 0.212 | 0.947 | 0.179 | 0.393 | 0.233 | 0.911 | 0.223 | 0.920 | 0.229 | 0.910 | 0.220 | 0.919 | 0.220 | 0.710 | 0.192 | 0.7/4 | 0.219 | 0.933 | 0.222 | 0.920 | 0.104 | 0.394 |
| \$\begin{bmatrix}{2} & DDIN 0.210 0.950 0.209 0.977 0.170 0.990 0.239 0.916 0.237 0.929 0.227 0.926 0.214 0.945 0.221 0.937 0.188 0.982 0.220 0.940 0.223 0.936 0.164 0.990 \$\begin{bmatrix}{2} & BARCT 0.210 0.955 0.170 0.990 0.239 0.916 0.238 0.929 0.227 0.927 0.214 0.945 0.228 0.988 0.188 0.982 0.221 0.940 0.223 0.936 0.166 0.990 \$\begin{bmatrix}{2} & BARCT 0.901 0.957 0.170 0.989 0.233 0.920 0.227 0.947 0.212 0.940 0.188 0.982 0.221 0.940 0.188 0.982 0.210 0.940 0.123 0.930 0.123 0.910 0.212 0.947 0.210 0.948 0.188 0.980 0.211 0.940 0.166 0.983 0.160 0.930 0.210 | Ĭ. | MAXL | 0.211 | 0.950 | 0.209 | 0.957 | 0.172 | 0.990 | 0.239 | 0.916 | 0.237 | 0.929 | 0.226 | 0.928 | 0.214 | 0.946 | 0.221 | 0.937 | 0.189 | 0.982 | 0.221 | 0.940 | 0.224 | 0.936 | 0.167 | 0.990 |
| Σ Exers(v) 0.210 0.950 0.209 0.970 0.170 0.909 0.239 0.916 0.239 0.227 0.929 0.212 0.947 0.220 0.938 0.188 0.982 0.221 0.940 0.224 0.930 0.224 0.940 0.239 0.217 0.930 0.221 0.940 0.221 0.940 0.223 0.930 0.224 0.940 0.188 0.982 0.221 0.940 0.224 0.930 0.223 0.930 0.239 0.212 0.930 0.221 0.940 0.188 0.982 0.221 0.940 0.223 0.930 0.233 0.910 0.237 0.910 0.237 0.910 0.237 0.910 0.225 0.929 0.212 0.940 0.188 0.980 0.211 0.930 0.210 0.910 0.237 0.910 0.237 0.910 0.225 0.929 0.211 0.924 0.210 0.910 0.912 0.930 0.212 0.931 0.900 <th< td=""><td>Å.</td><td>ODIN</td><td>0.210</td><td>0.950</td><td>0.209</td><td>0.957</td><td>0.170</td><td>0.990</td><td>0.239</td><td>0.916</td><td>0.237</td><td>0.929</td><td>0.227</td><td>0.926</td><td>0.214</td><td>0.945</td><td>0.221</td><td>0.937</td><td>0.188</td><td>0.982</td><td>0.220</td><td>0.940</td><td>0.223</td><td>0.936</td><td>0.164</td><td>0.990</td></th<> | Å. | ODIN | 0.210 | 0.950 | 0.209 | 0.957 | 0.170 | 0.990 | 0.239 | 0.916 | 0.237 | 0.929 | 0.227 | 0.926 | 0.214 | 0.945 | 0.221 | 0.937 | 0.188 | 0.982 | 0.220 | 0.940 | 0.223 | 0.936 | 0.164 | 0.990 |
| D REACT 0.210 0.951 0.208 0.957 0.170 0.989 0.237 0.917 0.237 0.930 0.225 0.929 0.212 0.949 0.188 0.982 0.221 0.939 0.223 0.936 0.166 0.989 MAHA 0.208 0.941 0.205 0.944 0.128 0.940 0.188 0.982 0.221 0.939 0.223 0.936 0.166 0.989 MAHA 0.208 0.941 0.205 0.956 0.178 0.923 0.212 0.936 0.212 0.910 0.228 0.944 0.208 0.944 0.200 0.935 0.214 0.940 0.188 0.982 0.221 0.930 0.212 0.940 0.188 0.940 0.186 0.983 0.212 0.930 0.126 0.927 0.216 0.930 0.221 0.941 0.212 0.940 0.188 0.940 0.186 0.983 0.211 0.940 0.166 0.983 0.210 | ΕA | ENERGY | 0.210 | 0.950 | 0.209 | 0.957 | 0.170 | 0.990 | 0.239 | 0.916 | 0.238 | 0.929 | 0.227 | 0.927 | 0.214 | 0.947 | 0.220 | 0.938 | 0.188 | 0.982 | 0.221 | 0.940 | 0.224 | 0.936 | 0.162 | 0.990 |
| ψ κιπιτ 0.208 0.944 0.208 0.948 0.107 0.216 0.949 0.120 0.949 0.123 0.939 0.103 0.939 0.103 0.939 0.103 0.939 0.103 0.939 0.103 0.939 0.121 0.939 0.121 0.939 0.123 0.939 0.130 0.939 0.130 0.939 0.130 0.939 0.121 0.939 0.121 0.939 0.121 0.939 0.121 0.938 0.121 0.931 0.121 0.931 0.120 0.931 0.121 0. | Ξ | REACT | 0.210 | 0.951 | 0.208 | 0.957 | 0.170 | 0.980 | 0.237 | 0.917 | 0.237 | 0.930 | 0.225 | 0.920 | 0.212 | 0.940 | 0.218 | 0.940 | 0.188 | 0.982 | 0.221 | 0.930 | 0.223 | 0.936 | 0.166 | 0.980 |
| KMAHA Lob 0.494 0.495 0.495 0.416 0.925 0.216 0.925 0.216 0.925 0.216 0.926 0.216 0.926 0.216 0.926 0.216 0.936 0.218 0.940 0.126 0.944 0.208 0.944 0.200 0.936 0.210 0.940 0.212 0.938 0.190 L Outes 0.207 0.952 0.209 0.955 0.126 0.926 0.226 0.227 0.216 0.940 0.186 0.980 0.214 0.940 0.162 0.992 OUEs 0.202 0.957 0.209 0.955 0.179 0.982 0.218 0.940 0.162 0.992 0.178 0.936 0.214 0.945 0.188 0.980 0.207 0.950 0.218 0.940 0.162 0.992 MCos 0.197 0.66 0.201 0.947 0.201 0.947 0.201 0.947 0.208 0.950 0.188 0.980 < | S | DM | 0.200 | 0.041 | 0.200 | 0.042 | 0.102 | 0.062 | 0.210 | 0.022 | 0.210 | 0.020 | 0.215 | 0.020 | 0.222 | 0.011 | 0.200 | 0.044 | 0.200 | 0.052 | 0.210 | 0.040 | 0.212 | 0.020 | 0.102 | 0.060 |
| a lifeboor 0.207 0.992 0.209 0.920 0.225 0.920 0.226 0.927 0.216 0.943 0.216 0.940 0.186 0.983 0.214 0.945 0.214 0.945 0.186 0.992 0.216 0.992 0.216 0.940 0.126 0.940 0.126 0.992 0.216 0.940 0.128 0.992 0.216 0.940 0.216 0.940 0.128 0.940 0.128 0.940 0.124 0.940 0.218 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.124 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 0.128 0.940 <th< td=""><td>16</td><td>KWIAHA</td><td>0.208</td><td>0.941</td><td>0.205</td><td>0.948</td><td>0.192</td><td>0.903</td><td>0.218</td><td>0.923</td><td>0.210</td><td>0.930</td><td>0.213</td><td>0.930</td><td>0.222</td><td>0.911</td><td>0.208</td><td>0.944</td><td>0.200</td><td>0.933</td><td>0.210</td><td>0.940</td><td>0.212</td><td>0.938</td><td>0.193</td><td>0.900</td></th<> | 16 | KWIAHA | 0.208 | 0.941 | 0.205 | 0.948 | 0.192 | 0.903 | 0.218 | 0.923 | 0.210 | 0.930 | 0.213 | 0.930 | 0.222 | 0.911 | 0.208 | 0.944 | 0.200 | 0.933 | 0.210 | 0.940 | 0.212 | 0.938 | 0.193 | 0.900 |
| ↓ OURS 0.202 0.957 0.209 0.955 0.179 0.987 0.217 0.934 0.204 0.935 0.120 0.955 0.188 0.980 0.217 0.945 0.187 0.945 0.178 0.949 0.214 0.942 0.204 0.955 0.188 0.980 0.217 0.945 0.178 0.949 0.214 0.942 0.211 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.214 0.945 0.945 0.188 0.980 0.207 0.951 0.108 0.981 0.207 0.947 0.942 0.951 0.128 0.981 0.207 0.947 0.205 0.951 0.188 0.980 0.207 0.201 0.947 0.201 0.951 0.1 | B/ | IGEOOD | 0.207 | 0.952 | 0.209 | 0.956 | 0.173 | 0.992 | 0.235 | 0.920 | 0.226 | 0.936 | 0.226 | 0.927 | 0.215 | 0.943 | 0.216 | 0.940 | 0.186 | 0.983 | 0.214 | 0.945 | 0.218 | 0.940 | 0.162 | 0.992 |
| \$\bar{MCos}\$ 0.197 0.960 0.201 0.914 0.195 0.921 0.915 0.937 0.201 0.937 0.201 0.959 0.211 0.942 0.205 0.951 0.208 0.980 0.207 0.951 0.105 0.992 KNN 0.195 0.963 0.203 0.955 0.162 0.992 0.207 0.946 0.197 0.966 0.207 0.947 0.205 0.951 0.205 0.188 0.980 0.207 0.951 0.159 0.992 MAHA 0.194 0.964 0.199 0.964 0.192 0.942 0.197 0.966 0.207 0.947 0.205 0.951 0.188 0.980 0.207 0.951 0.159 0.992 MAHA 0.194 0.964 0.193 0.991 0.210 0.942 0.199 0.962 0.207 0.948 0.200 0.960 0.203 0.957 0.188 0.946 0.204 0.956 0.208 0.951 0.158 <td>Ē</td> <td>OURS</td> <td>0.202</td> <td>0.957</td> <td>0.209</td> <td>0.955</td> <td>0.179</td> <td>0.987</td> <td>0.217</td> <td>0.934</td> <td>0.208</td> <td>0.949</td> <td>0.214</td> <td>0.939</td> <td>0.208</td> <td>0.945</td> <td>0.204</td> <td>0.953</td> <td>0.190</td> <td>0.978</td> <td>0.207</td> <td>0.950</td> <td>0.211</td> <td>0.945</td> <td>0.178</td> <td>0.986</td> | Ē | OURS | 0.202 | 0.957 | 0.209 | 0.955 | 0.179 | 0.987 | 0.217 | 0.934 | 0.208 | 0.949 | 0.214 | 0.939 | 0.208 | 0.945 | 0.204 | 0.953 | 0.190 | 0.978 | 0.207 | 0.950 | 0.211 | 0.945 | 0.178 | 0.986 |
| KNN 0.195 0.963 0.203 0.955 0.162 0.974 0.197 0.966 0.207 0.947 0.205 0.951 0.105 0.971 0.106 0 | 2 | MCos | 0.197 | 0.960 | 0.201 | 0.961 | 0.159 | 0.992 | 0.213 | 0.937 | 0.201 | 0.959 | 0.211 | 0.942 | 0.205 | 0.951 | 0.208 | 0.950 | 0.188 | 0.980 | 0.207 | 0.951 | 0.210 | 0.947 | 0.159 | 0.992 |
| KAN 0.125 0.203 0.203 0.203 0.203 0.303 0.103 0.931 0.206 0.932 0.117 0.992 MAHA 0.194 0.964 0.119 0.940 0.127 0.947 0.203 0.931 0.203 0.931 0.203 0.931 0.203 0.931 0.203 0.931 0.203 0.931 0.204 0.932 0.157 0.992 MAHA 0.194 0.964 0.163 0.991 0.210 0.942 0.199 0.962 0.207 0.948 0.200 0.950 0.203 0.957 0.187 0.984 0.204 0.956 0.208 0.951 0.158 0.991 | | KNN | 0.105 | 0.062 | 0.202 | 0.055 | 0.162 | 0.002 | 0.207 | 0.046 | 0.107 | 0.066 | 0.207 | 0.047 | 0.205 | 0.051 | 0.205 | 0.055 | 0.199 | 0.081 | 0.202 | 0.057 | 0.206 | 0.052 | 0.157 | 0.002 |
| MAHA 0.194 0.964 0.199 0.964 0.163 0.991 0.210 0.942 0.199 0.962 0.207 0.948 0.200 0.960 0.203 0.957 0.187 0.984 0.204 0.956 0.208 0.951 0.158 0.991 | | IN IN IN | 0.195 | 0.903 | 0.203 | 0.935 | 0.102 | 0.992 | 0.207 | 0.940 | 0.19/ | 0.900 | 0.207 | 0.947 | 0.203 | 0.951 | 0.203 | 0.933 | 0.168 | 0.981 | 0.203 | 0.957 | 0.200 | 0.952 | 0.15/ | 0.992 |
| | | MAHA | 0.194 | 0.964 | 0.199 | 0.964 | 0.163 | 0.991 | 0.210 | 0.942 | 0.199 | 0.962 | 0.207 | 0.948 | 0.200 | 0.960 | 0.203 | 0.957 | 0.187 | 0.984 | 0.204 | 0.956 | 0.208 | 0.951 | 0.158 | 0.991 |

Table 6: Comparative analysis of AURC in the black-box SCOD framework between 12 existing OOD detection methods and our method (combining the other 12 methods) for CIFAR-100. Results are sorted in descending order by average AURC.

Table 7: Comparative analysis of AURC in the black-box SCOD framework between 12 existing OOD detection methods and our method (combining the other 12 methods) for a few models trained on ImageNet. Results are sorted in descending order by average AURC.

| | | A | VG | IN | AT. | NIN | ICO | Ope | NIM. | PLA | CES | SPE | CIES | SSE | B (E) | SSE | B (H) | TE | EX. |
|---------------------------|----------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| | | RC | ROC |
| _ | MAHA | 0.439 | 0.686 | 0.441 | 0.657 | 0.440 | 0.689 | 0.439 | 0.695 | 0.475 | 0.622 | 0.428 | 0.694 | 0.402 | 0.743 | 0.491 | 0.626 | 0.395 | 0.764 |
| (ET) | KNN | 0.365 | 0.810 | 0.351 | 0.831 | 0.376 | 0.804 | 0.355 | 0.846 | 0.347 | 0.796 | 0.367 | 0.831 | 0.335 | 0.874 | 0.432 | 0.699 | 0.349 | 0.800 |
| GEN | RMAHA | 0.354 | 0.849 | 0.329 | 0.874 | 0.360 | 0.838 | 0.355 | 0.854 | 0.368 | 0.837 | 0.333 | 0.881 | 0.337 | 0.863 | 0.400 | 0.793 | 0.350 | 0.854 |
| MAG | MCos | 0.350 | 0.872 | 0.310 | 0.929 | 0.368 | 0.838 | 0.342 | 0.890 | 0.347 | 0.873 | 0.355 | 0.870 | 0.337 | 0.888 | 0.427 | 0.750 | 0.314 | 0.940 |
| 1.1 | ENERGY | 0.348 | 0.875 | 0.307 | 0.928 | 0.365 | 0.840 | 0.332 | 0.897 | 0.334 | 0.909 | 0.356 | 0.867 | 0.339 | 0.883 | 0.413 | 0.784 | 0.341 | 0.894 |
| -12 | OURS | 0.343 | 0.882 | 0.314 | 0.909 | 0.353 | 0.864 | 0.329 | 0.899 | 0.340 | 0.915 | 0.338 | 0.889 | 0.329 | 0.895 | 0.404 | 0.800 | 0.318 | 0.833 |
| VET | KL M | 0.340 | 0.883 | 0.314 | 0.923 | 0.351 | 0.866 | 0.344 | 0.884 | 0.322 | 0.897 | 0.339 | 0.886 | 0.312 | 0.905 | 0.406 | 0.810 | 0.328 | 0.894 |
| SE | Igeood | 0.335 | 0.881 | 0.306 | 0.929 | 0.351 | 0.851 | 0.319 | 0.902 | 0.318 | 0.910 | 0.343 | 0.871 | 0.318 | 0.905 | 0.399 | 0.785 | 0.329 | 0.898 |
| OEN | MAXL | 0.334 | 0.880 | 0.307 | 0.928 | 0.345 | 0.851 | 0.317 | 0.901 | 0.319 | 0.914 | 0.342 | 0.870 | 0.322 | 0.892 | 0.400 | 0.789 | 0.323 | 0.898 |
| Ι | MSP | 0.323 | 0.890 | 0.298 | 0.935 | 0.331 | 0.880 | 0.323 | 0.890 | 0.319 | 0.913 | 0.312 | 0.904 | 0.310 | 0.911 | 0.354 | 0.843 | 0.331 | 0.882 |
| | Μάμα | 0.440 | 0.676 | 0.419 | 0.691 | 0.431 | 0.684 | 0.427 | 0.709 | 0.466 | 0.617 | 0.436 | 0.675 | 0.409 | 0.728 | 0.527 | 0.575 | 0.405 | 0.728 |
| (L | KNN | 0.383 | 0.763 | 0.414 | 0.683 | 0.384 | 0.767 | 0.381 | 0.788 | 0.425 | 0.687 | 0.369 | 0.777 | 0.351 | 0.825 | 0.402 | 0.740 | 0.340 | 0.837 |
| NE | MCos | 0.338 | 0.839 | 0.321 | 0.857 | 0.356 | 0.807 | 0.340 | 0.852 | 0.353 | 0.799 | 0.327 | 0.851 | 0.326 | 0.859 | 0.375 | 0.780 | 0.301 | 0.905 |
| IAGI | OURS DM | 0.327 | 0.874 | 0.304 | 0.893 | 0.340 | 0.860 | 0.316 | 0.898 | 0.332 | 0.859 | 0.319 | 0.882 | 0.318 | 0.898 | 0.380 | 0.796 | 0.308 | 0.906 |
| Ē | KMAHA KL M | 0.322 | 0.865 | 0.302 | 0.906 | 0.333 | 0.846 | 0.318 | 0.885 | 0.318 | 0.864 | 0.303 | 0.896 | 0.318 | 0.860 | 0.374 | 0.788 | 0.308 | 0.879 |
| 3-L | ODIN | 0.309 | 0.909 | 0.293 | 0.934 | 0.329 | 0.877 | 0.302 | 0.920 | 0.297 | 0.938 | 0.304 | 0.913 | 0.308 | 0.908 | 0.337 | 0.860 | 0.301 | 0.924 |
| NL. | Energy | 0.302 | 0.911 | 0.278 | 0.947 | 0.328 | 0.873 | 0.290 | 0.929 | 0.292 | 0.938 | 0.298 | 0.913 | 0.298 | 0.916 | 0.346 | 0.834 | 0.287 | 0.938 |
| INE | DOCTOR | 0.302 | 0.909 | 0.292 | 0.927 | 0.313 | 0.891 | 0.299 | 0.913 | 0.298 | 0.924 | 0.293 | 0.917 | 0.302 | 0.912 | 0.327 | 0.866 | 0.292 | 0.926 |
| 3ILI | REACT | 0.301 | 0.909 | 0.289 | 0.933 | 0.324 | 0.873 | 0.289 | 0.923 | 0.285 | 0.933 | 0.300 | 0.909 | 0.293 | 0.917 | 0.357 | 0.843 | 0.290 | 0.930 |
| ΜO | MSP | 0.298 | 0.902 | 0.283 | 0.927 | 0.312 | 0.884 | 0.296 | 0.903 | 0.293 | 0.916 | 0.290 | 0.909 | 0.298 | 0.904 | 0.323 | 0.858 | 0.289 | 0.916 |
| | MAXL | 0.292 | 0.918 | 0.275 | 0.950 | 0.313 | 0.885 | 0.281 | 0.935 | 0.281 | 0.945 | 0.288 | 0.922 | 0.287 | 0.924 | 0.335 | 0.841 | 0.275 | 0.945 |
| | KNN | 0.473 | 0.694 | 0.507 | 0.623 | 0.466 | 0.701 | 0.472 | 0.700 | 0.515 | 0.622 | 0.461 | 0.705 | 0.438 | 0.758 | 0.493 | 0.678 | 0.429 | 0.761 |
| ET) | MAHA | 0.452 | 0.737 | 0.448 | 0.731 | 0.452 | 0.732 | 0.449 | 0.748 | 0.466 | 0.700 | 0.447 | 0.737 | 0.423 | 0.791 | 0.518 | 0.647 | 0.410 | 0.808 |
| 3EN | MCOS | 0.419 | 0.794 | 0.402 | 0.822 | 0.428 | 0.773 | 0.418 | 0.802 | 0.448 | 0.734 | 0.406 | 0.812 | 0.410 | 0.809 | 0.462 | 0.745 | 0.382 | 0.858 |
| MAC | ODIN | 0.412 | 0.862 | 0.387 | 0.884 | 0.413 | 0.846 | 0.396 | 0.866 | 0.394 | 0.874 | 0.401 | 0.868 | 0.398 | 0.828 | 0.437 | 0.827 | 0.389 | 0.871 |
| E | OURS | 0.404 | 0.835 | 0.392 | 0.834 | 0.409 | 0.825 | 0.398 | 0.848 | 0.413 | 0.814 | 0.396 | 0.846 | 0.389 | 0.864 | 0.454 | 0.775 | 0.378 | 0.877 |
| 3-6 | IGEOOD | 0.400 | 0.853 | 0.388 | 0.869 | 0.406 | 0.838 | 0.387 | 0.861 | 0.394 | 0.863 | 0.403 | 0.851 | 0.400 | 0.855 | 0.432 | 0.817 | 0.393 | 0.870 |
| ET | KL M PMAUA | 0.398 | 0.863 | 0.392 | 0.881 | 0.394 | 0.857 | 0.405 | 0.861 | 0.391 | 0.867 | 0.389 | 0.872 | 0.386 | 0.869 | 0.450 | 0.810 | 0.374 | 0.888 |
| EN | ENERGY | 0.390 | 0.854 | 0.364 | 0.890 | 0.393 | 0.833 | 0.392 | 0.863 | 0.390 | 0.820 | 0.370 | 0.852 | 0.379 | 0.866 | 0.459 | 0.761 | 0.370 | 0.848 |
| BII | DOCTOR | 0.381 | 0.871 | 0.375 | 0.887 | 0.386 | 0.859 | 0.373 | 0.876 | 0.374 | 0.885 | 0.373 | 0.877 | 0.379 | 0.876 | 0.413 | 0.828 | 0.378 | 0.880 |
| Ŭ | MSP | 0.377 | 0.873 | 0.362 | 0.892 | 0.382 | 0.862 | 0.369 | 0.876 | 0.369 | 0.887 | 0.372 | 0.876 | 0.375 | 0.879 | 0.411 | 0.831 | 0.372 | 0.883 |
| | MAXL | 0.376 | 0.884 | 0.365 | 0.903 | 0.381 | 0.872 | 0.367 | 0.890 | 0.365 | 0.902 | 0.371 | 0.888 | 0.366 | 0.896 | 0.435 | 0.810 | 0.358 | 0.906 |
| | Maha Kl M | 0.378 | 0.782 | 0.343 | 0.835 | 0.403 | 0.736 | 0.352 | 0.823 | 0.379 | 0.764 | 0.384 | 0.773 | 0.370 | 0.791 | 0.472 | 0.644 | 0.318 | 0.893 |
| Ê | KL M Energy | 0.326 | 0.900 | 0.313 | 0.919 | 0.339 | 0.881 | 0.321 | 0.906 | 0.301 | 0.924 | 0.343 | 0.885 | 0.294 | 0.928 | 0.363 | 0.844 | 0.313 | 0.914 |
| NE | KNN | 0.323 | 0.877 | 0.310 | 0.893 | 0.334 | 0.853 | 0.310 | 0.899 | 0.313 | 0.892 | 0.329 | 0.868 | 0.307 | 0.903 | 0.399 | 0.757 | 0.282 | 0.948 |
| AGE | ODIN | 0.320 | 0.890 | 0.308 | 0.914 | 0.334 | 0.863 | 0.308 | 0.902 | 0.308 | 0.917 | 0.328 | 0.874 | 0.314 | 0.903 | 0.356 | 0.833 | 0.307 | 0.912 |
| (IM | MCos | 0.319 | 0.892 | 0.288 | 0.940 | 0.335 | 0.860 | 0.307 | 0.912 | 0.307 | 0.909 | 0.324 | 0.886 | 0.310 | 0.905 | 0.391 | 0.780 | 0.286 | 0.949 |
| 01 | OURS | 0.319 | 0.889 | 0.288 | 0.938 | 0.333 | 0.885 | 0.307 | 0.903 | 0.293 | 0.932 | 0.324 | 0.883 | 0.330 | 0.804 | 0.303 | 0.817 | 0.299 | 0.917 |
| 1-1 | IGEOOD | 0.315 | 0.902 | 0.302 | 0.917 | 0.323 | 0.885 | 0.302 | 0.916 | 0.301 | 0.928 | 0.325 | 0.885 | 0.303 | 0.924 | 0.356 | 0.842 | 0.307 | 0.917 |
| SNI | MAXL | 0.314 | 0.893 | 0.302 | 0.909 | 0.327 | 0.869 | 0.301 | 0.906 | 0.300 | 0.923 | 0.325 | 0.877 | 0.306 | 0.908 | 0.351 | 0.834 | 0.301 | 0.915 |
| \mathbf{R}_{E} | RMAHA MSD | 0.312 | 0.893 | 0.295 | 0.925 | 0.318 | 0.881 | 0.307 | 0.905 | 0.314 | 0.886 | 0.306 | 0.906 | 0.309 | 0.890 | 0.343 | 0.850 | 0.302 | 0.903 |
| | DOCTOR | 0.311 | 0.894 | 0.293 | 0.910 | 0.320 | 0.879 | 0.309 | 0.893 | 0.304 | 0.913 | 0.308 | 0.885 | 0.303 | 0.910 | 0.333 | 0.854 | 0.313 | 0.894 |
| | Μάμα | 0.433 | 0.719 | 0.411 | 0.741 | 0.437 | 0.713 | 0.425 | 0.740 | 0.461 | 0.667 | 0.425 | 0.727 | 0.407 | 0.760 | 0.506 | 0.628 | 0.395 | 0.779 |
| | KNN | 0.368 | 0.828 | 0.364 | 0.834 | 0.377 | 0.810 | 0.365 | 0.835 | 0.365 | 0.825 | 0.372 | 0.823 | 0.343 | 0.865 | 0.446 | 0.709 | 0.315 | 0.919 |
| (LE | ODIN | 0.353 | 0.880 | 0.331 | 0.913 | 0.367 | 0.854 | 0.344 | 0.891 | 0.336 | 0.911 | 0.355 | 0.876 | 0.348 | 0.888 | 0.406 | 0.807 | 0.341 | 0.899 |
| EN | REACT | 0.353 | 0.872 | 0.315 | 0.927 | 0.379 | 0.830 | 0.340 | 0.892 | 0.327 | 0.919 | 0.358 | 0.876 | 0.361 | 0.848 | 0.414 | 0.777 | 0.331 | 0.908 |
| IAG | KL M OURS | 0.352 | 0.887 | 0.329 | 0.920 | 0.354 | 0.879 | 0.355 | 0.885 | 0.341 | 0.899 | 0.366 | 0.883 | 0.324 | 0.908 | 0.409 | 0.824 | 0.342 | 0.895 |
| Ð | MCos | 0.350 | 0.873 | 0.317 | 0.922 | 0.364 | 0.844 | 0.347 | 0.883 | 0.343 | 0.880 | 0.341 | 0.879 | 0.341 | 0.880 | 0.433 | 0.756 | 0.311 | 0.939 |
| -34 | RMAHA | 0.346 | 0.862 | 0.323 | 0.902 | 0.354 | 0.851 | 0.343 | 0.870 | 0.350 | 0.856 | 0.327 | 0.893 | 0.338 | 0.866 | 0.391 | 0.801 | 0.346 | 0.853 |
| NET | ENERGY | 0.345 | 0.876 | 0.322 | 0.909 | 0.360 | 0.846 | 0.334 | 0.889 | 0.325 | 0.913 | 0.349 | 0.869 | 0.341 | 0.883 | 0.400 | 0.801 | 0.332 | 0.901 |
| RES] | MAXL | 0.340 | 0.883 | 0.323 | 0.916 | 0.349 | 0.861 | 0.330 | 0.893 | 0.318 | 0.911 | 0.330 | 0.870 | 0.324 | 0.905 | 0.392 | 0.803 | 0.327 | 0.904 |
| ц | DOCTOR | 0.334 | 0.890 | 0.316 | 0.922 | 0.338 | 0.880 | 0.337 | 0.884 | 0.328 | 0.907 | 0.327 | 0.896 | 0.324 | 0.906 | 0.360 | 0.844 | 0.341 | 0.884 |
| | MSP | 0.332 | 0.885 | 0.309 | 0.922 | 0.337 | 0.875 | 0.332 | 0.880 | 0.325 | 0.902 | 0.328 | 0.889 | 0.324 | 0.898 | 0.360 | 0.835 | 0.338 | 0.879 |
| | Мана | 0.398 | 0.751 | 0.375 | 0.776 | 0.412 | 0.722 | 0.386 | 0.774 | 0.416 | 0.703 | 0.393 | 0.756 | 0.385 | 0.766 | 0.481 | 0.645 | 0.334 | 0.870 |
| ~ | KL M | 0.338 | 0.888 | 0.319 | 0.918 | 0.348 | 0.869 | 0.337 | 0.898 | 0.338 | 0.897 | 0.328 | 0.897 | 0.307 | 0.914 | 0.395 | 0.819 | 0.334 | 0.891 |
| Ē | ENERGY | 0.338 | 0.878 | 0.305 | 0.918 | 0.356 | 0.846 | 0.319 | 0.902 | 0.328 | 0.908 | 0.342 | 0.870 | 0.325 | 0.895 | 0.399 | 0.790 | 0.333 | 0.895 |
| GEN | ODIN | 0.337 | 0.886 | 0.331 | 0.923 | 0.349 | 0.852 | 0.324 | 0.881 | 0.324 | 0.913 | 0.338 | 0.882 | 0.312 | 0.905 | 0.388 | 0.805 | 0.289 | 0.896 |
| MA | REACT | 0.330 | 0.876 | 0.295 | 0.933 | 0.353 | 0.834 | 0.312 | 0.899 | 0.304 | 0.926 | 0.337 | 0.874 | 0.335 | 0.853 | 0.386 | 0.790 | 0.317 | 0.897 |
| I) (I | MAXL | 0.329 | 0.882 | 0.308 | 0.918 | 0.341 | 0.855 | 0.310 | 0.904 | 0.316 | 0.912 | 0.333 | 0.877 | 0.312 | 0.903 | 0.388 | 0.796 | 0.325 | 0.896 |
| 3-13 | MCOS RMAHA | 0.329 | 0.885 | 0.297 | 0.935 | 0.345 | 0.852 | 0.317 | 0.907 | 0.321 | 0.895 | 0.328 | 0.886 | 0.318 | 0.898 | 0.407 | 0.767 | 0.296 | 0.943 |
| SNE | IGEOOD | 0.323 | 0.894 | 0.304 | 0.925 | 0.333 | 0.874 | 0.305 | 0.918 | 0.311 | 0.918 | 0.326 | 0.886 | 0.303 | 0.923 | 0.380 | 0.811 | 0.325 | 0.900 |
| RE | OURS | 0.320 | 0.900 | 0.293 | 0.934 | 0.335 | 0.877 | 0.306 | 0.920 | 0.314 | 0.904 | 0.316 | 0.903 | 0.309 | 0.916 | 0.388 | 0.813 | 0.302 | 0.932 |
| | DOCTOR | 0.319 | 0.890 | 0.303 | 0.923 | 0.329 | 0.868 | 0.310 | 0.897 | 0.317 | 0.903 | 0.305 | 0.897 | 0.303 | 0.909 | 0.342 | 0.842 | 0.340 | 0.878 |
| | INI O L | 0.518 | 0.094 | 0.294 | 0.927 | 0.329 | 0.0/4 | 0.510 | 0.901 | 0.317 | 0.908 | 0.508 | 0.901 | 0.304 | 0.913 | 0.540 | 0.043 | 0.337 | 0.002 |

Table 8: Comparative analysis of AURC in the black-box SCOD framework between 12 existing OOD detection methods and our method (combining the other 12 methods) for vision transformers trained on ImageNet. Results are sorted in descending order by average AURC.

| | | | VG | IN | АТ | NIN | ICO | OPE | NIM | PLA | CES | SPE | CIES | SSE | (E) | SSF | (н) | TE | x |
|-----|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------------|-------|-------|-------|-------|
| | | RC | ROC | RC | ROC | RC | ROC |
| | | | | | | | | | | | | | | | | | | | |
| | KL M | 0.271 | 0.920 | 0.236 | 0.965 | 0.284 | 0.902 | 0.257 | 0.939 | 0.266 | 0.925 | 0.278 | 0.909 | 0.260 | 0.932 | 0.324 | 0.860 | 0.265 | 0.930 |
| | KNN | 0.263 | 0.919 | 0.245 | 0.955 | 0.275 | 0.895 | 0.251 | 0.941 | 0.263 | 0.920 | 0.273 | 0.904 | 0.251 | 0.941 | 0.299 | 0.854 | 0.251 | 0.942 |
| | OURS | 0.262 | 0.936 | 0.233 | 0.969 | 0.277 | 0.914 | 0.252 | 0.954 | 0.260 | 0.940 | 0.267 | 0.929 | 0.257 | 0.948 | 0.292 | 0.888 | 0.261 | 0.942 |
| ΕT | REACT | 0.257 | 0.926 | 0.237 | 0.962 | 0.269 | 0.902 | 0.245 | 0.948 | 0.251 | 0.935 | 0.271 | 0.910 | 0.245 | 0.946 | 0.284 | 0.876 | 0.256 | 0.932 |
| EN | Energy | 0.255 | 0.940 | 0.234 | 0.967 | 0.268 | 0.920 | 0.245 | 0.956 | 0.251 | 0.947 | 0.273 | 0.919 | 0.245 | 0.956 | 0.273 | 0.908 | 0.251 | 0.947 |
| IAC | DOCTOR | 0.255 | 0.935 | 0.235 | 0.969 | 0.267 | 0.916 | 0.246 | 0.949 | 0.255 | 0.936 | 0.259 | 0.929 | 0.250 | 0.942 | 0.270 | 0.903 | 0.255 | 0.935 |
| Ē | MSP | 0.254 | 0.936 | 0.234 | 0.968 | 0.266 | 0.916 | 0.245 | 0.950 | 0.254 | 0.938 | 0.258 | 0.928 | 0.251 | 0.944 | 0.270 | 0.905 | 0.256 | 0.937 |
| 16 | MCos | 0.254 | 0.935 | 0.238 | 0.964 | 0.265 | 0.913 | 0.242 | 0.955 | 0.248 | 0.943 | 0.266 | 0.918 | 0.244 | 0.953 | 0.281 | 0.887 | 0.246 | 0.950 |
| ·B/ | MAXL | 0.253 | 0.943 | 0.240 | 0.967 | 0.261 | 0.927 | 0.244 | 0.956 | 0.250 | 0.948 | 0.270 | 0.922 | 0.243 | 0.957 | 0.268 | 0.914 | 0.247 | 0.951 |
| É | ODIN | 0.250 | 0.944 | 0.236 | 0.968 | 0.261 | 0.925 | 0.240 | 0.958 | 0.247 | 0.949 | 0.265 | 0.924 | 0.240 | 0.958 | 0.263 | 0.916 | 0.245 | 0.951 |
| > | RMAHA | 0.246 | 0.939 | 0.228 | 0.969 | 0.253 | 0.926 | 0.236 | 0.957 | 0.246 | 0.938 | 0.247 | 0.941 | 0.242 | 0.943 | 0.272 | 0.893 | 0.244 | 0.941 |
| | IGEOOD | 0.245 | 0.943 | 0.236 | 0.970 | 0.258 | 0.920 | 0.233 | 0.960 | 0.240 | 0.950 | 0.258 | 0.928 | 0.235 | 0.958 | 0.261 | 0.911 | 0.241 | 0.949 |
| | MAHA | 0.243 | 0.944 | 0.219 | 0.970 | 0.251 | 0.933 | 0.235 | 0.962 | 0.244 | 0.945 | 0.248 | 0.942 | 0.240 | 0.953 | 0.271 | 0.897 | 0.241 | 0.953 |
| | KL M | 0.256 | 0.934 | 0.225 | 0.971 | 0.265 | 0.920 | 0.246 | 0.947 | 0.252 | 0.937 | 0.264 | 0.920 | 0.248 | 0.943 | 0.296 | 0.886 | 0.247 | 0.944 |
| | OURS | 0.246 | 0.943 | 0.223 | 0.975 | 0.257 | 0.925 | 0.239 | 0.956 | 0.246 | 0.941 | 0.247 | 0.938 | 0.242 | 0.951 | 0.268 | 0.907 | 0.243 | 0.950 |
| Ê | KNN | 0.245 | 0.936 | 0.233 | 0.963 | 0.257 | 0.911 | 0.233 | 0.955 | 0.239 | 0.943 | 0.254 | 0.923 | 0.233 | 0.955 | 0.275 | 0.884 | 0.235 | 0.955 |
| ZE. | MCos | 0.241 | 0.947 | 0.226 | 0.969 | 0.253 | 0.924 | 0.234 | 0.960 | 0.236 | 0.955 | 0.250 | 0.932 | 0.235 | 0.959 | 0.261 | 0.914 | 0.236 | 0.959 |
| GE | MSP | 0.240 | 0.946 | 0.224 | 0.975 | 0.246 | 0.935 | 0.233 | 0.957 | 0.240 | 0.946 | 0.246 | 0.936 | 0.237 | 0.952 | 0.257 | 0.919 | 0.240 | 0.949 |
| MA | DOCTOR | 0.240 | 0.945 | 0.224 | 0.976 | 0.249 | 0.930 | 0.233 | 0.954 | 0.239 | 0.945 | 0.245 | 0.936 | 0.235 | 0.951 | 0.255 | 0.916 | 0.237 | 0.948 |
| Ξ | ENERGY | 0.239 | 0.953 | 0.219 | 0.974 | 0.250 | 0.936 | 0.232 | 0.967 | 0.236 | 0.959 | 0.252 | 0.935 | 0.233 | 0.964 | 0.258 | 0.922 | 0.234 | 0.963 |
| /16 | REACT | 0.236 | 0.94/ | 0.218 | 0.972 | 0.241 | 0.939 | 0.229 | 0.959 | 0.254 | 0.916 | 0.234 | 0.954 | 0.233 | 0.952 | 0.245 | 0.931 | 0.235 | 0.949 |
| Ę | IGEOOD | 0.230 | 0.950 | 0.225 | 0.974 | 0.247 | 0.930 | 0.225 | 0.965 | 0.232 | 0.954 | 0.245 | 0.935 | 0.228 | 0.961 | 0.255 | 0.919 | 0.230 | 0.958 |
| 5 | ODIN | 0.233 | 0.955 | 0.229 | 0.975 | 0.241 | 0.939 | 0.227 | 0.900 | 0.231 | 0.958 | 0.246 | 0.937 | 0.228 | 0.904 | 0.231 | 0.924 | 0.227 | 0.904 |
| | RMAHA | 0.234 | 0.950 | 0.220 | 0.975 | 0.244 | 0.941 | 0.220 | 0.909 | 0.230 | 0.902 | 0.243 | 0.940 | 0.228 | 0.907 | 0.248 | 0.931 | 0.227 | 0.907 |
| | Мана | 0.231 | 0.954 | 0.210 | 0.974 | 0.235 | 0.940 | 0.223 | 0.967 | 0.229 | 0.957 | 0.232 | 0.955 | 0.226 | 0.959 | 0.249 | 0.923 | 0.232 | 0.961 |
| | IZI M | 0.225 | 0.002 | 0.207 | 0.056 | 0.207 | 0.000 | 0.222 | 0.017 | 0.220 | 0.002 | 0.200 | 0.000 | 0.220 | 0.017 | 0.251 | 0.020 | 0.220 | 0.011 |
| | KL M | 0.295 | 0.903 | 0.257 | 0.956 | 0.305 | 0.886 | 0.286 | 0.917 | 0.290 | 0.903 | 0.301 | 0.899 | 0.277 | 0.917 | 0.355 | 0.836 | 0.289 | 0.911 |
| | KNN | 0.291 | 0.901 | 0.272 | 0.939 | 0.300 | 0.879 | 0.280 | 0.922 | 0.296 | 0.888 | 0.292 | 0.902 | 0.281 | 0.920 | 0.332 | 0.829 | 0.277 | 0.929 |
| Ē | ENERGY | 0.285 | 0.917 | 0.255 | 0.902 | 0.298 | 0.895 | 0.274 | 0.934 | 0.279 | 0.919 | 0.200 | 0.912 | 0.275 | 0.931 | 0.320 | 0.838 | 0.270 | 0.928 |
| N. | DOCTOR | 0.280 | 0.920 | 0.253 | 0.901 | 0.290 | 0.899 | 0.270 | 0.944 | 0.270 | 0.941 | 0.292 | 0.908 | 0.273 | 0.938 | 0.307 | 0.880 | 0.274 | 0.930 |
| AGE | MSP | 0.278 | 0.917 | 0.255 | 0.959 | 0.288 | 0.901 | 0.275 | 0.920 | 0.277 | 0.910 | 0.200 | 0.913 | 0.273 | 0.931 | 0.301 | 0.870 | 0.277 | 0.915 |
| Ŵ | REACT | 0.276 | 0.915 | 0.252 | 0.936 | 0.287 | 0.893 | 0.275 | 0.924 | 0.270 | 0.927 | 0.279 | 0.880 | 0.275 | 0.920 | 0.303 | 0.866 | 0.270 | 0.930 |
| 9 | MCos | 0.275 | 0.926 | 0.254 | 0.960 | 0.290 | 0.899 | 0.266 | 0.944 | 0.270 | 0.932 | 0.278 | 0.921 | 0.269 | 0.938 | 0.310 | 0.867 | 0.264 | 0.947 |
| S/1 | RMAHA | 0.275 | 0.915 | 0.252 | 0.959 | 0.285 | 0.898 | 0.265 | 0.935 | 0.274 | 0.914 | 0.268 | 0.929 | 0.272 | 0.917 | 0.313 | 0.851 | 0.269 | 0.920 |
| Ĕ. | MAXL | 0.273 | 0.935 | 0.256 | 0.964 | 0.284 | 0.913 | 0.266 | 0.949 | 0.263 | 0.948 | 0.286 | 0.918 | 0.267 | 0.947 | 0.296 | 0.893 | 0.265 | 0.946 |
| > | ODIN | 0.272 | 0.934 | 0.259 | 0.962 | 0.283 | 0.915 | 0.266 | 0.948 | 0.262 | 0.948 | 0.282 | 0.918 | 0.266 | 0.947 | 0.294 | 0.895 | 0.267 | 0.943 |
| | Igeood | 0.269 | 0.922 | 0.257 | 0.963 | 0.283 | 0.894 | 0.258 | 0.943 | 0.258 | 0.935 | 0.281 | 0.905 | 0.257 | 0.942 | 0.300 | 0.864 | 0.261 | 0.934 |
| | MAHA | 0.269 | 0.922 | 0.245 | 0.962 | 0.278 | 0.906 | 0.256 | 0.945 | 0.269 | 0.918 | 0.266 | 0.930 | 0.263 | 0.931 | 0.308 | 0.855 | 0.263 | 0.930 |
| | KNN | 0.357 | 0.831 | 0.337 | 0.866 | 0.369 | 0.810 | 0.340 | 0.862 | 0.369 | 0.802 | 0.355 | 0.832 | 0.336 | 0.864 | 0.426 | 0.731 | 0.325 | 0.884 |
| | KL M | 0.345 | 0.882 | 0.302 | 0.937 | 0.361 | 0.860 | 0.339 | 0.899 | 0.326 | 0.894 | 0.351 | 0.877 | 0.332 | 0.888 | 0.425 | 0.796 | 0.321 | 0.905 |
| | Maha | 0.342 | 0.862 | 0.303 | 0.923 | 0.350 | 0.851 | 0.326 | 0.894 | 0.357 | 0.828 | 0.332 | 0.880 | 0.330 | 0.881 | 0.400 | 0.785 | 0.343 | 0.853 |
| ΕT | OURS | 0.335 | 0.897 | 0.296 | 0.942 | 0.352 | 0.872 | 0.321 | 0.920 | 0.331 | 0.901 | 0.337 | 0.895 | 0.326 | 0.912 | 0.395 | 0.818 | 0.322 | 0.916 |
| EN | RMAHA | 0.332 | 0.876 | 0.300 | 0.937 | 0.345 | 0.856 | 0.317 | 0.904 | 0.334 | 0.866 | 0.318 | 0.898 | 0.326 | 0.880 | 0.397 | 0.784 | 0.321 | 0.884 |
| IAG | MCos | 0.331 | 0.882 | 0.301 | 0.924 | 0.350 | 0.851 | 0.317 | 0.907 | 0.331 | 0.878 | 0.330 | 0.880 | 0.318 | 0.901 | 0.393 | 0.794 | 0.308 | 0.921 |
| Ē | Igeood | 0.329 | 0.891 | 0.308 | 0.932 | 0.353 | 0.852 | 0.311 | 0.919 | 0.315 | 0.910 | 0.345 | 0.866 | 0.307 | 0.923 | 0.395 | 0.792 | 0.302 | 0.931 |
| 16 | ODIN | 0.326 | 0.904 | 0.303 | 0.944 | 0.347 | 0.867 | 0.311 | 0.928 | 0.314 | 0.925 | 0.339 | 0.887 | 0.312 | 0.922 | 0.375 | 0.825 | 0.306 | 0.935 |
| Ĺ. | REACT | 0.325 | 0.896 | 0.288 | 0.952 | 0.344 | 0.862 | 0.305 | 0.927 | 0.311 | 0.919 | 0.336 | 0.879 | 0.317 | 0.904 | 0.388 | 0.800 | 0.307 | 0.923 |
| Ė | MSP | 0.322 | 0.887 | 0.299 | 0.930 | 0.337 | 0.863 | 0.316 | 0.895 | 0.319 | 0.893 | 0.321 | 0.884 | 0.316 | 0.894 | 0.354 | 0.832 | 0.310 | 0.902 |
| > | Energy | 0.321 | 0.906 | 0.293 | 0.947 | 0.345 | 0.867 | 0.304 | 0.933 | 0.307 | 0.929 | 0.336 | 0.888 | 0.307 | 0.925 | 0.377 | 0.822 | 0.300 | 0.939 |
| | DOCTOR | 0.321 | 0.899 | 0.303 | 0.933 | 0.334 | 0.881 | 0.316 | 0.907 | 0.319 | 0.906 | 0.319 | 0.898 | 0.315 | 0.908 | 0.353 | 0.846 | 0.308 | 0.915 |
| | MAXL | 0.314 | 0.907 | 0.294 | 0.946 | 0.334 | 0.872 | 0.299 | 0.928 | 0.300 | 0.928 | 0.328 | 0.891 | 0.299 | 0.926 | 0.367 | 0.824 | 0.292 | 0.939 |