# Data Augmentation Policy Search for Long-Term Forecasting

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### Abstract

Data augmentation serves as a popular regularization technique to combat overfitting challenges in neural networks. While automatic augmentation has demonstrated success in image classification tasks, its application to time-series problems, particularly in long-term forecasting, has received comparatively less attention. To address this gap, we introduce a time-series automatic augmentation approach named TSAA, which is both efficient and easy to implement. The solution involves tackling the associated bilevel optimization problem through a two-step process: initially training a non-augmented model for a limited number of epochs, followed by an iterative split procedure. During this iterative process, we alternate between identifying a robust augmentation policy through Bayesian optimization and refining the model while discarding suboptimal runs. Extensive evaluations on challenging univariate and multivariate forecasting benchmark problems demonstrate that TSAA consistently outperforms several robust baselines, suggesting its potential integration into prediction pipelines. Code is available at this repository: https://github.com/azencot-group/TSAA.

# 1 Introduction

Modern machine learning tools require large volumes of data to effectively solve challenging tasks. However, high-quality labeled data is difficult to obtain as manual labeling is costly and it may require human expertise (Shorten & Khoshgoftaar, 2019). Small datasets may lead to overfitting in overparameterized models, a phenomenon in which the model struggles with examples it has not seen before (Allen-Zhu et al., 2019). One of the effective methods to alleviate poor generalization issues is via *data augmentation* (DA). Data augmentation aims to generate artificial new examples whose statistical features match the true distribution of the data (Simard et al., 1998). In practice, DA has been shown to achieve state-of-the-art (SOTA) results in e.g., vision (Krizhevsky et al., 2012) and natural language (Wei & Zou, 2019) tasks.

Unfortunately, DA is not free from challenges. For instance, Tian et al. (2020b) showed that the effectivity of augmented samples depends on the downstream task. To this end, recent approaches explored automatic augmentation tools, where a good DA policy is searched for (Lemley et al., 2017; Cubuk et al., 2019). While automatic frameworks achieved impressive results on image classification tasks (Zheng et al., 2022) and other data modalities, problems with time-series data received significantly less attention Kaufman & Azencot (2024a); Nochumsohn et al. (2024). Toward bridging this gap, we propose in this work a new automatic data augmentation method, designed for *time-series forecasting* problems.

Time-series forecasting is a long-standing task in numerous scientific and engineering fields (Chatfield, 2000). While deep learning techniques achieved groundbreaking results on vision and NLP problems already a decade ago, time-series forecasting (TSF) was considered by many to be too challenging for deep models, up until recently (Oreshkin et al., 2020). While recent linear approaches showed interesting forecast results (Zeng et al., 2023; Nochumsohn et al., 2025), existing SOTA approaches for TSF are based on deep learning

architectures that are structurally similar to vision models. In particular, current TSF deep models are overparameterized Kaufman & Azencot (2024b), and thus they may benefit from similar regularization techniques which were found effective for vision models, such as (automatic) data augmentation. Ultimately, our work is motivated by the limited availability of DA tools for time-series tasks (Wen et al., 2020).

The main contributions of our work can be summarized as follows: 1) We develop a novel automatic data augmentation approach for long-term time-series forecasting tasks. Our approach is based on a carefully designed dictionary of time-series transformations, Bayesian optimization for policy search, and pruning tools that enforce early stopping of ineffective networks. While these components appear in existing work, their combination and adaptation to time-series forecasting was not done before, to the best of our knowledge. 2) We analyze the optimal policies our approach finds. Our analysis sheds light into the most effective transformations, and it may inspire others in designing effective data augmentation techniques for time-series data. 3) Our approach augments existing time-series forecasting baselines, and we extensively evaluated it on long-term forecasting univariate and multivariate TSF benchmarks with respect to several strong baseline architectures. We find that our framework enhances performance in most long-term forecast settings and across most datasets and baseline architectures.

# 2 Related Work

**Time-series forecasting.** Recently, several neural network approaches for TSF have been proposed. Based on recurrent neural networks, DeepAR (Salinas et al., 2020) produced probabilistic forecasts with uncertainty quantification. The N-BEATS (Oreshkin et al., 2020) model employs fully connected layers with skip connections, and subsequent work (Challu et al., 2022) improved long-term forecasting via pooling and interpolation. Another line of works based on the transformer architecture (Vaswani et al., 2017) used a sparse encoder and a generative decoder in the Informer (Zhou et al., 2021), trend-seasonality decomposition in the Autoformer (Wu et al., 2021), and Fourier and Wavelet transformations in the FEDformer (Zhou et al., 2022). Recently, Pyraformer (Liu et al., 2021) significantly reduced the complexity bottleneck of the attention mechanism, PatchTST (Nie et al., 2023) exchanges the point-wise attention input with a tokenized sub-series representation. Finally, Zeng et al. (2023) propose a single-layer MLP with a larger input lookback.

**Data augmentation.** DA techniques have appeared since the early rise of modern deep learning to promote labeled image invariance to certain transformations (Krizhevsky et al., 2012). Typical image augmentations include rotation, scaling, crop, and color manipulations. Recent methods focused on modalityagnostic methods which blend linearly the inputs and labels (Zhang et al., 2018) or utilize manifold learning approaches Kaufman & Azencot (2023; 2024b;a). Other works produce augmented views in the feature space (DeVries & Taylor, 2017; Verma et al., 2019). In contrast to image and text data, augmenting arbitrary time-series (TS) data have received less attention in the literature (Wen et al., 2020; Iwana & Uchida, 2021). In the review (Wen et al., 2020), the authors consider three different tasks: TS classification, TS anomaly detection, and TS forecasting. Their analysis is based on common time-series augmentation approaches such as scaling, adding noise (Um et al., 2017), window cropping or slicing, and stretching of time intervals (Le Guennec et al., 2016), dynamic time warping (Ismail Fawaz et al., 2019), perturbations of the frequency domain (Gao et al., 2020; Chen et al., 2023), and utilizing surrogate data (Lee et al., 2019). In (Smyl & Kuber, 2016), the authors discuss additional TS augmentation approaches including generating new TS using the residuals of a statistical TS (Bergmeir et al., 2016). Another technique would be to sub-sample the parameters, residuals, and forecasting from MCMC Bavesian models. The survey (Iwana & Uchida, 2021) further details a large list of TS augmentations such as jittering, rotation, time warping, time masking, interpolation and others in the context of time-series classification. The authors in (Wen et al., 2020) propose the selection and combination of augmentations using automatic approaches as a promising avenue for future research, which is the focus of the current work. Finally, we also mention the large body of work on generative modeling of time series (Yoon et al., 2019; Naiman et al., 2024b;a) which is related to data augmentation. We show in Fig. 1A two examples of DA policies.

Automatic DA. To avoid hand-tailored DA, recent efforts aimed for automatic tools, motivated by similar advances in neural architecture search (NAS) approaches (Zoph & Le, 2017). AutoAugment (Cubuk et al.,

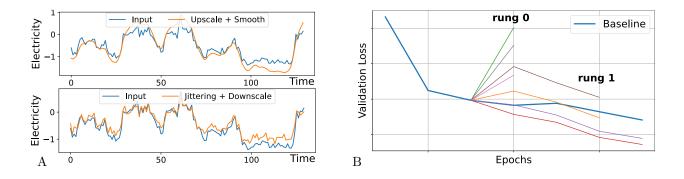


Figure 1: A) Two examples of sub-policies applied on Electricity data. B) The above plot demonstrates the behavior of ASHA with respect to the baseline model (blue). Some of the poorly performing runs are discontinued at the end of rungs, whereas the other runs train to completion.

2019) used a recurrent controller along with reinforcement learning for the search process, yielding a highly effective but computationally intensive framework. Following works such as Fast AutoAugment employed Bayesian optimization and density matching (Lim et al., 2019). RandAugment (Cubuk et al., 2020) reduces the search space significantly by introducing stochasticity. Tian et al. (2020a) suggested partial training using augmentation-wise weight sharing (AWS). Further, recent approaches utilize gradients for the search problem, including the differentiable automatic DA (DADA) (Li et al., 2020b) and Deep AutoAugment (Zheng et al., 2022). Cheung & Yeung (2020) developed automatic DA that does not depend on the data-modality as it exploits latent transformations. In (Fons et al., 2021), the authors propose adaptive-weighting strategies which favor a subset of time-series DA for classification, based on their effect on the training loss.

#### 3 Background

Below, we briefly describe background information on Bayesian optimization and pruning approaches which we use to find the best augmentation policy and improve model training efficiency, respectively.

**Tree-structured Parzen Estimators and the Expected Improvement.** Bayesian optimization relates to a family of techniques where an objective function  $f(x) : \mathbb{R}^d \to \mathbb{R}^+$  is minimized, i.e.,

$$\min_{x \to 0} f(x) . \tag{1}$$

In the typical setting, f is costly to evaluate, its gradients are not available, and  $d \leq 20$ . For instance, finding the hyperparameters (x) of a neural network (f) is a common use case for Bayesian optimization (Bergstra et al., 2013). Unlike grid/random search, Bayesian optimization methods utilize past evaluations of f to maintain a surrogate model p(y|x) for the objective function y = f(x). Thus, Bayesian optimization solves Eq. 1 while limiting the costly evaluations of f to a minimum.

A practical realization of Bayesian optimization is given by Sequential Model-Based Optimization (SMBO) (Hutter et al., 2011). SMBO iterates between model fitting with the existing parameters (exploitation) to parameter selection using the current model (exploration). SMBO constructs a surrogate model p(y|x), finds a set of parameters x that performs best on the p(y|x) using an acquisition function, applies the objective function f on x to obtain the score y, updates the surrogate model, and repeats the last three steps until convergence. Most SMBO techniques differ in their choice of the surrogate model and acquisition function. We will focus on Tree-structured Parzen Estimator (TPE) for the surrogate model, combined with Expected Improvement for the acquisition function. The main idea behind TPE is to model the surrogate via two distributions, l(x) and g(x), corresponding to model evaluations that yield positive, and negative improvement. Formally,

$$p(x|y) = \begin{cases} l(x) & y < y^* \\ g(x) & y \ge y^* \end{cases}$$
(2)

where  $y^*$  is a threshold score, and the surrogate model is obtained via Bayes rule. It can be shown that maximizing l(x)/g(x) leads to an optimal Expected Improvement (EI) (Bergstra et al., 2011).

Asynchronous Successive Halving. While Bayesian optimization uses a minimal number of evaluations of f, the overall minimization is computationally demanding due to the high cost of f, e.g., if f is a neural network that needs to be trained. To alleviate some of these costs, Asynchronous Successive Halving (ASHA) (Jamieson & Talwalkar, 2016; Li et al., 2020a) enforces early stopping of poorly performing parameters x, whereas parameters with low l(x), are trained to the fullest. In a fixed budget system, given a maximum resource R, minimum resource r, and a reduction factor  $\eta$ , ASHA works as follows. One creates model checkpoints during the training process at epochs  $\eta^j$  where  $j = 1, \ldots, \lfloor \log_{\eta} R/r \rfloor$ . Each checkpoint is referred to as a rung, and at the end of each rung, one keeps only the best  $\frac{1}{\eta}$  runs. To avoid waiting for all runs to reach the next rung, ASHA performs asynchronous evaluations to promote or halt runs on the go. We illustrate in Fig. 1B an example of a baseline model with multiple different runs, administered by ASHA.

# 4 Time-Series AutoAugment (TSAA)

Automatic augmentation via bi-level optimization. The task of finding data augmentations automatically during the training of a deep neural network model can be formulated as a bi-level optimization problem, see e.g., (Li et al., 2020b). Namely,

$$\min_{\theta} \quad \mathcal{L}_{\text{val}}(\omega, \theta) \tag{3}$$

subject to 
$$\min_{\boldsymbol{\omega}} \mathbb{E}_{p_{\theta}} \left[ \mathcal{L}_{tr}(\boldsymbol{\omega}, \theta) \right]$$
 (4)

At the top level, Eq. 3, the optimization aims to find the optimal augmentation policy  $\theta \sim p_{\theta}$ , where  $p_{\theta}$  is some distribution of augmentation policies, e.g., additive noise. Importantly, Eq. 3 minimizes the validation loss,  $\mathcal{L}_{val}$ , that is parameterized both by the augmentation policy and by the network weights  $\omega$ . The latter weights are obtained in the bottom level, Eq. 4, describing an optimization problem that is similar to standard training of a neural network as it minimizes the training loss,  $\mathcal{L}_{tr}$ . The main two differences in Eq. 4 from standard training is the dependence on  $\theta$  and the expectation over all possible augmentation policy distributions  $p_{\theta}$ , leading overall to mutually-dependent optimization problems, or, a bi-level optimization. Unfortunately, the above problem is difficult to solve in practice, and therefore, we relax it as detailed next.

**TSAA overview.** Our approach, which we call time-series automatic augmentation (TSAA), consists of two main steps, as illustrated in Fig. 2 and summarized in Alg. 1. In the first step, we partially train the model for a few epochs and construct a set of shared weights. The second step iterates between solving Eq. 3 in search of an augmentation policy using TPE and EI to solving Eq. 4 with fine-tuning and ASHA for an optimal model. A complexity analysis is given in App. D.

Step 1: compute shared weights. Solving Eq. 4 iteratively requires repeated trainings of the deep model, which is computationally prohibitive. To reduce these costs, we propose to partially train the baseline model and generate a shared set of weights  $\omega_{\text{share}}$ . Doing so, Step 2 is reduced to an iterative process of fine-tuning models for a small number of epochs, where  $\omega_{\text{share}}$  are shared across all augmentations policies. Beyond efficiency aspects, applying DA in the later stages of training is assumed to be more influential (Tian et al., 2020a). In practice, we partially train for  $\lfloor \beta K \rfloor$  epochs, where  $\beta = 0.5$  is a hyperparameter and K is the *active* number of train epochs. In our tests,  $K \leq 10$ , and it may be strictly less due to an early stopping scheduler. K is found by training the baseline model with no augmentation to completion and saving the weights after every epoch. Then, we define

$$\omega_{\text{share}} := \omega(|\beta K|) , \quad R := K - |\beta K| ,$$

where R is the maximum resource parameter, and r = 1 is the minimum resource, see Sec. 3.

Step 2: iterative split optimization. Given  $\omega_{\text{share}}$ , it remains to solve Eqs. 3 and 4 to find the best augmentation policy  $\theta^*$  and final weights  $\omega^*$ . In TSAA, we propose to split this problem to an iterative

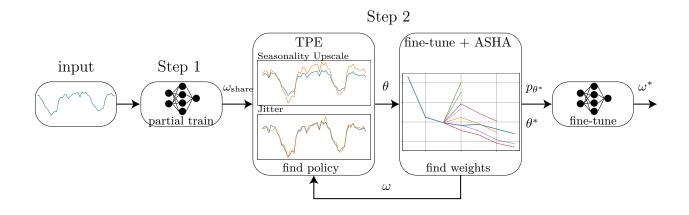


Figure 2: Our time-series automatic augmentation (TSAA) approach is based on a partial train of the model (Step 1), followed by an iterative process (Step 2) where we alternate between improving the augmentation policy  $\theta$  to training the model weights  $\omega$ . We find  $\omega^*$  by fine-tuning over  $p_{\theta^*}$ .

process, where we alternate between exploring augmentation policies  $\theta$  via Eq. 3 to exploiting the current policy and produce model weights  $\omega$  via Eq. 4. Namely, for a fixed set of weights  $\omega$ , the upper minimization finds the next policy  $\theta$  to try by evaluating the validation set. Then, we fine-tune the model using a fixed  $\theta$ with early stopping for a maximum of R epochs to produce the next  $\omega$ . This procedure is repeated until a predefined number of trials  $T_{\text{max}}$  is reached. The k best-performing policies define  $p_{\theta^*}$  from which  $\theta^*$  is sampled, where we only allow policies that improve the baseline validation loss. Finally, we fine-tune the model again to obtain  $\omega^*$ .

Solving Eq. 3. Existing work solved the upper problem using reinforcement learning (Cubuk et al., 2019; Tian et al., 2020a), grid search (Cubuk et al., 2020; Fons et al., 2021), and one-pass optimization (Li et al., 2020b; Zheng et al., 2022). Inspired by (Lim et al., 2019), we propose to use Tree-structured Parzen Estimator (TPE) with Expected Improvement (EI), see Sec. 3. In the context of TSAA, the parameters x in Eq. 1 represent the policy  $\theta$  and f is  $\mathcal{L}_{val}$ . The Bayesian optimization is conducted over the policy search space and time-series augmentations we describe below.

**Policy search space.** The augmentation policies  $\theta$  we consider are drawn from a distribution  $p_{\theta}$  over k sub-policies  $\Theta = \{\theta_1, \ldots, \theta_k\}$ . That is, the distribution  $p_{\theta}$  aggregates several independent distributions  $p(\theta_j)$ , where  $\theta_j \in \Theta$ . Thus,  $p_{\theta}$  allows to sample an augmentation  $\theta$  from each of the considered  $p(\theta_j)$ , i.e.,

$$\theta \sim p_{\theta} := \prod_{j=1}^{k} p(\theta_j) , \quad \theta_j \in \Theta , \Theta := \{\theta_1, \dots, \theta_k\} .$$
(5)

Each sub-policy  $\theta_j$  is composed of n transformations  $T_{j,i}$ , applied sequentially on the output data  $x_{i-1}$  of the previous transformation with  $x_0$  being the input data and  $m_{j,i}$  being the magnitude of the transformation. For instance, if the sub-policy  $\theta_j$  consists of trend downscale in  $T_{j,1}$  and flip in  $T_{j,2}$  with magnitudes  $m_{j,1} = \frac{1}{2}, m_{j,2} = \frac{1}{4}$ , respectively, then,  $\theta_j = T_{j,2}[T_{j,1}(x_0, \frac{1}{2}), \frac{1}{4}]$ . For the general case of n transformations,  $\theta_j$  is defined via

$$\theta_j = T_{j,n}(x_{n-1}, m_{j,n}) \circ \dots \circ T_{j,1}(x_0, m_{j,1}) .$$
(6)

**Time-series data augmentations.** While natural images are invariant to geometric transformations as translation and rotation, arbitrary time-series data need not be invariant to a certain type of transformations. Moreover, capturing the invariance in regression problems such as TSF may be more challenging than in classification tasks including images (Kaufman & Azencot, 2024a). Finally, time-series data may include slow and fast phenomena such as bursts of electricity usage and seasonal peaks, for which some DA may be

inapplicable. Thus, we propose to exploit DA that manipulate some features of the data and leave some features unchanged. For example, adjusting the trend while keeping the seasonality and noise components unaffected, or diversifying the time intervals in a way that the series mean and variance still stay the same. In particular, we suggest the following time-series transformations: identity, jittering, trend scaling, seasonality scaling, scaling, smoothing, noise scaling, flip, permutation, reverse, dynamic-time-stretching (DTS), window warping, and mixup. The magnitude of the augmentations can be controlled using a single parameter. The transformations are further elaborated in App. B and Tab. 4 in the appendix.

Solving Eq. 4. Finally, solving the bottom minimization may be achieved in a straightforward fashion via fine-tuning. However, as motivated in Sec. 4, doing so iteratively is costly. To prune runs, we augment our approach with Asynchronous Successive Halving (ASHA). Our choice to use ASHA over other techniques such as Bayesian Optimization HyperBand (BOHB) (Falkner et al., 2018) is motivated by the following reasons. First, BOHB has shown to be slightly inferior to ASHA (Li et al., 2020a). Second, In our setting  $R \in \{1, 2, ..., 5\}$  and  $\eta$  is set to be more aggresive. As a result, only two SHA brackets at most can be exploited in the HyperBand, thus limiting its effectiveness.

Algorithm 1 Time-Series AutoAugment (TSAA) **Inputs:** partial train factor  $\beta$ , resources R, r, max trials  $T_{\text{max}}$ , reduction factor  $\eta$ , and k best DA sub-policies  $\Lambda \leftarrow \emptyset$  $\{\text{empty set into }\Lambda\}$  $\omega_{\text{share}}, R \leftarrow \text{partial solve Eq. 4 with } \beta$ STATE  $\omega_0 \leftarrow \omega_{\text{share}}$ {initialize the weights  $\omega_0$  using the partial solution} for i = 1 to  $T_{\text{max}}$  do  $\theta_i \leftarrow \text{solve Eq. } 3 \text{ with TPE}(\Theta, \omega_{i-1})$  $w_i \leftarrow \text{fine-tune Eq. 4}$  with  $\omega_{\text{share}}$  and  $\text{ASHA}(r, R, \eta)$  $\Lambda \leftarrow \Lambda \cup \left\{ \left[ \theta_i, \ \mathcal{L}_{\text{val}}(\omega_i, \theta_i) \right] \right\}$ {add found policy and loss to  $\Lambda$ } end for  $p_{\theta^*} \leftarrow k$  best sub-policies  $\theta_i$  from  $\Lambda$  $\omega^* \leftarrow \text{fine-tune } \mathcal{L}_{\text{tr}}(\theta^* \sim p_{\theta^*})$ **return**  $p_{\theta^*}, \theta^*, \omega^*$  {return the optimal DA distribution, policy, and network weights}

# 5 Results

In what follows, we provide a comprehensive overview of our experimental setup, including models, datasets, and implementation details followed by evaluations of our approach. In the supplementary material, we offer additional information on hyperparameters (App. C), and extended results (App. E.1).

#### 5.1 Models and datasets

We extensively evaluate the performance of our Time-Series AutoAugment (TSAA) framework. To this end, we selected some of the most recent prominent time-series forecasting models. We consider the baseline architectures: **N-BEATS** (Oreshkin et al., 2020), a deep neural architecture based on backward and forward residual links and a very deep stack of fully-connected layers. **Informer** (Zhou et al., 2021) adapts the Transformer (Vaswani et al., 2017) architecture to time-series forecasting tasks, with a new attention mechanism. **Autoformer** (Wu et al., 2021) exchanges the self-attention module for an autocorrelation mechanism and introduces time-series decomposition as part of the model's encoding. Finally, **FEDformer** (Zhou et al., 2022) enables capturing more important details in time-series through frequency domain mapping.

For each of the given baseline models, we apply TSAA on six commonly-used datasets in the literature of long-term time-series forecasting: (1) **ETTm2** (Zhou et al., 2021) contains electricity transformer oil temperature data alongside 6 power load features. (2) **Electricity** (Zhou et al., 2021) is a collection of hourly electricity consumption data over the span of 2 years. (3) **Exchange** (Lai et al., 2018) consists of 17 years of daily foreign exchange rate records representing different currency pairs. (4) **Traffic** (Zhou et al., 2021) is an

hourly reported sensor data containing information about road occupancy rates. (5) Weather (Zhou et al., 2021) contains 21 different meteorological measurements, recorded every 10 minutes for an entire year. (6) ILI (Wu et al., 2021) includes weekly recordings of influenza-like illness patients.

We summarize in Tab. 5.1 the different datasets and their attributes such as their sampling *frequency*, variates which determine the number of channels in each example, the total number of *timesteps* in each dataset, the different *horizon* lengths used for forecasting, and lastly the *lookback* period which is the input length used for the prediction.

			Dataset Summary	у	
dataset	frequency	variates	total timesteps	horizon	lookback period
ETTm2	15 minutes	7	69,680	96, 192, 336, 720	96
Electricity	hourly	321	26,304	96,192,336,720	96
Exchange	daily	8	7,588	96,192,336,720	96
Traffic	hourly	862	17,544	96,192,336,720	96
Weather	10 minutes	21	52,696	96,192,336,720	96
ILI	weekly	7	966	24,  36,  48,  60	36

#### 5.2 Implementation details

**Baselines.** We train all models based on the implementation and architecture details as they appear in (Oreshkin et al., 2020) for N-BEATS and (Zhou et al., 2021; Wu et al., 2021; Zhou et al., 2022) for the Transformer-based models. The model weights are optimized with respect to the mean squared error (MSE) using the ADAM optimizer (Kingma & Ba, 2015) with an initial learning rate of  $10^{-3}$  for N-BEATS and  $10^{-4}$  for Transformer-based models. The maximum number of epochs is set to 10 allowing early-stopping with a patience parameter of 3. The reported baseline results are obtained using our environment and hardware, and they may slightly differ from the reported values for the respective methods. Every experiment is run on three different seed numbers, and the results are averaged over the runs. The Pytorch library (Paszke et al., 2019) is used for all model implementations, and executed with NVIDIA GeForce RTX 3090 24GB.

**Method.** We use Optuna (Akiba et al., 2019) for the implementations of TPE and ASHA. The number of trials  $T_{\text{max}}$  is set to 100. For TPE, In order to guarantee aggressive exploration at the beginning, we run the first 30% of trials with random search. For ASHA, r and  $\eta$  are set globally to 1 and 3 respectively. The maximum resource parameter R, representing the epochs, is set differently for each experiment, due to the baseline's early-stopping.

After the augmentation policy search is finalized, a maximum of k best policies are selected to obtain  $p_{\theta^*}$ , where k = 3, and the final model is *fine-tuned* with  $\theta^* \sim p_{\theta^*}$  using the shared weights  $\omega_{\text{share}}$ . We opt to fine-tune the model and not re-train from random weights so that the final model training matches our optimization process as close as possible. Indeed, Cubuk et al. (2020) discuss the potential differences between the final model behavior in comparison to the performance of the intermediate proxy tasks, i.e., the models obtained during optimization. As the similarity in performance between these models and the final model is not guaranteed, a natural choice is to similarly train the proxy tasks and the final model, as we propose.

Augmentations. Each transformation includes a different increasing or decreasing magnitude range which are all mapped to the range [0, 1]. This way, m = 0 implies the identity and m = 1 is the maximum scale. To eliminate cases of the identity being repeatedly chosen, we replace the lower bound in the range with an  $\epsilon > 0$  such that for all transformations in the search space only m > 0 is possible. The transformations *Trend* scale and Seasonality scale require computing the seasonality and trend components; we pre-compute these factors using the decomposition in STL (Cleveland et al., 1990) and treat it as part of the input data. Each augmentation is applied before the input is fed to the model, namely, on the input x and the target y of the train data batches.

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		Info	rmer	Autof	ormer	FEDfo	rmer-w	FEDfe	ormer-f		TS	AA	
		MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$MSE\%\uparrow$	$MAE\%\uparrow$
2	96	0.545	0.588	0.231	0.310	0.205	0.290	0.189	0.282	0.187	0.274	1.058	2.837
$ETTm_2$	192	1.054	0.808	0.289	0.346	0.270	0.329	0.258	0.326	0.255	0.314	1.163	3.681
Ę	336	1.523	0.948	0.341	0.375	0.328	0.364	0.323	0.363	0.304	0.350	5.882	3.581
되	720	3.878	1.474	0.444	0.434	0.433	0.425	0.425	0.421	0.398	0.403	6.353	4.276
ty	96	0.336	0.416	0.200	0.316	0.196	0.310	0.185	0.300	0.183	0.297	1.081	1.000
Electricity	192	0.360	0.441	0.217	0.326	0.199	0.310	0.201	0.316	0.195	0.309	2.010	0.323
set:	336	0.356	0.439	0.258	0.356	0.217	0.334	0.214	0.329	0.208	0.323	2.804	1.824
Ele	720	0.386	0.452	0.261	0.363	0.248	0.357	0.246	0.353	0.238	0.348	3.252	1.416
ee	96	1.029	0.809	0.150	0.281	0.151	0.282	0.142	0.271	0.143	0.272	-0.704	-0.369
Exchange	192	1.155	0.867	0.318	0.409	0.284	0.391	0.278	0.383	0.270	0.378	2.878	1.305
cch	336	1.589	1.011	0.713	0.616	0.442	0.493	0.450	0.497	0.459	0.504	-3.846	-2.231
É	720	3.011	1.431	1.246	0.872	1.227	0.868	1.181	0.841	1.213	0.842	-2.710	-0.119
	96	0.744	0.420	0.615	0.384	0.584	0.368	0.577	0.361	0.565	0.352	2.080	2.493
Traffic	192	0.753	0.426	0.670	0.421	0.596	0.375	0.610	0.379	0.571	0.351	4.195	6.400
Dra	336	0.876	0.495	0.635	0.392	0.590	0.365	0.623	0.385	0.584	0.359	1.017	1.644
Ľ.,	720	1.011	0.578	0.658	0.402	0.613	0.375	0.632	0.388	0.607	0.368	0.979	1.867
H	96	0.315	0.382	0.259	0.332	0.269	0.347	0.236	0.316	0.180	0.256	23.729	18.987
Weather	192	0.428	0.449	0.298	0.356	0.357	0.412	0.273	0.333	0.252	0.311	7.692	6.607
/ea	336	0.620	0.554	0.357	0.394	0.422	0.456	0.332	0.371	0.296	0.355	10.843	4.313
М	720	0.975	0.722	0.422	0.431	0.629	0.570	0.408	0.418	0.382	0.395	6.373	5.502
	24	5.349	1.582	3.549	1.305	2.752	1.125	3.268	1.257	2.760	1.123	-0.291	0.178
ILI	36	5.203	1.572	2.834	1.094	2.318	0.980	2.648	1.068	2.362	0.984	-1.898	-0.408
Π	48	5.286	1.594	2.889	1.122	2.328	1.006	2.615	1.072	2.264	0.988	2.749	1.789
	60	5.419	1.620	2.818	1.118	2.574	1.081	2.866	1.158	2.520	1.062	2.098	1.758

Table 1: Multivariate long-term time-series forecasting results on six datasets in comparison to five baseline models. Low MSE and MAE values are better, and high relative improvement MSE% and MAE% scores are better. Boldface text highlights the best performing models.

#### 5.3 Main results

In our experiments, we employ a similar setup to (Wu et al., 2021; Zhou et al., 2022), where the input length is 96 and the evaluated forecast horizon corresponds to 96, 192, 336, or 720. For ILI, we use input length 36 and horizons 24, 36, 48, 60. For a fair comparison, we re-produce all baseline results on our system, and the augmentations are applied on the same generated batches as the baseline. Our main results are summarized in Tab. 1 and Tab. 2 including all the baseline results and TSAA. For TSAA, we include the best performing model trained on all baseline architectures. The full results for every architecture with and without TSAA are provided in the appendix spanning tables 6-14. We detail the mean absolute error (MAE) and mean squared error (MSE) (Oreshkin et al., 2020). Lower values are better, and boldface text highlights the best performing model for each dataset and metric. For TSAA, we also include the *relative improvement* percentage, i.e.,  $100 \cdot (e_b - e_n)/e_b$ , where  $e_b$  is the best baseline error and  $e_n$  is our result. We denote by MSE% and MAE% the relative improvement of MSE and MAE, respectively. A higher improvement is better.

Multivariate time-series forecasting results. Based on the results in Tab. 1, we observe that most datasets benefit from automatic augmentation, where in the vast majority of cases, TSAA improves the baseline scores. It is apparent that TSAA yields stronger performance in particular in the long-horizon settings with 6.35% (0.425  $\rightarrow$  0.398) reduction in ETTm2, 3.25% (0.246  $\rightarrow$  0.238) reduction in Electricity, and 2.1% (2.328  $\rightarrow$  2.264) reduction in ILI. One of the more prominent results appears for Weather 96 and 336 with reductions in MSE of 23.73% (0.236  $\rightarrow$  0.180) and 10.84% (0.332  $\rightarrow$  0.296), respectively. For the Exchange dataset, TSAA obtains slightly higher errors with respect to the FEDformer-w baseline. Overall, TSAA achieves the *best results* in 39 error metrics, in comparison to FEDformer-f and FEDformer-w with 4 and 5 best models, respectively.

Univariate time-series forecasting results. Similar to the multivariate results, most long horizon settings benefit from TSAA. With a 21.74% average reduction across all datasets with a horizon of 720. Furthermore, the results that stand out the most are the MSE and MAE reductions in Weather, with a

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		Info	rmer	Autof	ormer	FEDfo	rmer-f	N-BE	ATS-I	N-BEA	ATS-G		Т	SAA	
		MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE	$\mathrm{MSE}{\downarrow}$	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$MAE\%\uparrow$
5	96	0.085	0.225	0.123	0.270	0.068	0.198	0.080	0.213	0.080	0.210	0.068	0.192	0.000	3.030
E.	192	0.130	0.282	0.141	0.289	0.096	0.238	0.103	0.240	0.110	0.250	0.096	0.237	0.000	0.420
ETTm2	336	0.161	0.314	0.170	0.319	0.138	0.286	0.162	0.312	0.172	0.320	0.139	0.290	-0.725	-1.399
되	720	0.221	0.373	0.206	0.353	0.189	0.335	0.199	0.347	0.201	0.353	0.187	0.336	1.058	-0.299
ty	96	0.261	0.367	0.454	0.508	0.244	0.364	0.326	0.402	0.324	0.397	0.244	0.354	0.000	2.747
ici.	192	0.285	0.386	0.511	0.532	0.276	0.382	0.350	0.417	0.363	0.420	0.277	0.368	-0.362	3.665
sct:	336	0.324	0.417	0.739	0.651	0.347	0.432	0.393	0.440	0.392	0.443	0.310	0.394	4.321	5.516
Electricity	720	0.632	0.612	0.673	0.610	0.408	0.473	0.458	0.490	0.489	0.502	0.378	0.447	7.353	5.497
ee	96	0.490	0.554	0.149	0.308	0.133	0.284	0.210	0.344	0.223	0.351	0.093	0.236	30.075	16.901
ang	192	0.790	0.721	0.290	0.415	0.292	0.419	1.130	0.840	0.783	0.675	0.215	0.352	25.862	15.181
Exchange	336	2.146	1.223	0.708	0.662	0.477	0.532	1.587	1.047	2.622	1.266	0.532	0.572	-11.530	-7.519
Ex	720	1.447	1.008	1.324	0.892	1.304	0.882	0.870	0.747	2.588	1.303	0.527	0.594	39.425	20.482
	96	0.262	0.348	0.266	0.372	0.210	0.318	0.181	0.268	0.159	0.240	0.158	0.239	0.629	0.417
Traffic	192	0.294	0.376	0.272	0.379	0.206	0.311	0.177	0.263	0.181	0.264	0.160	0.243	9.605	7.605
Ira	336	0.308	0.390	0.261	0.374	0.217	0.322	0.180	0.271	0.155	0.239	0.156	0.244	-0.645	-2.092
Ľ '	720	0.364	0.440	0.269	0.372	0.243	0.342	0.226	0.316	0.212	0.304	0.189	0.279	10.849	8.224
H	96	0.005	0.048	0.009	0.078	0.009	0.073	0.003	0.044	0.003	0.043	0.001	0.024	66.667	44.186
Weather	192	0.004	0.051	0.009	0.068	0.007	0.067	0.004	0.046	0.004	0.047	0.001	0.027	75.000	41.304
/ea	336	0.003	0.043	0.006	0.058	0.006	0.062	0.004	0.048	0.005	0.054	0.002	0.035	33.333	18.605
М	720	0.004	0.049	0.007	0.063	0.006	0.060	0.004	0.049	0.004	0.048	0.002	0.034	50.000	29.167
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civariate	۲ 40			30		40			30		20		20		
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Table 2: Univariate long-term time-series forecasting results on five datasets in comparison to five baseline models. Low MSE and MAE values are better, and high relative improvement MSE% and MAE% scores are better. Boldface text highlights the best performing models.

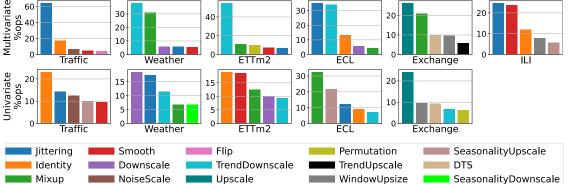


Figure 3: The best five performing transformations per dataset attained with TSAA, measured with the percentage proportion of the selected operations (%ops). Each colored bar represents a transformation and the y-axis represents the percentage proportion the given transformation accounts for.

66%, 75%, 33, 50%%, and respectively 44.2%, 41.3%, 17.6%, 29.2% performance improvements corresponding to the 96, 192, 336, and 720 horizons. Further, it is evident in Tabs. 10-14, that the improvements in the Weather dataset are not limited to a specific baseline architecture. In contrast to the multivariate setting, TSAA achieves significantly better scores on the Exchange dataset with average improvements of 21% and 11.27% for the MSE and MAE metrics. Notably, the results in the univariate case are slightly more involved than the multivariate setting such that that only Weather always benefits from TSAA, whereas the results for other datasets are mixed. Still, TSAA shows a positive advantage over all baseline models. In particular, TSAA obtained the best models for 32 error metrics, whereas FEDformer-f and N-BEATS-G are better in 9 and 2 measures.

**Policy analysis.** The most noticeable selected transformations are illustrated in Fig. 3. It is evident that the transformations Trend Downscale, Jittering, Mixup, and Smoothing are some of the prominent selections in the overall setup. Trend Downscale accounts for more than 30% of the operations in ETTm2, Weather

and Electricity; this may indicate that the deep models tend to overestimate the trend, and thus it requires downscaling. Jittering and Smoothing on the other hand, do not violate time-series characteristics such as trend or seasonality but still promote diversity within the given dataset, where Smoothing is approximately the opposite of Jittering. Notably, Mixup appeared as one of the five most important transformations for four and three datasets in the multivariate and univariate settings, respectively. We believe that Mixup is beneficial to TSF since it samples from a vicinal distribution whose variability is higher than the original train set. We show in Fig. 5 the outcome with and without TSAA compared to the ground truth, showing that employing custom policies per signal may significantly improve forecasting.

#### 6 Ablation and Analysis

#### 6.1 Parameter selection

**Choice of**  $\beta$ . In what follows, we motivate our choice for the  $\beta$  hyperparameter which dictates for how many epochs we pre-train the baseline architecture to obtain  $\omega_{\text{share}}$ . To this end, we investigate the effect of utilizing different values of  $\beta$ . We consider four different settings: 1) full training with augmentation, i.e.,  $\beta = 0.0, 2$  half training with augmentation, i.e.,  $\beta = 0.5, 3$  augmentation applied only in the last epoch, 4) baseline training with no augmentation, i.e.,  $\beta = 1.0$ . We used TSAA on the ILI with respect to N-BEATS-G in the univariate setting, and Informer, Autoformer and FEDformer-f in the multivariate case, as well as on multivariate ETTm2 with Autoformer and FEDformer-f. We plot the averaged results of these architectures in Fig. 4A, showing four colored curves corresponding to the various forecasting horizons 24/96, 36/192, 48/336 and 60/720 with colors blue, orange, green and red, respectively. The best models are obtained for  $\beta = 0.0$  and  $\beta = 0.5$ , that is, full- and half-augmented training. Somewhat surprisingly, two of the four best forecasting horizons (36/192, 48/336) are obtained for  $\beta = 0.5$ . Overall, the fully augmented model (i.e.,  $\beta = 1.0$ ) attains a 5.1% average improvement over the baseline, whereas using  $\beta = 0.5$  yields a 5.3% average improvement. Thus, fully training with augmentation achieves similar performance to half training, while requiring significantly more resources. Indeed, Tian et al. (2020a) employs a similar strategy, and thus, we propose to generate  $\omega_{\text{share}}$  after training for half of the active epochs, and we fine-tune the model using optimal augmentation policies.

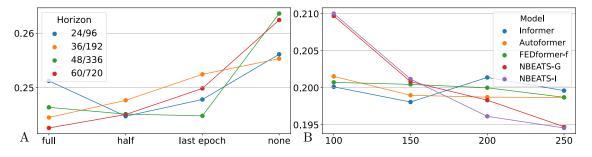


Figure 4: A) The normalized average performance measures as a function of different  $\beta$  values. Our results indicate that  $\beta = 0.5$  (half) attains the best computational resources to performance gain ratio. B) We plot the normalized average performance measures as a function of different  $T_{\text{max}}$  values. As the number of trials grows, we observe better overall performance.

Reduction factor and linked operations. In Sec. 3, we introduced the reduction factor  $\eta$  that controls the number of kept runs in ASHA. Additionally, we discuss in Sec. 4 that every sub-policy is composed of *n* linked operations of time-series augmentations. Here, we would like to empirically justify our choices for these two hyperparameters. Our ablation study uses the ILI dataset on the 36, 48, 60 forecasting tasks, with N-BEATS-G for the univariate case, and Informer, Autoformer, and FEDformer-f for the multivariate configuration. We test the values  $\eta \in \{2, 3\}$  and  $n \in \{1, 2\}$ . Every experiment is repeated three times, and we analyze the average results.

Overall, we propose to use the values  $\eta = 3$  and n = 2 due to the following observations arising from our experiments. The improvement difference between  $\eta = 2$  and  $\eta = 3$  is only 0.12% in favor of  $\eta = 2$ , thus

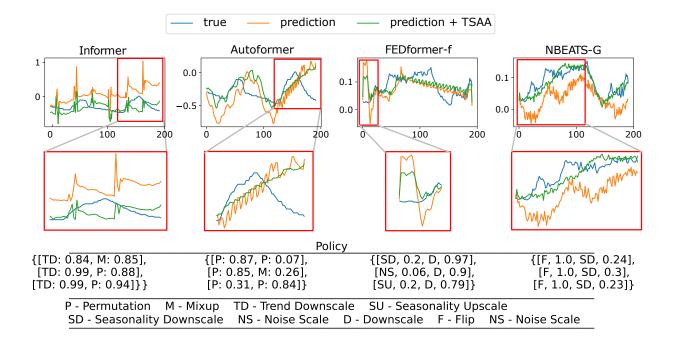


Figure 5: The ground truth, prediction, and prediction with augmentation attained with TSAA applied to the same forecast target in ETTm2 with Informer, Autoformer multivariate, and Weather with FEDformer-f and NBEATS-G univariate. It is shown that augmentation can assist the different models to achieve more accurate predictions with better alignment, reduce excessive noise, and curtail outliers. The attained policies are given underneath each plot.

suggesting that neither exhibits a statistically-dominant performance advantage. Nevertheless,  $\eta = 3$  is resource efficient as it reduces the amount of kept runs  $1/\eta$  by 16.67%. Moreover, a single operation n = 1attains a **6.4%** average improvement compared to the baseline, whereas two linked operations n = 2 yield a **7.4%** average improvement.

**Convergence of TSAA.** In our experiments, we look for good augmentation policies for  $T_{\text{max}} = 100$  iterations. Here, we explore the effect of this value on the performance of the resulting models. We evaluate our framework on the ILI dataset with the architectures Informer, Autoformer, FEDformer-f, N-BEATS-G and N-BEATS-I using varying values for  $T_{\text{max}} \in \{100, 150, 200, 250\}$ . Intuitively, greater  $T_{\text{max}}$  values may result in an improved convergence and a better overall performance as the framework can explore and exploit a larger variety of configurations from the search space. Indeed, we show in Fig. 4B the normalized average MSE values obtained for the various tests. We observe an MSE reduction of 1% for the transformer-based models when increasing  $T_{\text{max}} = 100$  to  $T_{\text{max}} = 250$ . The N-BEATS architecture benefited more and achieved a 7.25% reduction. In conclusion, the hyperparameter  $T_{\text{max}}$  presents a natural trade-off to the practitioner: higher  $T_{\text{max}}$  values generally lead to better performance at a higher computational cost, whereas lower values are less demanding computationally but present inferior performance.

#### 6.2 AutoAugment Method Comparison

We compare TSAA to other efficient AutoAugment methods via an experiment that shows that both Fast AutoAugment (Lim et al., 2019) and RandAugment (Cubuk et al., 2020) are *inconsistent* and thus inferior to TSAA. In this experiment, we tested the performance of deploying Fast AutoAugment and RandAugment with the same search space, with the exception of discretized magnitude ranges so RandAugment falls in line with the original method. The given methods were tested on Autoformer and FEDformer-f multivariate together with datasets: ETTm2, Traffic, Weather, and ILI. The results are provided in Tab. 3. For Fast AutoAugment

		Best B	aseline	Fast	AA	RandAu	ıgment	TS	AA
	Metric	MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE
5	96	0.189	0.282	0.197	0.279	0.192	0.282	0.187	0.274
ETTm2	192	0.258	0.326	0.262	0.319	0.257	0.323	0.255	0.314
Ę	336	0.323	0.363	<u>0.322</u>	0.356	0.326	0.364	0.311	0.350
斑	720	0.425	0.421	<u>0.415</u>	<u>0.407</u>	0.427	0.420	0.406	0.403
	96	0.577	0.361	0.655	0.410	0.590	0.376	0.577	0.362
Ψ	192	<u>0.610</u>	0.379	0.652	0.408	0.622	0.390	0.601	0.371
Traffic	336	0.623	0.385	0.674	0.421	0.626	0.392	0.619	0.383
Γ.	720	0.632	0.388	0.705	0.427	0.643	0.396	0.632	0.388
I	96	0.236	0.316	0.191	0.252	0.203	0.275	0.207	0.285
Weather	192	0.273	0.333	0.240	0.290	0.267	0.332	0.252	0.311
/ea	336	0.332	0.371	0.290	0.321	0.328	0.364	<u>0.313</u>	0.355
M	720	0.408	0.418	0.363	0.367	0.398	0.413	0.382	0.395
	24	3.268	1.257	4.671	1.603	3.160	1.234	3.150	1.219
Ę	36	2.648	1.068	3.835	1.375	2.457	1.019	2.578	1.049
ILLI	48	2.615	1.072	3.694	1.359	2.558	1.045	<u>2.609</u>	1.069
	60	2.866	1.158	3.855	1.410	2.775	1.108	<u>2.805</u>	<u>1.140</u>
	%AI	0.0	0.0	-9.5	-4.88	1.67	1.22	3.33	3.1

Table 3: Comparison of automatic augmentation approaches including TSAA, Fast AutoAugment and RandAugment. We denote by %AI the average improvement in percentage.

we set K = 3 folds which control the number of subsets, each subset explores and exploits 100 augmentation trials. For RandAugment, we discretize the magnitude range to 8 bins and utilize the partial train scheme with the same  $\beta$  as in TSAA, to allow RandAugment to benefit from the same approach. While it is shown that Fast AutoAugment and RandAugment are superior on Weather and ILI respectively, they attain inferior results on the other datasets. Nevertheless, TSAA is shown to be most effective on Traffic and ETTm2 and second-best on ILI and Weather. Additionally, TSAA maintains a consistent improvement across all datasets providing a 3.33% average MSE reduction as opposed to RandAugment which offers approximately half of that, or Fast AutoAugment with a negative average MSE reduction. In conclusion, TSAA is more consistent with better overall performance when compared to prominent AutoAugment methods in the time-series domain.

# 7 Conclusion

In this work, we study the task of data augmentation in the setting of time-series forecasting. While recent approaches based on automatic augmentation achieved state-of-the-art results in image classification tasks, problems involving arbitrary time-series information received less attention. Thus, we propose a novel time-series automatic augmentation (TSAA) method that relaxes a difficult bilevel optimization. In practice, our framework performs a partial training of the baseline architecture, followed by an iterative split process. Our iterations alternate between finding the best DA policy for a given set of model weights, to fine-tuning the model based on a specific policy. In comparison to several strong methods on multiple univariate and multivariate benchmarks, our framework improves the baseline results in the majority of prediction settings.

In the future, we would like to explore better ways for relaxing the bilevel optimization, allowing to train an end-to-end model (Li et al., 2020b; Zheng et al., 2022). Further, we believe that our approach would benefit from stronger time-series augmentation transformations. Thus, one possible direction forward is to incorporate learnable DA modules, similar in spirit to filters of convolutional models.

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# **A** Appendix

In what follows, we present additional details the transformations used in our method (App. B), hyperparameter values (App. C), complexity analysis of TSAA (App. D), and lastly, we provide extended result tables for every baseline alongside TSAA (App. E.1).

### **B** Time-series transformations

In this section, we offer a detailed description of the different time-series transformations, which can be found in Tab. 4 and depicted in Fig. 6 with m = 0.85 compared to the original signal. For each of the transformations *Trend scale*, *Scale*, *Seasonality scale*, *Window warping*, we use two separate and independent transformations to demonstrate an increase or decrease of the given effect.

Table 4: Our search space is composed of the following time-series transformations and their associated magnitude range.

Transformation	Description	Range of magni- tudes
Jittering	Adds white noise with $\sigma$ controlled by $m$ (Um et al., 2017). *	[0,0.1]
Trend scale	Multiplies the trend component by $m$ . *	[1,10], [0,1]
Scale	Multiplies the entire series by $m$ (Um et al., 2017).	[1,3], [0.3,1]
Seasonality scale	Multiplies the seasonality component by $m$ .	[1,3], [0,1]
Smooth	Performs low-pass filtering with a convolution kernel, where $m$ controls the kernel size.	[0,11]
Noise scale	Performs high-pass filtering with a second-order con- volution kernel to extract the difference, which is then multiplied by $m$ and added back to the original series.	[0,1]
Permutation	Exchanges two non-overlapping time intervals, such that the interval size is controlled by $m$ . (Um et al., 2017).	[0,0.3]
Dynamic time stretching	Manipulates the length of different non-overlapping time intervals, where $m$ controls the manipulation magnitude. (Nguyen et al., 2020).	[1,5]
Window warping	Manipulates the length of the entire window (Um et al., 2017).	[1,1.5], [0.5,1]
Mixup	Linearly interpolates between two series, $m$ controls the contribution of each series (Zhang et al., 2018).	[0, 0.5]
Identity	Returns the original series.	None
Flip	Flip the series relative to the value location by multiplying by $(-1)$ (Iwana & Uchida, 2021). *	$\{0,1\}$
Reverse	Change the relative location of the time steps to span from end to start.	$\{0,1\}$

\* marks a transformation implemented with min-max scaling to ensure equal relative changes.

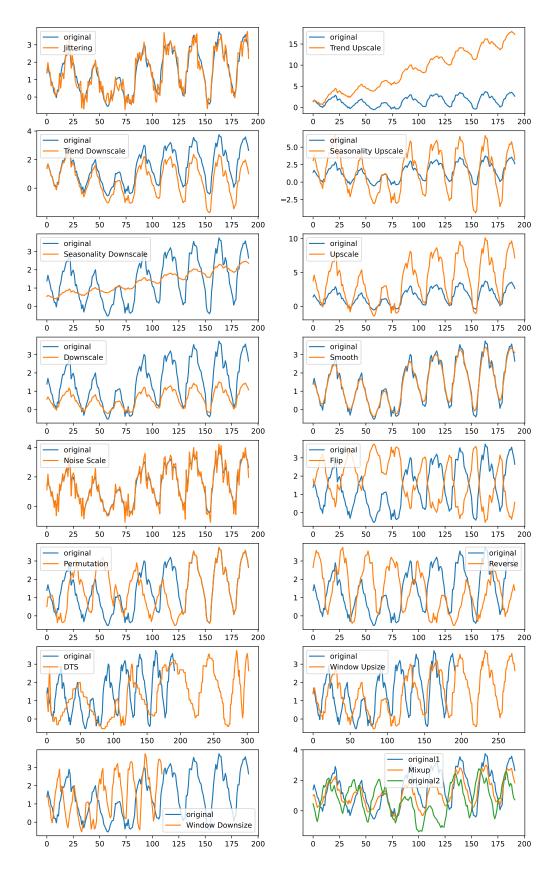


Figure 6: We demonstrate the effect of different transformations when applied to the same example from the Electricity dataset. Blue and orange represent the original signal and its transformed version, respectively.

# C TSAA hyperparameters

We detail in Tab. 5 the hyperparameter values we used in the evaluation of TSAA.

Table 5: Hyperparameter values used in the evaluation of TSAA.

	N	Iodel Para	nete	ers -	TSA	4A				
	exploration									
$T_{max}$	trials fraction	m range	n	$\eta$	r	resource type	$\beta$	k		
100	0.3	(0,1]	2	3	1	epoch	0.5	3		

# **D** Complexity

A straightforward upper bound of our method is given by  $\mathcal{O}((1-\beta)KT_{max})$  evaluated in epochs, where K,  $(1-\beta)$ , and  $T_{max}$  correspond to the number of active epochs the model trains for, the fraction of K to be used for fine-tuning, and the maximum number of trials, respectively. However, for TSAA to practically reach such an upper bound when K > 2 would require each trial to outperform the preceding trials, thus avoiding being pruned by ASHA. This setup is very unlikely for the following reasons: (1) a fraction size 0.3 of  $T_{max}$  of starting trials are manually dedicated to random search to promote aggressive exploration at the start. (2) To the best of our knowledge Bayesian Optimization does not guarantee monotonic improvement and inherently promotes exploration (Bergstra et al., 2011). (3)  $\mathcal{L}_{val}(\theta, w^*)$  is not promised to be convex with respect to  $\theta$ , making it even more difficult to attain a monotonic improvement. In our empirical evaluations, we have observed different operations with different transformations being selected, as opposed to a single policy being repeatedly selected, which strengthens our claim. Further, we would like to share a solid example from our empirical experiments with FEDformer-w applied to Electricity with a horizon of 336. This setup is considered resource expensive as one epoch may take as long as 20 minutes on a single RTX3090. In the given setup, K was set to 8 and  $\beta = 0.5$  as defined in the hyperparameter table Tab. 5. Therefore, according to the bound mentioned above, the total number of epochs would be 400 epochs. However, the use of ASHA with Bayesian optimization reduced it to 170, proving the computational impact. For comparison, applying a naive approach without ASHA and  $\beta$  will result in a total number of 800 training epochs.

### E Extended results

In this section, we provide the performance of TSAA for each individual model featured in Tab. 1 and Tab. 2 in the main text. We can observe from the multivariate results that Informer benefits the most from TSAA, with the 720 horizon in particular. On the other end, TSAA struggles to achieve significant improvements in FEDformer-f, especially for the Exchange dataset. In the univariate setting, unlike the multivariate setting, the models NBEATS-G and NBEATS-I gain large improvement rates in Exchange thanks to TSAA. Overall, we can conclude that all models and datasets exhibit a degree of improvement with the support of TSAA.

# E.1 TSF results

Tabs. 6, 7, 8, 9, 10, 11, 12, 13, 14 detail the extended results for every baseline architecture and dataset we considered in the main text.

Table 6:	Informer multivariate
Informer	TSAA

		Info	rmer		Т	SAA	
		MSE	MAE	$MSE\downarrow$	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$
2	96	0.545	0.588	0.224	0.321	58.899	45.408
$ETTm_2$	192	1.054	0.808	0.270	0.355	74.383	56.064
E	336	1.523	0.948	0.304	0.374	80.039	60.549
Ē	720	3.878	1.474	0.398	0.435	89.737	70.488
Electricity	96	0.336	0.416	0.324	0.407	3.571	2.163
ric	192	0.360	0.441	0.336	0.419	6.667	4.989
ect	336	0.356	0.439	0.347	0.429	2.528	2.278
Ē	720	0.386	0.452	0.381	0.448	1.295	0.885
e	96	1.029	0.809	0.512	0.569	50.243	29.666
ang	192	1.155	0.867	0.791	0.696	31.515	19.723
Exchange	336	1.589	1.011	1.040	0.763	34.550	24.530
Ê	720	3.011	1.431	1.213	0.842	59.714	41.160
~	96	0.744	0.420	0.723	0.408	2.823	2.857
Traffic	192	0.753	0.426	0.735	0.414	2.390	2.817
Ira	336	0.876	0.495	0.811	0.462	7.420	6.667
`	720	1.011	0.578	0.985	0.566	2.572	2.076
ы	96	0.315	0.382	0.180	0.256	42.857	32.984
Weather	192	0.428	0.449	0.253	0.331	40.888	26.281
Vea	336	0.620	0.554	0.296	0.361	52.258	34.838
5	720	0.975	0.722	0.392	0.426	59.795	40.997
	24	5.349	1.582	5.313	1.559	0.673	1.454
ILI	36	5.203	1.572	5.260	1.581	-1.096	-0.573
Π	48	5.286	1.594	5.415	1.623	-2.440	-1.819
	60	5.419	1.620	5.300	1.593	2.196	1.667

	Ta	able 8	: FED	forme	r-f mu	ltivaria	te
			ormer-f			ISAA	
		MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$
5	96	0.189	0.282	0.187	0.274	1.058	2.837
ETTm2	192	0.258	0.326	0.255	0.314	1.163	3.681
E	336	0.323	0.363	0.311	0.350	3.715	3.581
ΕÌ	720	0.425	0.421	0.406	0.403	4.471	4.276
ty	96	0.185	0.300	0.185	0.300	0.000	0.000
i:	192	0.201	0.316	0.201	0.316	0.000	0.000
Electricity	336	0.214	0.329	0.214	0.329	0.000	0.000
ĕ	720	0.246	0.353	0.246	0.353	0.000	0.000
ee.	96	0.142	0.271	0.149	0.277	-4.930	-2.214
ang	192	0.278	0.383	0.273	0.380	1.799	0.783
Exchange	336	0.450	0.497	0.517	0.540	-14.889	-8.652
É	720	1.181	0.841	2.440	1.343	-106.605	-59.691
	96	0.577	0.361	0.577	0.362	0.000	-0.277
Traffic	192	0.610	0.379	0.601	0.371	1.475	2.111
Гra	336	0.623	0.385	0.619	0.383	0.642	0.519
	720	0.632	0.388	0.632	0.388	0.000	0.000
r	96	0.236	0.316	0.207	0.285	12.288	9.810
Weather	192	0.273	0.333	0.252	0.311	7.692	6.607
/ea	336	0.332	0.371	0.313	0.355	5.723	4.313
5	720	0.408	0.418	0.382	0.395	6.373	5.502
	24	3.268	1.257	3.150	1.219	3.611	3.023
ILI	36	2.648	1.068	2.578	1.049	2.644	1.779
П	48	2.615	1.072	2.609	1.069	0.229	0.280
	60	2.866	1.158	2.805	1.140	2.128	1.554

	0	0.000	01.010	10.1.20
	1.040	0.763	34.550	24.530
	1.213	0.842	59.714	41.160
0.	723	0.408	2.823	2.857
0.'	735	0.414	2.390	2.817
0.8	811	0.462	7.420	6.667
0.9	985	0.566	2.572	2.076
0.18	80	0.256	42.857	32.984
0.2	53	0.331	40.888	26.281
0.2	96	0.361	52.258	34.838
0.	392	0.426	59.795	40.997
5.	313	1.559	0.673	1.454
5.	260	1.581	-1.096	-0.573
	415	1.623	-2.440	-1.819
ļ	0.410			
5	.300	1.593	2.196	1.667
5	5.415 5 <b>.300</b> orme	1.593 r-f mu	2.196 Itivaria	
5. foi	300 rme	1.593 r-f mu	ltivaria	te
5. fo м	.300 rme ⊠SE↓	1.593 <u>r-f mu</u> T	ltivaria SAA	te
5. for M	300 rme SE↓ 187	1.593 r-f mu MAE↓	ltivaria SAA MSE%↑	te MAE%↑
5 fo M 0 0	.300 orme ISE↓ .187 .255	1.593 <u>r-f mu</u> MAE↓ 0.274	ltivaria SAA MSE%↑ 1.058	te MAE%↑ 2.837
5. <u>fo</u> M 0. 0.	300 rme SE↓ 187 255 311	1.593 <u>r-f mu</u> MAE↓ 0.274 0.314	ltivaria SAA MSE%↑ 1.058 1.163	te MAE%↑ 2.837 3.681
5 fo 0 0 0	.300	1.593 r-f mu MAE↓ 0.274 0.314 0.350	ltivaria SAA MSE%↑ 1.058 1.163 3.715	te MAE%↑ 2.837 3.681 3.581
5. for M 0. 0. 0. 0. 0.	300 rme SE↓ 187 255 311 406 185	1.593 <u>r-f mu</u> MAE↓ 0.274 0.314 0.350 0.403	ltivaria SAA MSE%↑ 1.058 1.163 3.715 4.471	te MAE%↑ 2.837 3.681 3.581 4.276
5. M 0. 0. 0. 0. 0. 0.	.300 rme ISE↓ .187 .255 .311 .406	1.593 <u>r-f mu</u> MAE↓ 0.274 0.314 0.350 0.403 0.300	ltivaria SAA MSE%↑ 1.058 1.163 3.715 4.471 0.000	MAE%↑           2.837           3.681           3.581           4.276           0.000
5.: foi 0.: 0.: 0.: 0.: 0.:	300 rme SE↓ 187 255 311 406 185 201 214	1.593 <u>r-f mu</u> MAE↓ 0.274 0.314 0.350 0.403 0.300 0.316	ltivaria SAA MSE%↑ 1.058 1.163 3.715 4.471 0.000 0.000	MAE%↑           2.837           3.681           3.581           4.276           0.000           0.000
5. <u>for</u> M 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	300 rme SE↓ 187 255 311 406 185 201 214 246	1.593 <u>r-f mu</u> MAE↓ 0.274 0.314 0.350 0.403 0.300 0.316 0.329	ltivaria SAA MSE%↑ 1.058 1.163 3.715 4.471 0.000 0.000 0.000	MAE%↑           2.837           3.681           3.581           4.276           0.000           0.000           0.000
5. fo 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.	300 rme SE↓ 187 255 311 406 185 201	$\begin{array}{c} 1.593 \\ \hline r-f \ mu \\ \hline T \\ MAE\downarrow \\ 0.374 \\ 0.314 \\ 0.350 \\ 0.403 \\ 0.300 \\ 0.316 \\ 0.329 \\ 0.353 \end{array}$	ltivaria <sup>,</sup> 'SAA MSE%↑ 1.058 1.163 3.715 4.471 0.000 0.000 0.000 0.000	MAE%↑           2.837           3.681           3.581           4.276           0.000           0.000           0.000           0.000

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$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	84	5.48	8.658	0.293	0.211	0.310	0.231	96	~			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	91	5.49	6.920	0.327	0.269	0.346	0.289	192	Ë			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	67	4.26	5.572	0.359	0.322	0.375	0.341	336	L			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	<b>21</b>	6.22	7.658	0.407	0.410	0.434	0.444	720	E			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	30	4.43	6.000	0.302	0.188	0.316	0.200	96	ty			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	513	-0.61	-1.843	0.328	0.221	0.326	0.217	192	rici			
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	<b>24</b>	1.12	2.326	0.352	0.252	0.356	0.258		ect			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	06	3.30	4.981	0.351	0.248	0.363	0.261	720	ă			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	03	3.20	4.667	0.272	0.143	0.281	0.150	96	e			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	<i>)</i> 12	-3.91	-8.176	0.425	0.344	0.409	0.318	192	nag			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	)58	-4.05	-4.067	0.641	0.742	0.616	0.713	336	ch			
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	174	-34.17	-60.273	1.170	1.997	0.872	1.246	720	Ĥ			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	44	2.34	2.114	0.375	0.602	0.384	0.615	96				
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	88	1.18	1.045	0.416	0.663	0.421	0.670	192	ĕ			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	<b>76</b>	1.27	1.260	0.387	0.627	0.392	0.635	336	Гra			
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	746	-0.74	-0.608	0.405	0.662	0.402	0.658	720				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	48	12.04	16.602	0.292	0.216	0.332	0.259	96	H			
5 336 0.357 0.394 0.341 0.381 4.482 3.2 720 0.422 0.421 0.207 0.410 5.024 4.8	<b>18</b>	5.61	6.711	0.336	0.278	0.356	0.298	192	the			
5 790 0 499 0 491 0 207 0 410 5094 49	99	3.29	4.482	0.381	0.341	0.394	0.357	336	/ea			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	72	4.87	5.924	0.410	0.397	0.431	0.422	720	5			
24   <b>3.549</b> 1.305   3.565 <b>1.302</b> -0.451 <b>0.2</b>	30	0.23	-0.451	1.302	3.565	1.305	3.549	24				
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	77	2.37	2.823	1.068	2.754	1.094	2.834	36	Б			
$\exists$ 48   2.889 1.122   <b>2.856 1.114 1.142 0.7</b>	<b>13</b>	0.71	1.142	1.114	2.856	1.122	2.889	48	Π			
60 <b>2.818 1.118</b> 2.826 <b>1.118</b> -0.284 <b>0.0</b>	00	0.00	-0.284	1.118	2.826	1.118	2.818	60				

#### 9: FEDformer-w multivariate

	<u> </u>	<u>ble 9:</u>	FED	tormei	<u>-w mu</u>	iltivaria	<u>ite</u>
		FEDfo	rmer-w			SAA	
		MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$
5	96	0.205	0.290	0.199	0.280	2.927	3.448
L <sup>m</sup>	192	0.270	0.329	0.255	0.314	5.556	4.559
ETTm2	336	0.328	0.364	0.316	0.352	3.659	3.297
표	720	0.433	0.425	0.410	0.404	5.312	4.941
Electricity	96	0.196	0.310	0.183	0.297	6.633	4.194
rici	192	0.199	0.310	0.195	0.309	2.010	0.323
sct	336	0.217	0.334	0.208	0.323	4.147	3.293
Ē	720	0.248	0.357	0.238	0.348	4.032	2.521
e	96	0.151	0.282	0.144	0.272	4.636	3.546
an	192	0.284	0.391	0.270	0.378	4.930	3.325
Exchange	336	0.442	0.493	0.459	0.504	-3.846	-2.231
Ē	720	1.227	0.868	1.952	1.167	-59.087	-34.447
~	96	0.584	0.368	0.565	0.352	3.253	4.348
Traffic	192	0.596	0.375	0.571	0.351	4.195	6.400
Ira	336	0.590	0.365	0.584	0.359	1.017	1.644
	720	0.613	0.375	0.607	0.368	0.979	1.867
Ħ	96	0.269	0.347	0.213	0.291	20.818	16.138
Weather	192	0.357	0.412	0.274	0.339	23.249	17.718
/ea	336	0.422	0.456	0.335	0.379	20.616	16.886
5	720	0.629	0.570	0.406	0.423	35.453	25.789
	24	2.752	1.125	2.760	1.123	-0.291	0.178
ILI	36	2.318	0.980	2.362	0.984	-1.898	-0.408
П	48	2.328	1.006	2.264	0.988	2.749	1.789
	60	2.574	1.081	2.520	1.062	2.098	1.758

	Table 10: Informer univariate								
		rmer			SAA				
	MSE	MAE	MSE↓	MAE↓	$MSE\%\uparrow$	$MAE\%\uparrow$			
№ 96	0.085	0.225	0.085	0.226	0.000	-0.444			
<u>E</u> 192	0.130	0.282	0.128	0.279	1.538	1.064			
Cult 192 192 336 720	0.161	0.314	0.164	0.317	-1.863	-0.955			
720	0.221	0.373	0.221	0.371	0.000	0.536			
A:         96           192         192           336         720           B:         720           96         192           336         720           336         720	0.261	0.367	0.245	0.356	6.130	2.997			
-E 192	0.285	0.386	0.297	0.401	-4.211	-3.886			
<b>5</b> 336	0.324	0.417	0.433	0.485	-33.642	-16.307			
ā 720	0.632	0.612	0.707	0.644	-11.867	-5.229			
<sub>ඩ</sub> 96	0.490	0.554	0.149	0.307	69.592	44.585			
He 192	0.790	0.721	0.260	0.402	67.089	44.244			
-5 <u>3</u> 336	2.146	1.223	0.744	0.671	65.331	45.135			
년 720	1.447	1.008	0.527	0.594	63.580	41.071			
	0.262	0.348	0.254	0.342	3.053	1.724			
96 192 336 ⊥	0.294	0.376	0.284	0.367	3.401	2.394			
Ë 336	0.308	0.390	0.300	0.384	2.597	1.538			
720	0.364	0.440	0.326	0.409	10.440	7.045			
	0.005	0.048	0.003	0.043	40.000	10.417			
4 192 f	0.004	0.051	0.003	0.038	25.000	25.490			
S 336	0.003	0.043	0.004	0.047	-33.333	-9.302			
> 720	0.004	0.049	0.003	0.043	25.000	12.245			
Table 12: FEDformer-f univariate									
Т	FEDfc	ormer-f			SAA				
T			Dform   <sub>MSE↓</sub>			e MAE%↑			
96	FEDfc MSE 0.068	ormer-f MAE 0.198	MSE↓   0.068	T MAE↓ <b>0.198</b>	SAA MSE%↑ <b>0.000</b>	MAE%↑ <b>0.000</b>			
96	FEDfc MSE 0.068 0.096	ormer-f MAE 0.198 0.238	MSE↓ 0.068 0.096	T MAE↓ 0.198 0.238	SAA MSE%↑ 0.000 0.000	MAE%↑ 0.000 0.000			
96 192 336	FEDfc MSE 0.068 0.096 0.138	ormer-f MAE 0.198 0.238 0.286	MSE↓ 0.068 0.096 0.140	T MAE↓ 0.198 0.238 0.290	SAA MSE%↑ 0.000 0.000 -1.449	MAE%↑ 0.000 0.000 -1.399			
96 H 192 336 720	FEDfc MSE 0.068 0.096	ormer-f MAE 0.198 0.238	MSE↓ 0.068 0.096	T MAE↓ 0.198 0.238	SAA MSE%↑ 0.000 0.000	MAE%↑ 0.000 0.000			
96 H 192 336 720	FEDfo MSE 0.068 0.096 0.138 0.189 0.244	ormer-f           MAE           0.198           0.238           0.286           0.335	MSE↓ 0.068 0.096 0.140 0.190 0.244	T MAE↓ 0.198 0.238 0.290 0.336 0.356	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.000	MAE%↑ 0.000 0.000 -1.399 -0.299 2.198			
96 H 192 336 720	FEDfo MSE 0.096 0.138 0.189 0.244 0.276	ormer-f           MAE           0.198           0.238           0.286           0.335           0.364           0.382	MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277	T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.381	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.000 -0.362	MAE%↑ 0.000 0.000 -1.399 -0.299 2.198 0.262			
96 192 336 720	FEDfc MSE 0.068 0.096 0.138 0.189 0.244 0.276 0.347	ormer-f           MAE           0.198           0.238           0.286           0.335           0.364           0.382           0.432	MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277 0.347	T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.381 0.432	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.000 -0.362 0.000	MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000			
96 192 336 720	FEDfo MSE 0.096 0.138 0.189 0.244 0.276	ormer-f         MAE           0.198         0.238           0.238         0.335           0.364         0.382           0.432         0.473	MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277	T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.381 0.432 0.473	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.000 -0.362	MAE%↑ 0.000 0.000 -1.399 -0.299 2.198 0.262			
96 192 336 720	FEDfc MSE 0.068 0.138 0.189 0.244 0.276 0.347 0.408 0.133	ormer-f         MAE         0.198         0.238         0.286         0.335         0.364         0.382         0.432         0.473         0.284	MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277 0.347 0.408 0.145	T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.381 0.432 0.473 0.293	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.000 -0.362 0.000 0.000 0.000 -9.023	MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169			
96 H 192 336 720	FEDfc MSE 0.096 0.138 0.189 0.244 0.276 0.347 0.408 0.133 0.292	mmer-f           MAE           0.198           0.238           0.335           0.364           0.382           0.432           0.432           0.284           0.419	MSE↓           0.068           0.096           0.140           0.190           0.244           0.277           0.347           0.408           0.145           0.313	T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.381 0.432 0.473 0.293 0.434	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.000 -0.362 0.000 0.000 0.000 0.000 -9.023 -7.192	MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580			
96 H 192 336 720	FEDfc MSE 0.068 0.138 0.189 0.244 0.276 0.347 0.408 0.133 0.292 0.477	mmer-f MAE 0.198 0.238 0.286 0.335 0.364 0.382 0.432 0.432 0.432 0.473 0.284 0.419 0.532	MSE↓           0.068           0.096           0.140           0.190           0.244           0.277           0.347           0.408           0.145           0.313           0.575	T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.381 0.432 0.432 0.473 0.293 0.434 0.595	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000 0.00000 0.0000	MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842			
96         192           192         336           720         720           192         192           192         720           192         720           96         192           720         336           96         192           336         720           336         720	FEDfc MSE 0.068 0.138 0.189 0.244 0.276 0.347 0.408 0.133 0.292 0.477 1.304	mmer-f MAE 0.198 0.238 0.286 0.335 0.364 0.382 0.432 0.432 0.432 0.473 0.284 0.284 0.532 0.882	MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277 0.347 0.347 0.408 0.145 0.313 0.575 2.852	T MAE↓ 0.198 0.238 0.290 0.336 0.336 0.381 0.432 0.473 0.293 0.434 0.595 1.453	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.000 -0.362 0.000 0.000 0.000 0.000 -9.023 -7.192	MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739			
96 192 200 200 200 200 200 200 200 200 200 2	FEDfc MSE 0.068 0.138 0.189 0.244 0.246 0.347 0.408 0.133 0.292 0.477 1.304 0.210	rmer-f MAE 0.198 0.238 0.286 0.335 0.364 0.364 0.432 0.473 0.473 0.284 0.419 0.532 0.482 0.419	MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277 0.347 0.347 0.408 0.145 0.313 0.575 2.852 0.191	T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.356 0.381 0.432 0.473 0.434 0.595 1.453 0.292	SAA MSE%↑ 0.000 -1.449 -0.529 0.000 -0.362 0.000 0.000 0.000 0.000 0.000 -9.023 -7.192 -20.545 -118.712 9.048	MAE%↑ 0.000 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176			
96 192 202 202 202 202 202 202 202 202 202 2	FEDfc MSE 0.068 0.138 0.138 0.244 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.206	nmer-f           MAE           0.198           0.238           0.286           0.335           0.364           0.382           0.473           0.284           0.532           0.582           0.318	MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.197	T MAE↓ 0.198 0.238 0.238 0.336 0.336 0.336 0.381 0.432 0.433 0.434 0.293 0.434 0.553 1.453 1.453	SAA MSE%↑ 0.000 0.000 -1.49 -0.529 0.000 -0.362 0.000 0.000 -0.362 0.000 0.000 -0.362 0.000 0.000 -0.362 -0.129 -0.529 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00	MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215			
P6         192           192         336           720         720           192         720           192         720           192         336           720         336           720         336           720         336           720         720           96         192           192         720           720	FEDfc MSE 0.096 0.138 0.276 0.347 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.206 0.217	mmer-f MAE 0.198 0.238 0.238 0.335 0.335 0.335 0.335 0.432 0.432 0.432 0.432 0.432 0.532 0.882 0.882 0.882 0.318 0.311 0.322	MSE4 0.068 0.096 0.140 0.140 0.244 0.277 0.347 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.197 0.204	T MAE↓ 0.198 0.238 0.290 0.336 0.386 0.381 0.432 0.432 0.433 0.434 0.595 1.453 0.292 0.301 0.309	SAA MSE%↑ 0.000 0.000 -1.449 -0.529 0.000 0.0362 0.000 0.000 0.000 -9.023 -7.192 -20.545 -118.712 18.712 4.369 5.991	MAE%↑ 0.000 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215 4.037			
Jarding         Beckright           192         192           192         192           192         192           192         192           192         192           192         192           96         96           192         192           96         192 <td>FEDfc MSE 0.096 0.138 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.206 0.217 0.243</td> <td>nmer-f           MAE           0.198           0.238           0.286           0.335           0.364           0.382           0.473           0.284           0.532           0.582           0.318</td> <td>MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.197</td> <td>T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.381 0.432 0.432 0.433 0.434 0.595 1.453 0.292 0.301 0.309 0.318</td> <td>SAA MSE%↑ 0.000 -1.449 -0.529 0.000 -0.362 0.000 0.000 -9.023 -7.192 -20.545 -118.712 9.048 4.369 5.991 9.877</td> <td>MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215 4.037 7.018</td>	FEDfc MSE 0.096 0.138 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.206 0.217 0.243	nmer-f           MAE           0.198           0.238           0.286           0.335           0.364           0.382           0.473           0.284           0.532           0.582           0.318	MSE↓ 0.068 0.096 0.140 0.190 0.244 0.277 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.197	T MAE↓ 0.198 0.238 0.290 0.336 0.356 0.381 0.432 0.432 0.433 0.434 0.595 1.453 0.292 0.301 0.309 0.318	SAA MSE%↑ 0.000 -1.449 -0.529 0.000 -0.362 0.000 0.000 -9.023 -7.192 -20.545 -118.712 9.048 4.369 5.991 9.877	MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215 4.037 7.018			
Jarding         Beckright           192         192           192         192           192         192           192         192           192         192           192         192           96         96           192         192           96         192 <td>FEDfc MSE 0.096 0.138 0.276 0.347 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.210 0.217 0.217 0.243</td> <td>mmer-f MAE 0.198 0.238 0.238 0.335 0.335 0.335 0.432 0.432 0.432 0.432 0.432 0.432 0.532 0.882 0.882 0.318 0.318 0.322 0.342</td> <td>MSE4 0.068 0.140 0.190 0.244 0.277 0.347 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.191 0.204 0.219 0.204 0.219</td> <td>T MAE↓ 0.198 0.238 0.290 0.336 0.381 0.432 0.432 0.433 0.434 0.595 1.453 0.292 0.301 0.309 0.309 0.309 0.318</td> <td>SAA MSE%↑ 0.000 -1.449 -0.529 0.000 0.0362 0.000 0.003 0.005 0</td> <td>MAE%↑ 0.000 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215 4.037 7.018 54.795</td>	FEDfc MSE 0.096 0.138 0.276 0.347 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.210 0.217 0.217 0.243	mmer-f MAE 0.198 0.238 0.238 0.335 0.335 0.335 0.432 0.432 0.432 0.432 0.432 0.432 0.532 0.882 0.882 0.318 0.318 0.322 0.342	MSE4 0.068 0.140 0.190 0.244 0.277 0.347 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.191 0.204 0.219 0.204 0.219	T MAE↓ 0.198 0.238 0.290 0.336 0.381 0.432 0.432 0.433 0.434 0.595 1.453 0.292 0.301 0.309 0.309 0.309 0.318	SAA MSE%↑ 0.000 -1.449 -0.529 0.000 0.0362 0.000 0.003 0.005 0	MAE%↑ 0.000 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215 4.037 7.018 54.795			
Jarding         Beckright           192         192           192         192           192         192           192         192           192         192           192         192           96         96           192         192           96         192 <td>FEDfc MSE 0.068 0.138 0.189 0.276 0.347 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.210 0.217 0.243</td> <td>rmer-f MAE 0.198 0.238 0.286 0.335 0.362 0.432 0.432 0.432 0.432 0.473 0.532 0.882 0.318 0.318 0.318 0.318 0.318 0.322 0.342</td> <td>MSE↓ 0.068 0.096 0.140 0.190 0.247 0.347 0.347 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.191 0.204 0.219 0.002 0.002 0.002</td> <td>T MAE↓ 0.198 0.238 0.290 0.336 0.381 0.432 0.432 0.432 0.434 0.595 1.453 0.292 0.301 0.309 0.318 0.333 0.033 0.034</td> <td>SAA MSE%↑ 0.000 -1.449 -0.529 0.000 -0.300 0.000 0.000 0.000 -9.023 -7.192 -20.545 -118.712 9.048 4.369 5.991 9.877 7.778 71.429</td> <td>MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215 4.037 7.018 54.795 49.254</td>	FEDfc MSE 0.068 0.138 0.189 0.276 0.347 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.210 0.217 0.243	rmer-f MAE 0.198 0.238 0.286 0.335 0.362 0.432 0.432 0.432 0.432 0.473 0.532 0.882 0.318 0.318 0.318 0.318 0.318 0.322 0.342	MSE↓ 0.068 0.096 0.140 0.190 0.247 0.347 0.347 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.191 0.204 0.219 0.002 0.002 0.002	T MAE↓ 0.198 0.238 0.290 0.336 0.381 0.432 0.432 0.432 0.434 0.595 1.453 0.292 0.301 0.309 0.318 0.333 0.033 0.034	SAA MSE%↑ 0.000 -1.449 -0.529 0.000 -0.300 0.000 0.000 0.000 -9.023 -7.192 -20.545 -118.712 9.048 4.369 5.991 9.877 7.778 71.429	MAE%↑ 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215 4.037 7.018 54.795 49.254			
96           192           336           720           20           192           192           192           192           192           192           192           336           720           96           96           96           96           96           91           192           192           192           720	FEDfc MSE 0.096 0.138 0.276 0.347 0.276 0.347 0.408 0.133 0.292 0.477 1.304 0.210 0.210 0.217 0.217 0.243	mmer-f MAE 0.198 0.238 0.238 0.335 0.335 0.335 0.432 0.432 0.432 0.432 0.432 0.432 0.532 0.882 0.882 0.318 0.318 0.322 0.342	MSE4 0.068 0.140 0.190 0.244 0.277 0.347 0.347 0.408 0.145 0.313 0.575 2.852 0.191 0.191 0.204 0.219 0.204 0.219	T MAE↓ 0.198 0.238 0.290 0.336 0.381 0.432 0.432 0.433 0.434 0.595 1.453 0.292 0.301 0.309 0.309 0.309 0.318	SAA MSE%↑ 0.000 -1.449 -0.529 0.000 0.0362 0.000 0.003 0.005 0	MAE%↑ 0.000 0.000 -1.399 -0.299 2.198 0.262 0.000 0.000 -3.169 -3.580 -11.842 -64.739 8.176 3.215 4.037 7.018 54.795			

	Table 14: NBEATS-G univariate									
		NBEA	ATS-G		Г	SAA				
		MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$			
2	96	0.080	0.210	0.071	0.192	11.250	8.571			
ETTm2	192	0.110	0.250	0.109	0.246	0.909	1.600			
E	336	0.172	0.320	0.176	0.323	-2.326	-0.938			
⊡	720	0.201	0.353	0.218	0.366	-8.458	-3.683			
ty	96	0.324	0.397	0.263	0.354	18.827	10.831			
Electricity	192	0.363	0.420	0.278	0.368	23.416	12.381			
sct	336	0.392	0.443	0.350	0.422	10.714	4.740			
Ē	720	0.489	0.502	0.378	0.447	22.699	10.956			
ee.	96	0.223	0.351	0.093	0.236	58.296	32.764			
Exchange	192	0.783	0.675	0.215	0.352	72.542	47.852			
ch	336	2.622	1.266	1.167	0.861	55.492	31.991			
Ē	720	2.588	1.303	1.687	1.033	34.815	20.721			
	96	0.159	0.240	0.158	0.239	0.629	0.417			
Traffic	192	0.181	0.264	0.160	0.243	11.602	7.955			
Гra	336	0.155	0.239	0.156	0.244	-0.645	-2.092			
[	720	0.212	0.304	0.189	0.279	10.849	8.224			
H	96	0.003	0.043	0.002	0.031	33.333	27.907			
Weather	192	0.004	0.047	0.002	0.028	50.000	40.426			
ea	336	0.005	0.054	0.004	0.037	20.000	31.481			
2	720	0.004	0.048	0.002	0.036	50.000	25.000			

		lable 11: Autoformer univariate							
		Autofe	ormer		Г	SAA			
		MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$		
2	96	0.123	0.270	0.106	0.250	13.821	7.407		
$ETTm_2$	192	0.141	0.289	0.126	0.273	10.638	5.536		
E	336	0.170	0.319	0.139	0.290	18.235	9.091		
되	720	0.206	0.353	0.187	0.338	9.223	4.249		
ty	96	0.454	0.508	0.388	0.456	14.537	10.236		
Electricity	192	0.511	0.532	0.463	0.509	9.393	4.323		
seti	336	0.739	0.651	0.493	0.517	33.288	20.584		
Еľ	720	0.673	0.610	0.532	0.549	20.951	10.000		
ge	96	0.149	0.308	0.146	0.295	2.013	4.221		
anj	192	0.290	0.415	0.298	0.416	-2.759	-0.241		
Exchange	336	0.708	0.662	0.712	0.643	-0.565	2.870		
Ē	720	1.324	0.892	2.703	1.390	-104.154	-55.830		
	96	0.266	0.372	0.248	0.351	6.767	5.645		
Traffic	192	0.272	0.379	0.249	0.353	8.456	6.860		
Dra	336	0.261	0.374	0.239	0.347	8.429	7.219		
ι.	720	0.269	0.372	0.237	0.343	11.896	7.796		
н	96	0.009	0.078	0.003	0.039	66.667	50.000		
the	192	0.009	0.068	0.003	0.040	66.667	41.176		
Weather	336	0.006	0.058	0.004	0.046	33.333	20.690		
М	720	0.007	0.063	0.004	0.046	42.857	26.984		

	,	Table 1	13: NI	BEAT	S-I un	ivariate	:
		NBEA	ATS-I		Т	SAA	
		MSE	MAE	$MSE\downarrow$	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$
5	96	0.080	0.213	0.075	0.202	6.250	5.164
д	192	0.103	0.240	0.102	0.237	0.971	1.250
$ETTm_2$	336	0.162	0.312	0.171	0.321	-5.556	-2.885
E	720	0.199	0.347	0.231	0.376	-16.080	-8.357
ty	96	0.326	0.402	0.270	0.360	17.178	10.448
Electricity	192	0.350	0.417	0.277	0.368	20.857	11.751
čti	336	0.393	0.440	0.310	0.394	21.120	10.455
ΕĬ	720	0.458	0.490	0.394	0.453	13.974	7.551
e	96	0.210	0.344	0.093	0.238	55.714	30.814
an	192	1.130	0.840	0.215	0.352	80.973	58.095
Exchange	336	1.587	1.047	0.532	0.572	66.478	45.368
Ê	720	0.870	0.747	0.744	0.665	14.483	10.977
	96	0.181	0.268	0.183	0.270	-1.105	-0.746
Ĕ	192	0.177	0.263	0.176	0.263	0.565	0.000
Traffic	336	0.180	0.271	0.180	0.270	0.000	0.369
C	720	0.226	0.316	0.224	0.311	0.885	1.582
H	96	0.003	0.044	0.001	0.024	66.667	45.455
the	192	0.004	0.046	0.001	0.027	75.000	41.304
Weather	336	0.004	0.048	0.004	0.035	0.000	27.083
Μ	720	0.004	0.049	0.002	0.034	50.000	30.612

Table 11: Autoformer univariate

# E.2 Main results with standard deviation

The following tables Tabs. 15, 16 augment the tables presented in Sec. 5 in the main text with standard deviation measures computed over three different seed numbers.

Table 15: Multivariate long-term time-series forecasting results with the standard deviation.

			0	Autoformer		FEDformer-w		1	C
		Info MSE	rmer MAE	Autor MSE	ormer MAE	MSE FEDIo	rmer-w MAE	MSE FEDIC	ormer-f MAE
				I		I		I	
12	96	$0.545 \pm 0.024$	$0.588 \pm 0.014$	$0.231 \pm 0.004$	$0.31 \pm 0.0$	$0.205 \pm 0.001$	$0.29 \pm 0.0$	$0.189 \pm 0.001$	$0.282 \pm 0.001$
ETTm2	192	$1.054 \pm 0.044$	$0.808 \pm 0.018$	$0.289 \pm 0.013$	$0.346 \pm 0.01$	$0.27 \pm 0.0$	$0.329 \pm 0.0$	$0.258 \pm 0.002$	$0.326 \pm 0.001$
EI	$336 \\ 720$	$\begin{array}{c} 1.523 \pm 0.036 \\ 3.878 \pm 0.072 \end{array}$	$\begin{array}{c} 0.948 \pm 0.014 \\ 1.474 \pm 0.004 \end{array}$	$\begin{array}{c} 0.341 \pm 0.008 \\ 0.444 \pm 0.005 \end{array}$	$\begin{array}{c} 0.375 \pm 0.004 \\ 0.434 \pm 0.005 \end{array}$	$\begin{array}{c} 0.328 \pm 0.0 \\ 0.433 \pm 0.005 \end{array}$	$\begin{array}{c} 0.364 \pm 0.0 \\ 0.425 \pm 0.005 \end{array}$	$\begin{array}{c} 0.323 \pm 0.004 \\ 0.425 \pm 0.008 \end{array}$	$\begin{array}{c} 0.363 \pm 0.004 \\ 0.421 \pm 0.001 \end{array}$
city	96	$0.336 \pm 0.013$	$0.416 \pm 0.007$	$0.2 \pm 0.007$	$0.316 \pm 0.007$	$0.196 \pm 0.002$	$0.31 \pm 0.002$	$0.185 \pm 0.001$	$0.3 \pm 0.001$
tri	$192 \\ 336$	$0.36 \pm 0.015$ 0.256 ± 0.007	$\begin{array}{c} 0.441 \pm 0.012 \\ 0.439 \pm 0.006 \end{array}$	$0.217 \pm 0.0$	$0.326 \pm 0.002$ 0.256 ± 0.012	$0.199 \pm 0.001$ $0.217 \pm 0.001$	$\begin{array}{c} 0.31 \pm 0.002 \\ 0.334 \pm 0.001 \end{array}$	$\begin{array}{c} 0.201 \pm 0.007 \\ 0.214 \pm 0.002 \end{array}$	$\begin{array}{c} 0.316 \pm 0.008 \\ 0.329 \pm 0.002 \end{array}$
Electricity	720	$\begin{array}{c} 0.356 \pm 0.007 \\ 0.386 \pm 0.012 \end{array}$	$0.439 \pm 0.000$ $0.452 \pm 0.01$	$\begin{array}{c} 0.258 \pm 0.024 \\ 0.261 \pm 0.002 \end{array}$	$\begin{array}{c} 0.356 \pm 0.013 \\ 0.363 \pm 0.004 \end{array}$	$\begin{array}{c} 0.217 \pm 0.001 \\ 0.248 \pm 0.004 \end{array}$	$0.354 \pm 0.001$ $0.357 \pm 0.004$	$0.214 \pm 0.002$ $0.246 \pm 0.002$	$\begin{array}{c} 0.329 \pm 0.002 \\ 0.353 \pm 0.0 \end{array}$
								1	'
1ge	96	$1.029 \pm 0.038$	$0.809 \pm 0.02$	$0.15 \pm 0.005$	$0.281 \pm 0.005$	$0.151 \pm 0.004$	$0.282 \pm 0.004$	$0.142 \pm 0.004$	$0.271 \pm 0.004$
thai	$     \begin{array}{c}       192 \\       336     \end{array} $	$\begin{array}{c} 1.155 \pm 0.038 \\ 1.589 \pm 0.048 \end{array}$	$\begin{array}{c} 0.867 \pm 0.015 \\ 1.011 \pm 0.011 \end{array}$	$\begin{array}{c} 0.318 \pm 0.012 \\ 0.713 \pm 0.516 \end{array}$	$\begin{array}{c} 0.409 \pm 0.008 \\ 0.616 \pm 0.243 \end{array}$	$\begin{array}{c} 0.284 \pm 0.003 \\ 0.442 \pm 0.003 \end{array}$	$\begin{array}{c} 0.391 \pm 0.002 \\ 0.493 \pm 0.001 \end{array}$	$\begin{array}{c} 0.278 \pm 0.003 \\ 0.45 \pm 0.003 \end{array}$	$\begin{array}{c} 0.383 \pm 0.001 \\ 0.497 \pm 0.001 \end{array}$
Exchange	720	$3.011 \pm 0.302$	$1.431 \pm 0.067$	$1.246 \pm 0.007$	$0.010 \pm 0.243$ $0.872 \pm 0.002$	$0.442 \pm 0.003$ $1.227 \pm 0.024$	$0.493 \pm 0.001$ $0.868 \pm 0.011$	$1.181 \pm 0.018$	$0.497 \pm 0.001$ $0.841 \pm 0.002$
_									
ic.	96 102	$0.744 \pm 0.006$	$0.42 \pm 0.006$	$0.615 \pm 0.015$	$0.384 \pm 0.009$	$0.584 \pm 0.005$	$0.368 \pm 0.005$	$0.577 \pm 0.001$	$0.361 \pm 0.002$
Traffic	$\frac{192}{336}$	$\begin{array}{c} 0.753 \pm 0.01 \\ 0.876 \pm 0.024 \end{array}$	$\begin{array}{c} 0.426 \pm 0.011 \\ 0.495 \pm 0.013 \end{array}$	$\begin{array}{c} 0.67 \pm 0.068 \\ 0.635 \pm 0.027 \end{array}$	$\begin{array}{c} 0.421 \pm 0.045 \\ 0.392 \pm 0.014 \end{array}$	$\begin{array}{c} 0.594 \pm 0.007 \\ 0.59 \pm 0.001 \end{array}$	$\begin{array}{c} 0.372 \pm 0.007 \\ 0.365 \pm 0.002 \end{array}$	$\begin{array}{c} 0.61 \pm 0.003 \\ 0.623 \pm 0.005 \end{array}$	$\begin{array}{c} 0.379 \pm 0.004 \\ 0.385 \pm 0.004 \end{array}$
f	720	$1.011 \pm 0.032$	$0.435 \pm 0.013$ $0.578 \pm 0.018$	$0.035 \pm 0.027$ $0.658 \pm 0.011$	$0.392 \pm 0.014$ $0.402 \pm 0.01$	$0.53 \pm 0.001$ $0.613 \pm 0.006$	$0.305 \pm 0.002$ $0.375 \pm 0.003$	$0.632 \pm 0.005$ $0.632 \pm 0.006$	$0.388 \pm 0.004$ $0.388 \pm 0.007$
				1					
ler	96 102	$0.315 \pm 0.004$ 0.428 ± 0.005	$0.382 \pm 0.004$ 0.440 ± 0.012	$0.259 \pm 0.014$ $0.208 \pm 0.012$	$0.332 \pm 0.011$ 0.256 ± 0.012	$0.269 \pm 0.011$ $0.257 \pm 0.001$	$0.347 \pm 0.008$ 0.412 ± 0.002	$0.236 \pm 0.024$ $0.272 \pm 0.012$	$0.316 \pm 0.028$ 0.222 $\pm 0.012$
Weather	$\frac{192}{336}$	$\begin{array}{c} 0.428 \pm 0.005 \\ 0.62 \pm 0.027 \end{array}$	$\begin{array}{c} 0.449 \pm 0.012 \\ 0.554 \pm 0.009 \end{array}$	$\begin{array}{c} 0.298 \pm 0.012 \\ 0.357 \pm 0.01 \end{array}$	$0.356 \pm 0.012$ 0.304 ± 0.011	$\begin{array}{c} 0.357 \pm 0.001 \\ 0.422 \pm 0.008 \end{array}$	$\begin{array}{c} 0.412 \pm 0.002 \\ 0.456 \pm 0.006 \end{array}$	$\begin{array}{c} 0.273 \pm 0.013 \\ 0.332 \pm 0.016 \end{array}$	$0.333 \pm 0.012$ 0.371 ± 0.016
We	720	$0.02 \pm 0.027$ $0.975 \pm 0.035$	$0.334 \pm 0.009$ $0.722 \pm 0.009$	$0.337 \pm 0.01$ $0.422 \pm 0.011$	$\begin{array}{c} 0.394 \pm 0.011 \\ 0.431 \pm 0.01 \end{array}$	$0.422 \pm 0.008$ $0.629 \pm 0.008$	$0.430 \pm 0.000$ $0.57 \pm 0.004$	$0.332 \pm 0.010$ $0.408 \pm 0.009$	$\begin{array}{c} 0.371 \pm 0.016 \\ 0.418 \pm 0.008 \end{array}$
	24	$5.349 \pm 0.229$	$1.582 \pm 0.052$	$3.549 \pm 0.33$	$1.305 \pm 0.068$	$2.752 \pm 0.023$	$1.125 \pm 0.005$	$3.268 \pm 0.04$	$1.257 \pm 0.014$
ILLI	36	$5.203 \pm 0.129$ $5.286 \pm 0.049$	$\begin{array}{c} 1.572 \pm 0.029 \\ 1.594 \pm 0.018 \end{array}$	$2.834 \pm 0.166$	$1.094 \pm 0.032$	$2.318 \pm 0.017$	$0.98 \pm 0.006$	$2.648 \pm 0.034$	$1.068 \pm 0.009$ 1.072 + 0.004
_	$48 \\ 60$	$5.280 \pm 0.049$ $5.419 \pm 0.103$	$1.594 \pm 0.018$ $1.62 \pm 0.019$	$\begin{array}{c} 2.889 \pm 0.178 \\ 2.818 \pm 0.157 \end{array}$	$\begin{array}{c} 1.122 \pm 0.033 \\ 1.118 \pm 0.039 \end{array}$	$\begin{array}{c} 2.328 \pm 0.043 \\ 2.574 \pm 0.052 \end{array}$	$\begin{array}{c} 1.006 \pm 0.013 \\ 1.081 \pm 0.016 \end{array}$	$\begin{array}{c} 2.615 \pm 0.019 \\ 2.866 \pm 0.031 \end{array}$	$\frac{1.072 \pm 0.004}{1.158 \pm 0.008}$
									1.100 ± 0.000
						I		I	
		TS	AA			1		1	I
						I		I	'
[2	96	TS	AA			1		1	'
Tm2	192	$\begin{array}{c} \text{TS} \\ \text{MSE} \\ \hline 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \end{array}$	$\begin{array}{c} \text{AA} & \\ \text{MAE} \\ \hline 0.274 \pm 0.000 \\ 0.314 \pm 0.001 \end{array}$			I		I	'
ETTm2	$\begin{array}{c} 192\\ 336 \end{array}$	$\begin{array}{c} & \text{TS}.\\ \text{MSE} \\ \hline 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \end{array}$	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$			I		I	'
ETTm2	192	$\begin{array}{c} \text{TS} \\ \text{MSE} \\ \hline 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \end{array}$	$\begin{array}{c} \text{AA} & \\ \text{MAE} \\ \hline 0.274 \pm 0.000 \\ 0.314 \pm 0.001 \end{array}$			I		I	
	192 336 720 96	$\begin{array}{c} & \text{TS}.\\ \text{MSE} \\ \hline 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \end{array}$	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$			I		I	
	192 336 720 96 192	$\begin{array}{c} & \text{TS} \\ \text{MSE} \\ \hline 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline 0.183 \pm 0.001 \\ 0.195 \pm 0.001 \end{array}$	$\begin{tabular}{ c c c c c c c } \hline AA & & & & & & & & & & & & & & & & & $			I		I	
	192 336 720 96 192 336	$\begin{array}{c} & \text{TS} \\ \text{MSE} \\ \hline 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline 0.183 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.208 \pm 0.002 \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ \hline 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ \hline \end{tabular}$			I		I	
Electricity ETTm2	192 336 720 96 192	$\begin{array}{c} & \text{TS} \\ \text{MSE} \\ \hline 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline 0.183 \pm 0.001 \\ 0.195 \pm 0.001 \end{array}$	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$			I		I	
Electricity	192 336 720 96 192 336	$\begin{array}{c} & \text{TS} \\ \text{MSE} \\ \hline 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline 0.183 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.208 \pm 0.002 \end{array}$	$\begin{tabular}{ c c c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ \hline 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ \hline \end{tabular}$			I		I	
Electricity	192 336 720 96 192 336 720 96 192	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline 0.183 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \end{array}$	$\begin{tabular}{ c c c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ \hline 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ \hline \end{tabular}$			I		I	
Electricity	192 336 720 96 192 336 720 96 192 336	$\begin{array}{c} & \text{TS} \\ \text{MSE} \\ \hline \\ 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline \\ 0.183 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.208 \pm 0.002 \\ 0.238 \pm 0.003 \\ \hline \\ 0.143 \pm 0.012 \\ 0.27 \pm 0.002 \\ 0.459 \pm 0.007 \\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE \\ \hline 0.274 \pm 0.000 \\ 0.314 \pm 0.001 \\ 0.350 \pm 0.002 \\ 0.403 \pm 0.002 \\ 0.297 \pm 0.001 \\ 0.309 \pm 0.002 \\ 0.323 \pm 0.002 \\ 0.348 \pm 0.003 \\ \hline 0.272 \pm 0.012 \\ 0.378 \pm 0.002 \\ 0.504 \pm 0.007 \\ \hline \end{tabular}$			I		I	
	192 336 720 96 192 336 720 96 192	$\begin{array}{c} & \text{TS} \\ \text{MSE} \\ \hline \\ 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline \\ 0.183 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.208 \pm 0.002 \\ 0.238 \pm 0.003 \\ \hline \\ 0.143 \pm 0.012 \\ 0.27 \pm 0.002 \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ \hline \end{tabular}$			I		I	
Exchange Electricity	192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline \\ 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline \\ 0.183 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \\ 0.143 \pm 0.012\\ 0.27 \pm 0.002\\ 0.459 \pm 0.007\\ 1.213 \pm 0.056\\ \hline \\ 0.565 \pm 0.005\\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ \hline 0.352 \pm 0.004 & \\ \hline \end{tabular}$			1		1	
Exchange Electricity	192 336 720 96 192 336 720 96 192 336 720	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline \\ 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline \\ 0.183 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \\ 0.143 \pm 0.012\\ 0.27 \pm 0.002\\ 0.459 \pm 0.007\\ 1.213 \pm 0.056\\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ \hline 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ \hline 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ \hline \end{tabular}$			1		1	
Exchange Electricity	192 336 720 96 192 336 720 96 192 336 720 96 192 336	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline \\ 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline \\ 0.183 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \\ 0.143 \pm 0.012\\ 0.27 \pm 0.002\\ 0.459 \pm 0.007\\ 1.213 \pm 0.056\\ \hline \\ 0.565 \pm 0.005\\ 0.572 \pm 0.002\\ 0.584 \pm 0.004\\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ 0.352 \pm 0.004 & \\ 0.351 \pm 0.001 & \\ 0.359 \pm 0.005 & \\ \hline \end{tabular}$			1		1	
Electricity	192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline \\ 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline \\ 0.195 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \\ 0.143 \pm 0.012\\ 0.27 \pm 0.002\\ 0.459 \pm 0.007\\ 1.213 \pm 0.056\\ \hline \\ 0.565 \pm 0.005\\ 0.572 \pm 0.002\\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ 0.352 \pm 0.004 & \\ 0.351 \pm 0.001 & \\ \hline \end{tabular}$			1		1	
Traffic Exchange Electricity	192 336 720 96 192 336 720 96 192 336 720 96 192 336	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline \\ 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline \\ 0.195 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \\ 0.143 \pm 0.012\\ 0.27 \pm 0.002\\ 0.459 \pm 0.007\\ 1.213 \pm 0.056\\ \hline \\ 0.565 \pm 0.005\\ 0.572 \pm 0.002\\ 0.584 \pm 0.004\\ 0.607 \pm 0.002\\ \hline \\ 0.18 \pm 0.024\\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ 0.352 \pm 0.004 & \\ 0.351 \pm 0.001 & \\ 0.359 \pm 0.005 & \\ 0.368 \pm 0.002 & \\ 0.256 \pm 0.024 & \\ \hline \end{tabular}$			1		1	
Traffic Exchange Electricity	$\begin{array}{c} 192\\ 336\\ 720\\ \\ 96\\ 192\\ 336\\ 720\\ \\ 96\\ 192\\ 336\\ 720\\ \\ 96\\ 192\\ 336\\ 720\\ \\ 96\\ 192\\ \\ 336\\ 720\\ \\ 96\\ 192\\ \\ 96\\ 192\\ \end{array}$	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline \\ 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline \\ 0.195 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \\ 0.143 \pm 0.012\\ 0.27 \pm 0.002\\ 0.459 \pm 0.007\\ 1.213 \pm 0.056\\ \hline \\ 0.565 \pm 0.005\\ 0.572 \pm 0.002\\ 0.584 \pm 0.004\\ 0.607 \pm 0.002\\ \hline \\ 0.18 \pm 0.024\\ 0.252 \pm 0.001\\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ 0.352 \pm 0.004 & \\ 0.351 \pm 0.001 & \\ 0.359 \pm 0.005 & \\ 0.368 \pm 0.002 & \\ 0.256 \pm 0.024 & \\ 0.311 \pm 0.002 & \\ \hline \end{tabular}$			1		1	
Traffic Exchange Electricity	192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline \\ 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline \\ 0.195 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \\ 0.143 \pm 0.012\\ 0.27 \pm 0.002\\ 0.459 \pm 0.007\\ 1.213 \pm 0.056\\ \hline \\ 0.565 \pm 0.005\\ 0.572 \pm 0.002\\ 0.584 \pm 0.004\\ 0.607 \pm 0.002\\ \hline \\ 0.18 \pm 0.024\\ 0.252 \pm 0.001\\ 0.296 \pm 0.001\\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ 0.352 \pm 0.004 & \\ 0.351 \pm 0.001 & \\ 0.359 \pm 0.005 & \\ 0.368 \pm 0.002 & \\ 0.256 \pm 0.024 & \\ 0.311 \pm 0.002 & \\ 0.355 \pm 0.005 & \\ \hline \end{tabular}$			1		1	
Exchange Electricity	$\begin{array}{c} 192\\ 336\\ 720\\ \\ 96\\ 192\\ 336\\ 720\\ \\ 96\\ 192\\ 336\\ 720\\ \\ 96\\ 192\\ 336\\ 720\\ \\ 96\\ 192\\ \\ 336\\ 720\\ \\ 96\\ 192\\ \\ 96\\ 192\\ \end{array}$	$\begin{array}{c} \text{TS}\\ \text{MSE}\\ \hline \\ 0.187 \pm 0.000\\ 0.255 \pm 0.001\\ 0.304 \pm 0.009\\ 0.398 \pm 0.007\\ \hline \\ 0.195 \pm 0.001\\ 0.195 \pm 0.001\\ 0.208 \pm 0.002\\ 0.238 \pm 0.002\\ 0.238 \pm 0.003\\ \hline \\ 0.143 \pm 0.012\\ 0.27 \pm 0.002\\ 0.459 \pm 0.007\\ 1.213 \pm 0.056\\ \hline \\ 0.565 \pm 0.005\\ 0.572 \pm 0.002\\ 0.584 \pm 0.004\\ 0.607 \pm 0.002\\ \hline \\ 0.18 \pm 0.024\\ 0.252 \pm 0.001\\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ 0.352 \pm 0.004 & \\ 0.351 \pm 0.001 & \\ 0.359 \pm 0.005 & \\ 0.368 \pm 0.002 & \\ 0.256 \pm 0.024 & \\ 0.311 \pm 0.002 & \\ \hline \end{tabular}$			1		1	
Traffic Exchange Electricity	192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720           96           192           336           720	$\begin{array}{c} {\rm TS} \\ {\rm MSE} \\ \hline \\ 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline \\ 0.183 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.208 \pm 0.002 \\ 0.238 \pm 0.002 \\ 0.238 \pm 0.003 \\ \hline \\ 0.143 \pm 0.012 \\ 0.27 \pm 0.002 \\ 0.459 \pm 0.007 \\ 1.213 \pm 0.056 \\ \hline \\ 0.565 \pm 0.005 \\ 0.572 \pm 0.002 \\ 0.584 \pm 0.004 \\ 0.607 \pm 0.002 \\ \hline \\ 0.18 \pm 0.024 \\ 0.252 \pm 0.001 \\ 0.296 \pm 0.001 \\ 0.382 \pm 0.006 \\ \hline \\ 2.76 \pm 0.063 \\ \hline \end{array}$	$\begin{tabular}{ c c c c c } \hline AA & MAE & \\ \hline 0.274 \pm 0.000 & \\ 0.314 \pm 0.001 & \\ 0.350 \pm 0.002 & \\ 0.403 \pm 0.002 & \\ 0.297 \pm 0.001 & \\ 0.309 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.323 \pm 0.002 & \\ 0.348 \pm 0.003 & \\ 0.272 \pm 0.012 & \\ 0.378 \pm 0.002 & \\ 0.504 \pm 0.007 & \\ 0.842 \pm 0.008 & \\ 0.352 \pm 0.004 & \\ 0.351 \pm 0.001 & \\ 0.359 \pm 0.005 & \\ 0.368 \pm 0.002 & \\ 0.256 \pm 0.024 & \\ 0.311 \pm 0.002 & \\ 0.355 \pm 0.005 & \\ \hline \end{tabular}$			1		1	
Weather Traffic Exchange Electricity	192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         92         336         720         93         94         336         720         92         336         720         92         336         720         936         192         336         720         936         192         336         720         936         192         336         720         24         36     <	$\begin{array}{c} {\rm TS} \\ {\rm MSE} \\ \hline \\ 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline \\ 0.195 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.208 \pm 0.002 \\ 0.238 \pm 0.002 \\ 0.238 \pm 0.003 \\ \hline \\ 0.143 \pm 0.012 \\ 0.27 \pm 0.002 \\ 0.459 \pm 0.007 \\ 1.213 \pm 0.056 \\ \hline \\ 0.565 \pm 0.005 \\ 0.572 \pm 0.002 \\ 0.584 \pm 0.004 \\ 0.607 \pm 0.002 \\ \hline \\ 0.18 \pm 0.024 \\ 0.252 \pm 0.001 \\ 0.296 \pm 0.001 \\ 0.382 \pm 0.006 \\ \hline \\ 2.76 \pm 0.063 \\ 2.362 \pm 0.024 \\ \hline \end{array}$	$\begin{array}{c} AA \\ MAE \\ \hline \\ 0.274 \pm 0.000 \\ 0.314 \pm 0.001 \\ 0.350 \pm 0.002 \\ 0.403 \pm 0.002 \\ 0.403 \pm 0.002 \\ 0.297 \pm 0.001 \\ 0.309 \pm 0.002 \\ 0.323 \pm 0.002 \\ 0.323 \pm 0.002 \\ 0.348 \pm 0.003 \\ 0.272 \pm 0.012 \\ 0.378 \pm 0.002 \\ 0.504 \pm 0.007 \\ 0.842 \pm 0.008 \\ 0.352 \pm 0.004 \\ 0.351 \pm 0.001 \\ 0.359 \pm 0.005 \\ 0.368 \pm 0.002 \\ 0.256 \pm 0.024 \\ 0.311 \pm 0.002 \\ 0.355 \pm 0.005 \\ 0.395 \pm 0.005 \\ 0.395 \pm 0.007 \\ 1.123 \pm 0.016 \\ 0.984 \pm 0.008 \\ \end{array}$			1		1	
Traffic Exchange Electricity	192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         94         36         720         93         94         192         336         720         94         192         336         720         94         192         336         720         936         192         336         720         94         36         48	$\begin{array}{c} {\rm TS} \\ {\rm MSE} \\ \hline \\ 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline \\ 0.183 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.208 \pm 0.002 \\ 0.238 \pm 0.002 \\ 0.238 \pm 0.003 \\ \hline \\ 0.143 \pm 0.012 \\ 0.27 \pm 0.002 \\ 0.459 \pm 0.007 \\ 1.213 \pm 0.056 \\ \hline \\ 0.565 \pm 0.005 \\ 0.572 \pm 0.002 \\ 0.584 \pm 0.004 \\ 0.607 \pm 0.002 \\ \hline \\ 0.584 \pm 0.004 \\ 0.607 \pm 0.002 \\ \hline \\ 0.18 \pm 0.024 \\ 0.252 \pm 0.001 \\ 0.382 \pm 0.006 \\ \hline \\ 2.76 \pm 0.063 \\ 2.362 \pm 0.024 \\ 2.264 \pm 0.074 \\ \hline \end{array}$	$\begin{array}{c} AA \\ MAE \\ \hline \\ 0.274 \pm 0.000 \\ 0.314 \pm 0.001 \\ 0.350 \pm 0.002 \\ 0.403 \pm 0.002 \\ 0.403 \pm 0.002 \\ 0.297 \pm 0.001 \\ 0.309 \pm 0.002 \\ 0.323 \pm 0.002 \\ 0.323 \pm 0.002 \\ 0.348 \pm 0.003 \\ 0.272 \pm 0.012 \\ 0.378 \pm 0.002 \\ 0.504 \pm 0.007 \\ 0.842 \pm 0.008 \\ 0.352 \pm 0.004 \\ 0.351 \pm 0.001 \\ 0.359 \pm 0.005 \\ 0.368 \pm 0.002 \\ 0.256 \pm 0.024 \\ 0.311 \pm 0.002 \\ 0.355 \pm 0.005 \\ 0.395 \pm 0.005 \\ 0.395 \pm 0.007 \\ 1.123 \pm 0.016 \\ 0.984 \pm 0.008 \\ 0.988 \pm 0.012 \\ \end{array}$			1		1	
Weather Traffic Exchange Electricity	192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         96         192         336         720         92         336         720         93         94         336         720         92         336         720         92         336         720         936         192         336         720         936         192         336         720         936         192         336         720         24         36     <	$\begin{array}{c} {\rm TS} \\ {\rm MSE} \\ \hline \\ 0.187 \pm 0.000 \\ 0.255 \pm 0.001 \\ 0.304 \pm 0.009 \\ 0.398 \pm 0.007 \\ \hline \\ 0.195 \pm 0.001 \\ 0.195 \pm 0.001 \\ 0.208 \pm 0.002 \\ 0.238 \pm 0.002 \\ 0.238 \pm 0.003 \\ \hline \\ 0.143 \pm 0.012 \\ 0.27 \pm 0.002 \\ 0.459 \pm 0.007 \\ 1.213 \pm 0.056 \\ \hline \\ 0.565 \pm 0.005 \\ 0.572 \pm 0.002 \\ 0.584 \pm 0.004 \\ 0.607 \pm 0.002 \\ \hline \\ 0.18 \pm 0.024 \\ 0.252 \pm 0.001 \\ 0.296 \pm 0.001 \\ 0.382 \pm 0.006 \\ \hline \\ 2.76 \pm 0.063 \\ 2.362 \pm 0.024 \\ \hline \end{array}$	$\begin{array}{c} AA \\ MAE \\ \hline \\ 0.274 \pm 0.000 \\ 0.314 \pm 0.001 \\ 0.350 \pm 0.002 \\ 0.403 \pm 0.002 \\ 0.403 \pm 0.002 \\ 0.297 \pm 0.001 \\ 0.309 \pm 0.002 \\ 0.323 \pm 0.002 \\ 0.323 \pm 0.002 \\ 0.348 \pm 0.003 \\ 0.272 \pm 0.012 \\ 0.378 \pm 0.002 \\ 0.504 \pm 0.007 \\ 0.842 \pm 0.008 \\ 0.352 \pm 0.004 \\ 0.351 \pm 0.001 \\ 0.359 \pm 0.005 \\ 0.368 \pm 0.002 \\ 0.256 \pm 0.024 \\ 0.311 \pm 0.002 \\ 0.355 \pm 0.005 \\ 0.395 \pm 0.005 \\ 0.395 \pm 0.007 \\ 1.123 \pm 0.016 \\ 0.984 \pm 0.008 \\ \end{array}$			1		1	

Table 16: Univariate long-term time-series forecasting results with the standard dev									
		Info	rmer	Autof	ormer	FEDfo	ormer-f	N-BE	ATS-I
		MSE	MAE	MSE	MAE	MSE	MAE	MSE	MAE
~	96	$0.085 \pm 0.004$	$0.225 \pm 0.006$	$0.123 \pm 0.017$	$0.27 \pm 0.018$	$0.068 \pm 0.001$	$0.198 \pm 0.002$	$0.08 \pm 0.003$	$0.213 \pm 0.006$
E.	192	$0.13 \pm 0.007$	$0.282 \pm 0.008$	$0.141 \pm 0.01$	$0.289 \pm 0.01$	$0.096 \pm 0.001$	$0.238 \pm 0.001$	$0.103 \pm 0.004$	$0.24 \pm 0.006$
ETTm2	336	$0.161 \pm 0.008$	$0.314 \pm 0.006$	$0.17 \pm 0.046$	$0.319\pm0.042$	$0.138 \pm 0.013$	$0.286\pm0.014$	$0.162 \pm 0.009$	$0.312 \pm 0.009$
머	720	$0.221 \pm 0.006$	$0.373\pm0.007$	$0.206 \pm 0.02$	$0.353\pm0.017$	$0.189 \pm 0.002$	$0.335\pm0.002$	$0.199 \pm 0.007$	$0.347 \pm 0.007$
Ń	96	$0.261 \pm 0.005$	$0.367 \pm 0.002$	$0.454 \pm 0.014$	$0.508 \pm 0.014$	$0.244 \pm 0.001$	$0.364 \pm 0.002$	$0.326 \pm 0.006$	$0.402 \pm 0.004$
icit	192	$0.285 \pm 0.006$	$0.386 \pm 0.003$	$0.511 \pm 0.05$	$0.532 \pm 0.027$	$0.276 \pm 0.004$	$0.382 \pm 0.004$	$0.35 \pm 0.008$	$0.417 \pm 0.005$
ctr	336	$0.324 \pm 0.004$	$0.417 \pm 0.004$	$0.739 \pm 0.086$	$0.651 \pm 0.042$	$0.347 \pm 0.007$	$0.432 \pm 0.006$	$0.393 \pm 0.008$	$0.44 \pm 0.003$
Electricity	720	$0.632 \pm 0.049$	$0.612\pm0.028$	$0.673 \pm 0.082$	$0.61\pm0.037$	$0.408 \pm 0.025$	$0.473 \pm 0.015$	$0.458 \pm 0.008$	$0.49\pm0.002$
e	96	$0.49 \pm 0.065$	$0.554 \pm 0.034$	$0.149 \pm 0.004$	$0.308 \pm 0.006$	$0.133 \pm 0.015$	$0.284 \pm 0.018$	$0.21 \pm 0.047$	$0.344 \pm 0.036$
Exchange	192	$0.79 \pm 0.039$	$0.721 \pm 0.016$	$0.29 \pm 0.005$	$0.415 \pm 0.004$	$0.292 \pm 0.002$	$0.419\pm0.003$	$1.13 \pm 0.392$	$0.84 \pm 0.153$
chi	336	$2.146 \pm 0.25$	$1.223 \pm 0.084$	$0.708 \pm 0.108$	$0.662 \pm 0.053$	$0.477 \pm 0.002$	$0.532 \pm 0.002$	$1.587 \pm 0.219$	$1.047 \pm 0.077$
Ē	720	$1.447 \pm 0.105$	$1.008\pm0.038$	$1.324 \pm 0.005$	$0.892\pm0.002$	$1.304 \pm 0.003$	$0.882\pm0.0$	$0.87 \pm 0.088$	$0.747 \pm 0.015$
	96	$0.262 \pm 0.006$	$0.348 \pm 0.006$	$0.266 \pm 0.005$	$0.372 \pm 0.01$	$0.21 \pm 0.006$	$0.318 \pm 0.009$	$0.181 \pm 0.004$	$0.268 \pm 0.005$
Traffic	192	$0.294 \pm 0.004$	$0.376 \pm 0.006$	$0.272 \pm 0.014$	$0.379 \pm 0.01$	$0.206 \pm 0.01$	$0.311 \pm 0.006$	$0.177 \pm 0.001$	$0.263 \pm 0.001$
Tad	336	$0.308 \pm 0.007$	$0.39 \pm 0.002$	$0.261 \pm 0.016$	$0.374 \pm 0.016$	$0.217 \pm 0.005$	$0.322\pm0.0$	$0.18 \pm 0.005$	$0.271 \pm 0.006$
Г	720	$0.364 \pm 0.018$	$0.44\pm0.017$	$0.269 \pm 0.012$	$0.372\pm0.005$	$0.243 \pm 0.021$	$0.342\pm0.021$	$0.226 \pm 0.003$	$0.316 \pm 0.004$
	96	$0.005 \pm 0.001$	$0.048 \pm 0.005$	$0.009 \pm 0.002$	$0.078 \pm 0.009$	$0.009 \pm 0.004$	$0.073 \pm 0.014$	$0.003 \pm 0.001$	$0.044 \pm 0.006$
Weather	192	$0.004 \pm 0.0$	$0.051 \pm 0.001$	$0.009 \pm 0.002$	$0.068 \pm 0.001$	$0.007 \pm 0.002$	$0.067\pm0.008$	$0.004 \pm 0.0$	$0.046 \pm 0.003$
eat	336	$0.003 \pm 0.001$	$0.043 \pm 0.004$	$0.006 \pm 0.001$	$0.058 \pm 0.006$	$0.006 \pm 0.001$	$0.062 \pm 0.007$	$0.004 \pm 0.001$	$0.048 \pm 0.004$
Μ	720	$0.004 \pm 0.002$	$0.049\pm0.007$	$0.007 \pm 0.001$	$0.063 \pm 0.004$	$0.006 \pm 0.001$	$0.06\pm0.007$	$0.004 \pm 0.0$	$0.049 \pm 0.003$
		N-BE/	ATS-G		AA			'	
		N-BEA MSE	ATS-G MAE	TS MSE	AA MAE				<u> </u>
	96		MAE						'
m2	96 192	MSE		MSE	MAE				'
TTm2		$  MSE \\ 0.08 \pm 0.005 $	$\frac{\text{MAE}}{0.21 \pm 0.007}$		$\begin{array}{c} \text{MAE} \\ 0.192 \pm 0.002 \end{array}$			·	
ETTm2	192		$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \end{array}$	$MSE = 0.068 \pm 0.001$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \end{array}$			·	
	$\frac{192}{336}$		$\begin{array}{c} {\rm MAE} \\ \\ \hline 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \end{array}$		$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \end{array}$				
	192 336 720	$\begin{tabular}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} {\rm MAE} \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \end{array}$	$\begin{tabular}{ c c c c c } MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \end{array}$				
	192 336 720 96	$\begin{tabular}{ c c c c c c c } MSE \\ \hline 0.08 \pm 0.005 \\ 0.11 \pm 0.004 \\ 0.172 \pm 0.007 \\ 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \end{array}$	$\begin{tabular}{ c c c c c } MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ \hline 0.354 \pm 0.012 \end{array}$				
Electricity ETTm2	192 336 720 96 192	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \end{array}$	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ \end{array} \\ \hline 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \end{array}$				
Electricity	192 336 720 96 192 336	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \end{array}$	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ 0.31 \pm 0.006 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ \end{array} \\ \hline \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \end{array}$				
Electricity	192 336 720 96 192 336 720	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \end{array}$	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ \hline 0.096 \pm 0.001 \\ \hline 0.139 \pm 0.005 \\ \hline 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ \hline 0.277 \pm 0.003 \\ \hline 0.31 \pm 0.006 \\ \hline 0.378 \pm 0.026 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \end{array}$				
Electricity	192 336 720 96 192 336 720 96	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \\ 0.351 \pm 0.045 \end{array}$	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ 0.31 \pm 0.006 \\ 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ \hline 0.236 \pm 0.007 \end{array}$				
	192 336 720 96 192 336 720 96 192	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ \hline 0.783 \pm 0.203 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \\ 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \end{array}$	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ 0.31 \pm 0.006 \\ 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ 0.215 \pm 0.035 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ \end{array} \\ \begin{array}{c} 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ \end{array} \\ \begin{array}{c} 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \end{array}$				
Exchange   Electricity	192 336 720 96 192 336 720 96 192 336	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.363 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ \hline 0.783 \pm 0.203 \\ \hline 2.622 \pm 1.07 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \\ 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \\ 1.266 \pm 0.23 \\ \end{array}$	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ 0.31 \pm 0.006 \\ 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ 0.215 \pm 0.035 \\ 0.532 \pm 0.045 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ \end{array} \\ \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ \end{array} \\ \\ \begin{array}{c} 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \\ 0.572 \pm 0.006 \end{array}$				
Exchange   Electricity	192 336 720 96 192 336 720 96 192 336 720	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ \hline 0.783 \pm 0.203 \\ \hline 2.622 \pm 1.07 \\ \hline 2.588 \pm 0.11 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \\ 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \\ 1.266 \pm 0.23 \\ 1.303 \pm 0.019 \\ \end{array}$	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ 0.31 \pm 0.006 \\ 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ 0.215 \pm 0.035 \\ 0.532 \pm 0.045 \\ 0.527 \pm 0.047 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \\ 0.572 \pm 0.006 \\ 0.594 \pm 0.019 \\ \end{array}$			·	
Exchange   Electricity	192 336 720 96 192 336 720 96 192 336 720 96	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ \hline 0.783 \pm 0.203 \\ \hline 2.622 \pm 1.07 \\ \hline 2.588 \pm 0.11 \\ \hline 0.159 \pm 0.001 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \hline 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \\ 1.266 \pm 0.23 \\ 1.303 \pm 0.019 \\ \hline 0.24 \pm 0.002 \end{array}$	$\begin{tabular}{ c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ 0.31 \pm 0.006 \\ 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ 0.215 \pm 0.035 \\ 0.532 \pm 0.045 \\ 0.527 \pm 0.047 \\ \hline 0.158 \pm 0.001 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \\ 0.572 \pm 0.006 \\ 0.594 \pm 0.019 \\ 0.239 \pm 0.001 \end{array}$				
Electricity	192 336 720 96 192 336 720 96 192 336 720 96 192	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ \hline 0.783 \pm 0.203 \\ \hline 2.622 \pm 1.07 \\ \hline 2.588 \pm 0.11 \\ \hline 0.159 \pm 0.001 \\ \hline 0.181 \pm 0.005 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \hline 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \\ 1.266 \pm 0.23 \\ 1.303 \pm 0.019 \\ \hline 0.24 \pm 0.002 \\ 0.264 \pm 0.001 \\ \hline \end{array}$	$\begin{tabular}{ c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ 0.31 \pm 0.006 \\ 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ 0.215 \pm 0.035 \\ 0.532 \pm 0.045 \\ 0.527 \pm 0.047 \\ \hline 0.158 \pm 0.001 \\ 0.16 \pm 0.0 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \\ 0.572 \pm 0.006 \\ 0.594 \pm 0.019 \\ 0.239 \pm 0.001 \\ 0.243 \pm 0.001 \\ \end{array}$				
Traffic   Exchange   Electricity	192 336 720 96 192 336 720 96 192 336 720 96 192 336	$\begin{tabular}{ c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ \hline 0.783 \pm 0.203 \\ \hline 2.622 \pm 1.07 \\ \hline 2.588 \pm 0.11 \\ \hline 0.159 \pm 0.001 \\ \hline 0.181 \pm 0.005 \\ \hline 0.155 \pm 0.001 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \hline 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \\ 1.266 \pm 0.23 \\ 1.303 \pm 0.019 \\ \hline 0.24 \pm 0.002 \\ 0.264 \pm 0.001 \\ 0.239 \pm 0.001 \\ \hline \end{array}$	$\begin{tabular}{ c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ 0.096 \pm 0.001 \\ 0.139 \pm 0.005 \\ 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ 0.277 \pm 0.003 \\ 0.31 \pm 0.006 \\ 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ 0.215 \pm 0.035 \\ 0.532 \pm 0.045 \\ 0.527 \pm 0.047 \\ \hline 0.158 \pm 0.001 \\ 0.156 \pm 0.004 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \\ 0.572 \pm 0.006 \\ 0.594 \pm 0.019 \\ 0.239 \pm 0.001 \\ 0.243 \pm 0.001 \\ 0.244 \pm 0.006 \end{array}$				
Traffic   Exchange   Electricity	192 336 720 96 192 336 720 96 192 336 720 96 192 336 720	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ 0.11 \pm 0.004 \\ 0.172 \pm 0.007 \\ 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ 0.363 \pm 0.005 \\ 0.392 \pm 0.002 \\ 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ 0.783 \pm 0.203 \\ 2.622 \pm 1.07 \\ 2.588 \pm 0.11 \\ \hline 0.159 \pm 0.001 \\ 0.181 \pm 0.005 \\ 0.155 \pm 0.001 \\ 0.212 \pm 0.003 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \hline 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \hline 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \hline 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \\ 1.266 \pm 0.23 \\ 1.303 \pm 0.019 \\ \hline 0.24 \pm 0.002 \\ 0.264 \pm 0.001 \\ 0.239 \pm 0.001 \\ 0.304 \pm 0.003 \\ \end{array}$	$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \\ 0.572 \pm 0.006 \\ 0.594 \pm 0.019 \\ 0.239 \pm 0.001 \\ 0.243 \pm 0.001 \\ 0.244 \pm 0.006 \\ 0.279 \pm 0.003 \\ \end{array}$			·	
Traffic   Exchange   Electricity	192 336 720 96 192 336 720 96 192 336 720 96 192 336 720 96	$\begin{tabular}{ c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ 0.11 \pm 0.004 \\ 0.172 \pm 0.007 \\ 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ 0.363 \pm 0.005 \\ 0.392 \pm 0.002 \\ 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ 0.783 \pm 0.203 \\ 2.622 \pm 1.07 \\ 2.588 \pm 0.11 \\ \hline 0.159 \pm 0.001 \\ 0.181 \pm 0.005 \\ 0.155 \pm 0.001 \\ 0.212 \pm 0.003 \\ \hline 0.003 \pm 0.0 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \\ 1.266 \pm 0.23 \\ 1.303 \pm 0.019 \\ \hline 0.24 \pm 0.002 \\ 0.264 \pm 0.001 \\ 0.239 \pm 0.001 \\ 0.304 \pm 0.003 \\ \hline 0.043 \pm 0.002 \\ \end{array}$	$\begin{tabular}{ c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ \hline 0.096 \pm 0.001 \\ \hline 0.139 \pm 0.005 \\ \hline 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ \hline 0.277 \pm 0.003 \\ \hline 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ \hline 0.215 \pm 0.035 \\ \hline 0.527 \pm 0.047 \\ \hline 0.158 \pm 0.001 \\ \hline 0.156 \pm 0.004 \\ \hline 0.189 \pm 0.002 \\ \hline 0.001 \pm 0.0 \\ \hline 0.001 \pm 0.0 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \\ 0.572 \pm 0.006 \\ 0.594 \pm 0.019 \\ 0.239 \pm 0.001 \\ 0.243 \pm 0.001 \\ 0.244 \pm 0.006 \\ 0.279 \pm 0.003 \\ 0.024 \pm 0.0 \end{array}$			·	
Exchange   Electricity	192 336 720 96 192 336 720 96 192 336 720 96 192 336 720 96 192 336 720	$\begin{tabular}{ c c c c c } \hline MSE \\ \hline 0.08 \pm 0.005 \\ \hline 0.11 \pm 0.004 \\ \hline 0.172 \pm 0.007 \\ \hline 0.201 \pm 0.008 \\ \hline 0.324 \pm 0.005 \\ \hline 0.363 \pm 0.005 \\ \hline 0.392 \pm 0.002 \\ \hline 0.489 \pm 0.013 \\ \hline 0.223 \pm 0.046 \\ \hline 0.783 \pm 0.203 \\ \hline 2.622 \pm 1.07 \\ \hline 2.588 \pm 0.11 \\ \hline 0.159 \pm 0.001 \\ \hline 0.181 \pm 0.005 \\ \hline 0.155 \pm 0.001 \\ \hline 0.212 \pm 0.003 \\ \hline 0.003 \pm 0.0 \\ \hline 0.004 \pm 0.001 \\ \hline \end{tabular}$	$\begin{array}{c} {\rm MAE} \\ \\ 0.21 \pm 0.007 \\ 0.25 \pm 0.005 \\ 0.32 \pm 0.007 \\ 0.353 \pm 0.008 \\ \\ 0.397 \pm 0.002 \\ 0.42 \pm 0.003 \\ 0.443 \pm 0.006 \\ 0.502 \pm 0.005 \\ \\ 0.351 \pm 0.045 \\ 0.675 \pm 0.085 \\ 1.266 \pm 0.23 \\ 1.303 \pm 0.019 \\ \\ 0.24 \pm 0.002 \\ 0.264 \pm 0.001 \\ 0.239 \pm 0.001 \\ 0.304 \pm 0.003 \\ \\ 0.043 \pm 0.002 \\ 0.047 \pm 0.004 \\ \end{array}$	$\begin{tabular}{ c c c c } \hline MSE \\ \hline 0.068 \pm 0.001 \\ \hline 0.096 \pm 0.001 \\ \hline 0.139 \pm 0.005 \\ \hline 0.187 \pm 0.008 \\ \hline 0.244 \pm 0.006 \\ \hline 0.277 \pm 0.003 \\ \hline 0.31 \pm 0.006 \\ \hline 0.378 \pm 0.026 \\ \hline 0.093 \pm 0.008 \\ \hline 0.215 \pm 0.035 \\ \hline 0.527 \pm 0.047 \\ \hline 0.158 \pm 0.001 \\ \hline 0.156 \pm 0.001 \\ \hline 0.189 \pm 0.002 \\ \hline 0.001 \pm 0.0 $	$\begin{array}{c} {\rm MAE} \\ \\ 0.192 \pm 0.002 \\ 0.237 \pm 0.004 \\ 0.29 \pm 0.005 \\ 0.336 \pm 0.001 \\ 0.354 \pm 0.012 \\ 0.368 \pm 0.003 \\ 0.394 \pm 0.005 \\ 0.447 \pm 0.012 \\ 0.236 \pm 0.007 \\ 0.352 \pm 0.017 \\ 0.572 \pm 0.006 \\ 0.594 \pm 0.019 \\ 0.239 \pm 0.001 \\ 0.243 \pm 0.001 \\ 0.244 \pm 0.006 \\ 0.279 \pm 0.003 \\ 0.024 \pm 0.0 \\ 0.027 \pm 0.001 \\ 0.027 \pm 0.001 \\ \end{array}$				

Table 16: Univariate long-term time-series forecasting results with the standard deviation.

### E.3 Comparing with Crossformer, PatchTST, and iTransformer models

Multivariate results for TSAA using the baselines: Crossformer, PatchTST, and iTransformer. Each result reports an average of three random seeds, with a lookback of 96. The results are presented in Tabs. 17, 18, and 19.

#### E.4 Autoformer and FEDformer augmented with the best augmentations

We show in Tabs. 20 and 21 a comparison between TSAA and Autoformer and FEDformer, respectively. Specifically, we train from scratch Autoformer and FEDformer only using the best augmentations found by TSAA. Overall, the results are inconsistent, highlighting that in some cases, these augmentations yield strong

-			former			SAA	
		MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$
5	96	0.263	0.35	0.197	0.283	25.095	19.143
$ETTm_2$	192	0.476	0.492	0.273	0.336	42.647	31.707
E	336	0.855	0.638	0.335	0.378	60.819	40.752
E	720	3.293	1.26	0.397	0.4	87.944	68.254
	96	0.144	0.243	0.141	0.24	2.083	1.235
ECL	192	0.165	0.264	0.157	0.254	4.848	3.788
Ĕ	336	0.189	0.287	0.175	0.275	7.407	4.181
	720	0.249	0.332	0.208	0.302	16.466	9.036
e	96	0.187	0.339	0.307	0.416	-64.171	-22.714
Exchange	192	0.61	0.623	1.022	0.757	-67.541	-21.509
ch	336	1.023	0.803	0.941	0.724	8.016	9.838
Ê	720	1.295	0.921	1.621	0.921	-25.174	0.0
~	96	0.684	0.399	0.68	0.4	0.585	-0.251
Ĕ	192	0.94	0.546	0.935	0.547	0.532	-0.183
Traffic	336	1.127	0.661	1.059	0.635	6.034	3.933
<u> </u>	720	1.349	0.792	1.345	0.796	0.297	-0.505
ħ	96	0.164	0.236	0.17	0.226	-3.659	4.237
Weather	192	0.217	0.301	0.228	0.279	-5.069	7.309
/ea	336	0.266	0.325	0.253	0.315	4.887	3.077
5	720	0.383	0.396	0.31	0.35	19.06	11.616
	24	4.324	1.413	4.267	1.401	1.318	0.849
ILI	36	4.565	1.432	4.261	1.375	6.659	3.98
	48	4.603	1.437	3.741	1.271	18.727	11.552
	60	4.571	1.435	4.193	1.362	8.27	5.087
				_			
	'Ta	ble 19	: i'Tra	nsforr	ner mu	iltivaria	ate
		iTrans	former		Г	SAA	
		MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$

Table 17: Crossformer multivariate

		Table 18: Patch 151 multivariate						
		Patcl	nTST		Г	SAA		
		MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$	
5	96	0.175	0.259	0.175	0.256	0.0	1.158	
E	192	0.242	0.303	0.24	0.301	0.826	0.66	
$ETTm_2$	336	0.303	0.341	0.302	0.339	0.33	0.587	
щ	720	0.401	0.399	0.4	0.396	0.249	0.752	
	96	0.187	0.269	0.187	0.269	0.0	0.0	
ECL	192	0.191	0.274	0.191	0.274	0.0	0.0	
Ĕ	336	0.206	0.29	0.206	0.289	0.0	0.345	
	720	0.248	0.323	0.248	0.324	0.0	-0.31	
ee	96	0.08	0.197	0.088	0.205	-10.0	-4.061	
Exchange	192	0.168	0.291	0.17	0.292	-1.19	-0.344	
ćch	336	0.313	0.403	0.312	0.403	0.319	0.0	
臣	720	0.818	0.679	0.818	0.679	0.0	0.0	
	96	0.523	0.339	0.521	0.337	0.382	0.59	
Traffic	192	0.519	0.333	0.517	0.332	0.385	0.3	
Ira	336	0.529	0.337	0.528	0.336	0.189	0.297	
	720	0.563	0.355	0.561	0.354	0.355	0.282	
Ħ	96	0.187	0.225	0.184	0.222	1.604	1.333	
Weather	192	0.233	0.264	0.232	0.263	0.429	0.379	
Vea	336	0.284	0.3	0.283	0.299	0.352	0.333	
5	720	0.356	0.347	0.355	0.346	0.281	0.288	
	24	2.335	0.975	2.079	0.938	10.964	3.795	
ILI	36	2.259	0.962	1.784	0.878	21.027	8.732	
п	48	2.41	0.992	2.157	0.949	10.498	4.335	
	60	2.297	0.965	1.947	0.918	15.237	4.87	

Table 18: PatchTST multivariate

	Ta	ble 19	: iTra	nsform	ner mu	ultivaria	ate
		iTrans	former		Г	SAA	
		MSE	MAE	MSE↓	$\mathrm{MAE}{\downarrow}$	$\mathrm{MSE}\%\uparrow$	$\mathrm{MAE}\%\uparrow$
2	96	0.184	0.27	0.18	0.259	2.174	4.074
$ETTm_2$	192	0.251	0.312	0.246	0.302	1.992	3.205
E	336	0.315	0.351	0.311	0.345	1.27	1.709
Ξ	720	0.41	0.405	0.403	0.397	1.707	1.975
	96	0.147	0.239	0.147	0.239	0.0	0.0
ECL	192	0.163	0.255	0.163	0.255	0.0	0.0
Ĕ	336	0.178	0.271	0.176	0.269	1.124	0.738
	720	0.208	0.298	0.209	0.297	-0.481	0.336
ee.	96	0.088	0.208	0.09	0.21	-2.273	-0.962
Exchange	192	0.18	0.303	0.181	0.304	-0.556	-0.33
ch	336	0.337	0.42	0.34	0.424	-0.89	-0.952
ΕX	720	0.864	0.704	0.906	0.723	-4.861	-2.699
	96	0.393	0.267	0.393	0.267	0.0	0.0
Traffic	192	0.412	0.277	0.412	0.275	0.0	0.722
Ira	336	0.423	0.282	0.423	0.281	0.0	0.355
<u> </u>	720	0.459	0.3	0.459	0.299	0.0	0.333
E.	96	0.175	0.215	0.173	0.212	1.143	1.395
Weather	192	0.227	0.261	0.226	0.259	0.441	0.766
ea	336	0.282	0.3	0.282	0.3	0.0	0.0
14	720	0.357	0.349	0.36	0.352	-0.84	-0.86
	24	2.775	1.11	2.565	1.065	7.568	4.054
Б	36	2.668	1.061	2.348	0.996	11.994	6.126
ILI	48	2.663	1.082	2.294	0.997	13.857	7.856
	60	2.921	1.159	2.651	1.098	9.243	5.263

results, but in other cases, results are inferior. In comparison, TSAA is consistent across all models and datasets.

#### E.5 Limitations of TSAA

TSAA shows less favorable results when applied to the Exchange dataset. While several factors may contribute to this underperformance, we would like to focus on what we believe is the key distinction of this dataset compared to others, supported by additional experiments. The Exchange dataset captures foreign exchange prices between major currency pairs, categorizing it as financial data similar to stock market data. It is widely accepted that financial data often exhibits random fluctuations, characteristic of a random walk (RW)

ma	gnitude	01 0.5.									
		TD MSE	TD MAE	Jittering MSE	Jittering MAE	Mixup MSE	Mixup MAE	Smooth MSE	Smooth MAE	TSAA MSE	TSAA MAE
	$\rm pred\_len$										
5	96	0.253	0.324	0.265	0.33	0.236	0.317	0.278	0.337	0.211	0.293
$^{2}m^{2}$	192	0.344	0.368	0.29	0.344	0.277	0.335	0.293	0.349	0.269	0.327
ETT	336	0.353	0.384	0.419	0.418	0.341	0.371	<u>0.334</u>	<u>0.37</u>	0.322	0.359
되	720	0.439	0.432	0.473	0.452	0.426	0.417	0.433	0.426	0.41	0.407
	Avg.	0.347	0.377	0.362	0.386	<u>0.32</u>	<u>0.36</u>	0.334	0.37	0.303	0.346
	96	0.632	0.402	0.623	0.385	0.633	0.401	0.634	0.396	0.602	0.375
Traffic	192	0.659	0.415	0.667	0.416	0.742	0.463	0.632	0.401	0.663	0.416
Dra	336	0.645	0.402	0.634	0.398	0.683	0.429	0.654	0.408	0.627	0.387
<u> </u>	720	0.679	0.416	0.665	0.407	0.744	0.455	0.661	0.406	0.662	0.405
	Avg.	0.654	0.409	0.647	0.401	0.7	0.437	0.645	0.403	0.639	0.396
H	96	0.242	0.317	0.259	0.328	0.222	0.297	0.246	0.32	0.216	0.292
Weather	192	0.295	0.355	0.324	0.375	<u>0.286</u>	0.346	0.331	0.382	0.278	0.336
/ea	336	0.367	0.4	0.358	0.391	0.327	0.367	0.379	0.408	0.341	0.381
14	720	0.436	0.443	0.428	0.43	0.396	0.411	0.449	0.449	0.397	0.41
	Avg.	<u>0.335</u>	<u>0.379</u>	0.342	0.381	0.308	0.355	0.351	0.39	0.308	0.355
	24	3.398	1.284	3.656	1.311	3.709	1.35	3.463	1.289	3.565	1.302
Ц	36	2.897	1.117	2.878	1.096	3.024	1.135	2.812	1.087	2.754	1.068
ILI	48	2.879	1.126	2.94	1.132	3.048	1.171	2.841	1.111	2.856	1.114
	60	2.85	1.135	2.849	<u>1.118</u>	3.106	1.198	2.805	1.114	<u>2.826</u>	<u>1.118</u>
	Avg.	3.006	1.166	3.081	1.164	3.222	1.214	2.98	1.15	3.0	1.15

Table 20: Autoformer: TSAA compared to the direct application of the best-performing transformations trend downscaling (TD), jittering, mixup, and smoothing. Each transformation was deployed with a fixed magnitude of 0.5.

Table 21: FEDformer: TSAA compared to the direct application of the best-performing transformations trend downscaling (TD), jittering, mixup, and smoothing. Each transformation was deployed with a fixed magnitude of 0.5.

	,	TD MSE	TD MAE	Jittering MSE	Jittering MAE	Mixup MSE	Mixup MAE	Smooth MSE	Smooth MAE	TSAA MSE	TSAA MAE
	${\rm pred\_len}$				-	_	_				
2	96	0.187	0.274	0.187	0.279	0.185	0.276	0.192	0.285	0.187	0.274
$\mathbb{C}$ m2	192	<u>0.253</u>	0.315	0.254	0.321	0.252	0.318	0.264	0.33	0.255	0.314
ETT	336	0.313	0.354	0.322	0.366	0.32	0.358	0.324	0.365	0.311	0.35
E	720	0.409	0.409	0.427	0.425	0.42	0.414	0.424	0.42	0.406	0.403
	Avg.	0.29	<u>0.338</u>	0.298	0.348	<u>0.294</u>	0.342	0.301	0.35	0.29	0.335
	96	0.596	0.382	0.575	0.36	0.592	0.379	0.592	0.368	0.577	0.362
Traffic	192	0.629	0.397	0.604	0.373	0.619	0.393	0.612	0.378	0.601	0.371
Ira	336	0.635	0.401	<u>0.62</u>	0.384	0.635	0.403	0.629	0.386	0.619	0.383
τ.	720	0.646	0.4	0.629	0.385	0.664	0.415	0.639	<u>0.387</u>	0.632	0.388
	Avg.	0.626	0.395	0.607	0.376	0.628	0.398	0.618	<u>0.38</u>	0.607	0.376
н	96	0.228	0.307	0.283	0.358	0.199	0.271	0.217	0.296	0.207	0.285
Weather	192	0.264	0.323	0.314	0.364	0.249	0.308	0.324	0.372	0.252	<u>0.311</u>
/ea	336	0.318	0.357	0.368	0.398	0.305	0.345	0.359	0.394	0.313	0.355
5	720	0.393	0.401	0.417	0.421	0.377	0.385	0.419	0.422	0.382	0.395
	Avg.	0.301	0.347	0.346	0.385	0.282	0.327	0.33	0.371	0.288	<u>0.336</u>
	24	3.306	1.272	3.272	1.254	3.544	1.329	3.258	1.253	3.15	1.219
П	36	2.682	1.082	2.638	1.063	2.877	1.127	2.653	1.069	2.578	1.049
ILLI	48	2.656	1.088	<u>2.61</u>	1.067	2.844	1.135	2.618	1.073	2.609	<u>1.069</u>
	60	2.92	1.178	2.87	1.158	3.072	1.213	2.832	<u>1.148</u>	2.805	1.14
	Avg.	2.891	1.155	2.848	<u>1.136</u>	3.084	1.201	2.84	<u>1.136</u>	2.786	1.119

behavior, as suggested in (Fama, 1965). We hypothesize that the random walk component is dominant in the Exchange dataset, which may explain why TSAA encounters difficulties when applied to datasets with a strong random walk influence.

To empirically validate our hypothesis, we evaluated the performance of TSAA on two different types of datasets: (1) A seasonal dataset (w/o RW), characterized by strong seasonal components without any random walk influence, and (2) A seasonal + random walk dataset (+RW), where a random walk component was added to the seasonal data. To further remove stationarity, both series were multiplied by an additional random walk vector, formally represented as: (1)  $x_s * x_{rw}$ , and (2)  $(x_s + x_{rw}) * \hat{x}_{rw}$ , where  $x_s$  is the seasonal component, and  $x_{rw}$  and  $\hat{x}_{rw}$  are two independent random walk vectors, with the operation \* applied element-wise. Examples of these datasets are illustrated in Fig. 7. The results indicate that, for both Autoformer and FEDformer, performance on the dataset containing a random walk component (+RW) is notably lower compared to the seasonal dataset (w/o RW), despite both sharing the same  $x_s$  and  $x_{rw}$  components. Specifically, the median and mean performance on the (w/o RW) dataset consistently surpass those of the (+RW) dataset across all

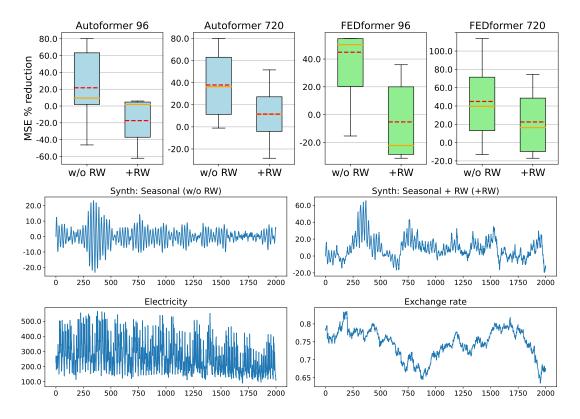
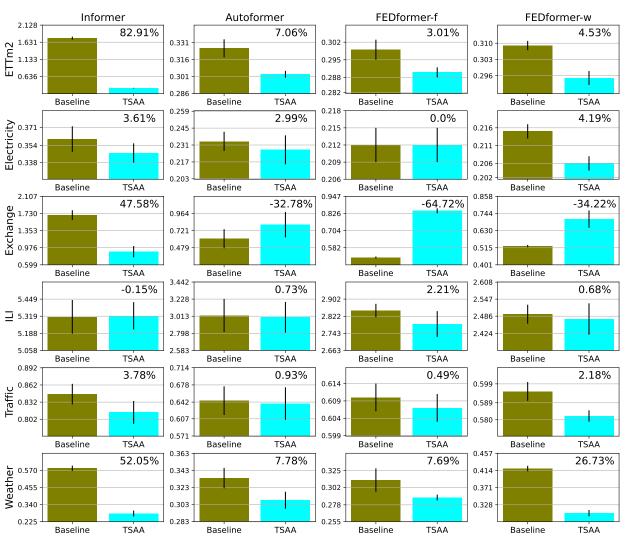


Figure 7: Top: MSE % reduction with TSAA for two synthetic datasets characterized by a seasonal component only (w/o RW), and a seasonal component with a random walk (+RW), respectively. The red dashed line and the orange line represent the mean and median respectively. The reported results represent the performance of five different setups. Bottom: Samples of the synthetic datasets used in the given experiments, and real datasets with similar corresponding characteristics.

configurations, as shown in Fig. 7. In our experiment, five different setups using generated datasets were tested, each maintaining the same  $x_s$ ,  $x_{rw}$ , and  $\hat{x}_{rw}$  components.

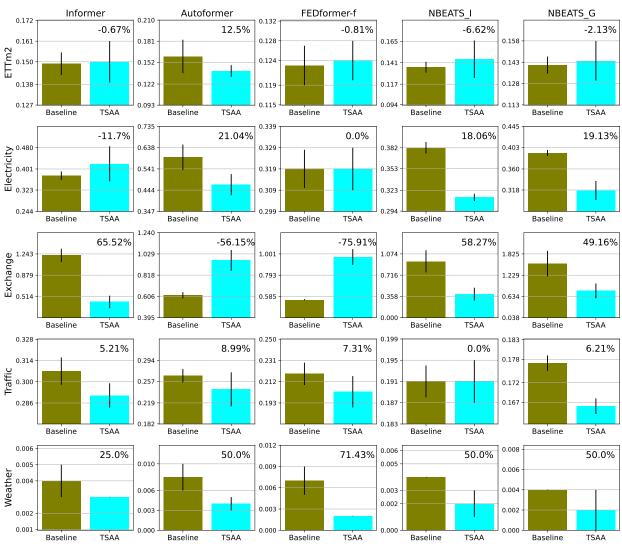
### E.6 Further results

In this section we provide bar comparisons of the results presented in E.1.



Multivariate

Figure 8: Multivariate comparison between TSAA and the baseline models per dataset. Rows represent the datasets and columns represent the models. Each score represents the average MSE across all four horizons, namely, 96,192,336, and 720.



Univariate

Figure 9: Univariate comparison between TSAA and the baseline models per dataset. Rows represent the datasets and columns represent the models. Each score represents the average MSE across all four horizons, namely, 96,192,336, and 720.

Dataset	Horizon	Baseline MSE	Baseline MAE	RandAugment MSE	RandAugment MAE	Fast AA MSE	Fast AA MAE	TSAA MSE	TSAA MAE
2	96	0.545	0.588	0.417	0.498	0.443	0.488	0.224	0.321
, E	192	1.054	0.808	0.583	0.579	0.796	0.661	0.27	0.355
ETTm2	336	1.523	0.948	0.957	0.757	1.565	0.974	0.304	0.374
E	720	3.878	1.474	<u>1.266</u>	0.886	3.639	1.469	0.398	0.435
-	96	0.336	0.416	0.325	0.418	0.369	0.445	0.324	0.407
ECL	192	0.36	0.441	0.347	0.435	0.388	0.463	0.336	0.419
Ĕ	336	0.356	0.439	0.354	0.441	0.916	0.776	0.347	0.429
	720	0.386	0.452	<u>0.385</u>	0.453	1.016	0.818	0.381	0.448
	96	0.744	0.42	0.754	0.425	0.948	0.539	0.723	0.408
Traffic	192	<u>0.753</u>	0.426	0.78	0.434	1.446	0.777	0.735	0.414
Ira	336	<u>0.876</u>	0.495	0.926	0.52	1.484	0.814	0.811	0.462
	720	<u>1.011</u>	0.578	1.12	0.632	1.511	0.819	0.985	0.566
J.	96	0.315	0.382	0.489	0.485	0.258	<u>0.339</u>	0.18	0.256
Weather	192	0.428	0.449	0.468	0.488	0.415	0.456	0.253	0.331
/ea	336	0.62	0.554	0.585	0.551	<u>0.542</u>	0.519	0.296	0.361
м	720	0.975	0.722	1.0	0.741	<u>0.819</u>	0.665	0.392	0.426
	24	5.349	1.582	4.82	1.451	<u>5.046</u>	<u>1.505</u>	5.313	1.559
ILI	36	5.203	1.572	4.326	1.385	5.264	<u>1.549</u>	5.26	1.581
Ξ	48	5.286	1.594	4.655	1.456	5.449	1.596	5.415	1.623
	60	5.419	1.62	4.542	1.448	5.684	1.659	<u>5.3</u>	<u>1.593</u>

Table 22: Informer: Comparison of automatic augmentation approaches including TSAA, Fast AutoAugment and RandAugment.

Table 23: Autoformer: Comparison of automatic augmentation approaches including TSAA, Fast AutoAugment and RandAugment.

Dataset	Horizon	Baseline MSE	Baseline MAE	RandAugment MSE	RandAugment MAE	Fast AA MSE	Fast AA MAE	TSAA MSE	TSAA MAE
ETTm2	96	0.231	0.31	0.223	0.307	0.222	0.303	0.211	0.293
	192	0.289	0.346	0.286	0.343	<u>0.282</u>	0.334	0.269	0.327
	336	0.341	0.375	0.333	<u>0.371</u>	0.352	0.377	0.322	0.359
	720	0.444	0.434	0.427	0.42	<u>0.422</u>	<u>0.413</u>	0.41	0.407
ECL	96	0.2	0.316	0.192	0.307	0.213	0.321	0.188	0.302
	192	0.217	0.326	0.217	0.326	0.249	0.346	0.221	0.328
	336	0.258	0.356	0.232	0.341	<u>0.25</u>	0.354	0.252	0.352
	720	0.261	0.363	0.279	0.378	0.274	0.37	0.248	0.351
Traffic	96	0.615	0.384	0.637	0.394	0.663	0.418	0.602	0.375
	192	0.67	0.421	0.636	0.393	0.764	0.48	0.663	0.416
	336	0.635	0.392	0.632	0.392	0.711	0.443	0.627	0.387
	720	0.658	0.402	0.663	0.409	0.872	0.526	0.662	0.405
Weather	96	0.259	0.332	0.251	0.325	0.196	0.26	0.216	0.292
	192	0.298	0.356	0.286	0.344	0.255	0.304	0.278	0.336
	336	0.357	0.394	0.328	0.364	0.307	0.338	0.341	0.381
	720	0.422	0.431	0.436	0.445	0.375	0.381	0.397	0.41
ГП	24	3.549	1.305	3.774	1.354	4.737	1.603	3.565	1.302
	36	2.834	1.094	2.89	1.103	3.864	1.375	2.754	1.068
	48	2.889	1.122	2.575	1.045	3.766	1.368	2.856	1.114
	60	<u>2.818</u>	<u>1.118</u>	2.775	1.108	3.92	1.412	2.826	<u>1.118</u>

Table 24: FEDformer-f: Comparison of automatic augmentation approaches including TSAA, Fast AutoAugment and RandAugment.

Dataset	Horizon	Baseline MSE	Baseline MAE	RandAugment MSE	RandAugment MAE	Fast AA MSE	Fast AA MAE	TSAA MSE	TSAA MAE
ETTm2	96	0.189	0.282	0.192	0.282	0.197	0.279	0.187	0.274
	192	0.258	0.326	0.257	0.323	0.262	0.319	0.255	0.314
	336	0.323	0.363	0.326	0.364	0.322	0.356	0.311	0.35
	720	0.425	0.421	0.43	0.422	0.415	0.407	0.406	0.403
ECL	96	0.185	0.3	0.19	0.304	0.201	0.313	0.185	0.3
	192	0.201	0.316	0.206	0.318	0.203	0.315	0.201	0.316
	336	0.214	0.329	0.227	0.338	0.22	0.331	0.214	0.329
	720	0.246	0.353	0.291	0.385	0.254	0.357	0.246	0.353
Traffic	96	0.577	0.361	0.59	0.376	0.655	0.41	0.577	0.362
	192	0.61	0.379	0.622	0.39	0.652	0.408	0.601	0.371
	336	0.623	0.385	0.626	0.392	0.674	0.421	0.619	0.383
	720	0.632	0.388	<u>0.643</u>	0.396	0.705	0.427	0.632	0.388
Weather	96	0.236	0.316	0.203	0.275	0.191	0.252	0.207	0.285
	192	0.273	0.333	0.267	0.331	0.24	0.29	0.252	0.311
	336	0.332	0.371	0.329	0.368	0.29	0.321	0.313	0.355
	720	0.408	0.418	0.398	0.413	0.363	0.367	0.382	<u>0.395</u>
III	24	3.268	1.257	3.16	<u>1.234</u>	4.671	1.612	3.15	1.219
	36	2.648	1.068	2.457	1.019	3.835	1.377	<u>2.578</u>	<u>1.049</u>
	48	2.615	1.072	2.558	1.06	3.694	1.359	2.609	<u>1.069</u>
	60	2.866	1.158	<u>2.822</u>	<u>1.146</u>	3.855	1.41	2.805	1.14