A Bayesian Approach to Designing Microstructures and Processing Pathways for Tailored Material Properties

Adam P. Generale¹ Conlain Kelly² Grayson H. Harrington² Andreas E. Robertson¹ Michael O. Buzzy² Surya R. Kalidindi^{1,2†}

¹ George W. Woodruff School of Mechanical Engineering
 ² School of Computational Science and Engineering
 † Corresponding author
 Georgia Institute of Technology, Atlanta GA 30332

{agenerale3,ckelly84,grayson.harrington,arobertson38,mbuzzy3}@gatech.edu surya.kalidindi@me.gatech.com

Abstract

Inverse problems are central to material design. While numerous studies have focused on designing microstructures by inverting structure-property linkages for various material systems, such efforts stop short of providing realizable paths to manufacture such structures. Accomplishing the dual task of designing a microstructure and a feasible manufacturing pathway to achieve a target property requires inverting the complete process-structure-property linkage. However, this inversion is complicated by a variety of challenges such as inherent microstructure stochasticity, high-dimensionality, and ill-conditioning of the inversion. In this work, we propose a Bayesian framework leveraging a lightweight flowbased generative approach for the stochastic inversion of the complete processstructure-property linkage. This inversion identifies a solution distribution in the processing parameter space; utilizing these processing conditions realizes materials with the target property sets. Our modular framework readily incorporates the output of stochastic forward models as conditioning variables for a flow-based generative model, thereby learning the complete joint distribution over processing parameters and properties. We demonstrate its application to the multi-objective task of designing processing routes of heterogeneous materials given target sets of bulk elastic moduli and thermal conductivities.

1 Introduction

The problems of material discovery, development, and deployment have historically been posed in the form of *inverse problems* [1] – mathematical challenges which repeatedly appear across almost every discipline [2–9]. In the context of materials, the primary challenges involve mapping between the spaces of material processing parameters Ω_1 , microstructures Ω_2 , and resulting functional properties Ω_3 . This introduces the notion of process–structure (PS) and structure–property forward linkages, which we denote as $\mathcal{G} : \Omega_1 \to \Omega_2$ and $\mathcal{F} : \Omega_2 \to \Omega_3$. However, the underlying goal of inverting the relationship between processing and property, remains an open problem. This composite relation $\mathcal{H} = \mathcal{F} \circ \mathcal{G} : \Omega_1 \to \Omega_3$ is commonly referred to as a process–structure–property (PSP) linkage.

It is impossible to disentangle material microstructures from how they deform, and consequently their bulk properties and performance. Unfortunately, consideration of microstructures introduces significant complexities to materials-specific inverse problems [1, 10]. First, material microstructures are complex hierarchical stochastic systems spanning a wide range of lengthscales [11, 12]. Across these length-scales, the evolution of local material states during processing steps, as well as their bulk response to external stimuli, are highly nonlinear and stochastic in nature [13–20]. Second, microstructure representation is inherently irregular and high-dimensional [21], such that any PS, $\mathcal{G}(\cdot)$, or SP linkage, $\mathcal{F}(\cdot)$, would necessarily need to be capable of modeling or approximating this behavior across high-dimensional domains. Taken as a whole, these factors result in an ill-posed and unstable composite inversion problem. In the presence of such stochastic forward models, the problem is more formally known as a *stochastic inverse problem* [22].

As a direct result of these challenges, current works have primarily focused on inverting individual SP linkages [23–30]. Even these works have achieved significant advancements over traditional approaches [15, 31, 32] through their use of distributional deep learning [33–38]. By learning a mapping of individual samples from the complex, irregular microstructure space to a topologically-well-structured, continuous latent space, traversal of this latent space can lead to the identification of unique and undiscovered materials. However, these current approaches rarely account for microstructure stochasticity. Further, learned latent spaces lack any particular domain knowledge or physics-supported topology (e.g., they do not naturally account for underlying symmetries) [23, 24, 26–30, 39]. Altogether, these limitations add unnecessary complexity into the generative model in order to distinguish between statistically-identical microstructures. Most critically, these approaches only partially solve the problem at hand; while knowledge of property-conditioned microstructures is certainly valuable, it does not provide any processing route for manufacturing such target microstructures of interest. This secondary inversion is usually handled via a domain-knowledge-dependent iterative search [14, 15].

In this work, we leverage several learning methods to efficiently solve the full PSP inverse problem. Specifically, the inverse problem is posed and solved in a Bayesian setting, which naturally accounts for stochasticity in the composite forward model and degeneracy in the inversion. The solution is generated using amortized variational inference [40]. In order to disentangle the microstructure space Ω_2 , we employ a statistical latent representation of microstructure, namely, 2-point spatial correlations [41,42]. Stochastic forward models are then constructed linking this representation to both processing parameters ($\Omega_1 \rightarrow \Omega_2$) and effective properties ($\Omega_2 \rightarrow \Omega_3$). The inverse linkage ($\Omega_1 \leftarrow \Omega_3$) itself is modeled using a conditional continuous normalizing flow, which is trained with its conditioning variable taken as the property output of the chained stochastic forward models. Once trained, this model can sample from the approximate posterior distribution of property-conditioned processing parameters. We conclude by applying the framework to the design of heterogeneous microstructures produced by phase-field simulation [43] and provide statistical analysis of our method's overall performance and reliability.

2 Background

Phase-Field Modeling: Phase-field simulations are commonly applied to model a number of manufacturing processes involving evolving interfaces (such as solidification/melting, spinodal decomposition, grain growth, recrystallization, and crack propagation [44, 45]). In particular, the Cahn-Hilliard equation is frequently used to describe spinodal decomposition, a spontaneous

thermodynamic-instability-induced phase separation [46]; this partial differential equation models a diffusion-driven process with a diffusivity constant \mathcal{D} , driving the evolution of composition variations, c, over characteristic length scales dictated by a gradient energy coefficient, γ . In our problem the spatially-dependent composition will take the role of material microstructure.

$$\frac{\delta c}{\delta t} = \mathcal{D}\nabla^2 \left(c^3 - c - \gamma \nabla^2 c \right) \tag{1}$$

Gaussian Processes: Throughout this work, the forward mappings (PS and SP linkages) are assumed to be stochastic, thus requiring forward uncertainty propagation. We approach this task through the use of Gaussian processes (\mathcal{GPs}) , an expressive and flexible construct, defining a distribution over a family of functions by describing their functional output covariance across the input domain. This covariance necessarily dictates the resulting function characteristics, and is constructed with a kernel function $k(\cdot, \cdot')$. Provided observations $\{\boldsymbol{x}_n, \boldsymbol{y}_n\}_{n=1}^N$ from an underlying generating process, a conditioned distribution over the space of functions $\{\boldsymbol{x} \to \boldsymbol{y}\}$ can be established, estimating the trend and the uncertainty of the data. For a more in depth discussion we defer to [47,48].

2-Point Spatial Correlations: This work uses 2-point spatial correlations [13, 14, 41] to construct descriptive microstructure features. This representation builds on the idea that the microstructure itself is a stochastic function, where individual observed microstructure instances are samples from the governing stochastic microstructure function [41,42]. This theoretical treatment accounts for the inherent stochasticity displayed by material microstructures, and allows for the underlying stochastic function to be linked to homogenized properties. It also provides a convenient mechanism to account for underlying symmetries (such as translation-equivarinace and periodicity).

In practice, 2-point spatial correlations can be computed as a convolution of the sampled discrete microstructure function m_s^{α} , where α is the material local state at voxel s. The resulting 2-point spatial correlations are then defined by the operation

$$f_r^{\alpha\beta} = \frac{1}{S} \sum_{s=1}^S m_s^{\alpha} m_{s+r}^{\beta} \tag{2}$$

where S defines the set of all voxels in the microstructural domain. These represent lower-order terms in a moment expansion of the true microstructure random process; for a number of materials systems, this term is dominant and captures most of the variation in bulk material properties. Dimensionality reduction techniques can then be effectively applied to the ensemble of 2-point spatial correlations to provide robust, information-dense features for the construction of PS and SP linkages [16, 49–55].

Conditional Flow Matching: Continuous normalizing flows (CNFs) [37] are an expressive and efficient method for density estimation which construct an invertible mapping between the standard normal distribution and a given data distribution. The mapping itself is specified via the dynamics of a neural ordinary differential equation (ODE) [37]. While these methods have historically exhibited difficulties during training [56, 57], *Conditional Flow Matching* (CFM) [38] has emerged as a powerful *simulation-free* technique for stabilizing the training of CNFs. This objective enables training of the CNF without requiring internal calls to an ODE solver during the training phase, instead matching the vector field of the conditional transport map.

3 Framework

In this section we propose a Bayesian Inversion [58] framework for solving the process-property stochastic inverse problem. Figure 1 visually summarizes the overarching strategy. To begin, we define notation specific to this particular problem. Inputs of the forward model are denote by the vector of processing parameters $\boldsymbol{\theta} \in \mathbb{R}^{D}$, the target effective property vector is denoted by $\boldsymbol{k} \in \mathbb{R}^{P}$,



Figure 1. Visual representation of proposed framework. The prior distribution in the first two dimensions is invertibly transformed to the uniform distribution, which can then be sampled to produce unique microstructure instantiations. This prior over processing parameters results in an equivalent prior in microstructure space when phase-field simulations are performed. This latent microstructure prior, alongside processing through quantification with 2-point spatial correlations and PCA embedding is also shown. The likelihood is then defined as a composition of probabilistic PS and SP linkages, which is subsequently used to perform amortized stochastic variational inference (SVI). Lastly, the image of posterior samples under the (true) PS forward model is displayed, demonstrating microstructure specificity to match target properties. $\tilde{\mathcal{H}}$ denotes the composite surrogate forward model, k the property set of interest, α the statistical low-dimensional PC representation of microstructure, and m microstructure.

and intermediate (2D, in this work) microstructures are written $m \in \mathbb{R}^{L \times L}$. Given an initial dataset of processing parameter, microstructure, and property triples, $\{\boldsymbol{\theta}_n, m_n, \boldsymbol{k}_n\}_{n=1}^N$, we create tractable estimations for the components of Bayes' theorem necessary for computing the desired posterior (e.g., $p(\boldsymbol{\theta}), p(\boldsymbol{k}|\boldsymbol{\theta}))^1$.

We note that a naïve approach to identifying the mappings $\mathcal{G} : \theta \to m$ and $\mathcal{F} : m \to k$ would necessarily traverse the high-dimensional stochastic microstructure space. This challenge would only be amplified during the inversion. We address these issues directly by quantifying microstructures through 2-point spatial correlations, and then embedding them into a lowerdimensional manifold through Principal Component Analysis (PCA) [53, 59–61], retaining Rprincipal components (PC) scores (denoted α) as descriptors. Importantly, this physics-informed R-dimensional representation has effectively demonstrated a robust ability of stratifying associated properties in the first handful of terms [49–55], enabling us to move through a R-dimensional microstructure space as higher-order terms result in minimal shifts in resulting properties. This distillation of global microstructure information greatly simplifies the overarching inversion, as identifying a distribution over the exceedingly high-dimensional microstructure space is wholly unnecessary. Rather, we can traverse this compact representation of the microstructure random process. Briefly, we note that this approach could potentially break down when the target properties are the result of localized processes, such as fracture and fatigue resistance [62–65].

In summary, the proposed modular framework utilizes surrogate forward models $\tilde{\mathcal{G}}$ and $\tilde{\mathcal{F}}$ to train a flow-based generative model to estimate the posterior mapping between desired properties and processing parameters. This cooperative reformulation avoids the problem of inverting this mapping directly from just data using solely a flow-based generative model, and instead provides a platform for which to construct smaller forward models as a continuous source of training data for the CNF.

4 Experiments & Discussion

In order to validate the proposed framework, we apply it to two different materials systems undergoing spinodal decomposition, with in depth analysis performed for two distinct test cases per system, and subsequently, a more general validation procedure applied to the entire property space. These two cases consist of (processing parameters, property) pairs denoted as $\{\theta^*, k^*\}$,

¹A reference summary of notation used throughout this work is presented in Appendix D.

	Al-Si			High-Contrast		
	E (GPa)	ν	κ (W/mK)	E (GPa)	ν	κ (W/mK)
Constituent 0	70	0.33	247	1	0.3	100
Constituent I	169	0.28	400	100	0.3	1

Table 1. Summary of constituent property assignment for low- and high-contrast ratio cases, displaying the isotropic elastic modulus (E), Poisson's ratio (ν) , and thermal conductivity (κ) of the constituents considered.

which we selected from a dataset of spinodal decomposition phase-field simulations. The phase-field simulations take a 3-dimensional processing parameter input θ , dictating disparate heterogeneous microstructure evolution pathways. The property set k considered includes both effective anisotropic elastic moduli and thermal conductivity.

The two materials systems considered were chosen to evaluate model performance with varying contrast between phases, as well as its ability to balance competing property targets. The low-contrast case corresponds to the Al-Si alloy material system, which is physically realizable. Conversely, the high-contrast case is a fictitious 2-element alloy in which the elastic and thermal properties trade off (and vary heavily) between phases. It is important to consider multiple contrast ratios because it has been well documented that PSP linkages become harder to construct with higher contrast ratios [66]. A summary of the constituent material parameters can be found in Table 1. These stress tests were selected to best scrutinize the proposed approach across sparse regions of the dataset and increasingly-complex material responses.

The dataset contains 10,000 two-phase microstructures of size 256×256 voxels, each associated with processing parameters θ_1 and θ_2 , sampled according to the log-uniform $\log(\theta) \sim \mathcal{U}(\log(0.1), \log(100))$, and $\theta_3 \sim \mathcal{U}(-0.7, 0.7)$. These processing parameters correspond to the mobility parameters of the two constituents (θ_1, θ_2) , and initial relative concentrations (θ_3) . Homogenized properties were extracted for each microstructure in the dataset through performing finite element simulations with Abaqus/Standard [67]. Figure 2a visually summarizes the resulting property set for these microstructures with Al-Si constituent property assignment and Figure 2b with the high-contrast assignment. Figure 2c displays the microstructure ensemble in the first 4 PC dimensions. The selected test cases are highlighted in each projection as p_1 and p_2 .

Figure 2c illustrates projections of the microstructure ensemble in the first 4 PCs. Each microstructure is statistically represented by a subset of its 2-point spatial correlations: we computed $\{f_r^{00}, f_r^{01}\}$ using Eq. (2), with the material local state indexed by $\{0, 1\}$. While this set of spatial correlations provides a robust statistical description of internal microstructure arrangement, it also doubles the dimensionality relative to the initial microstructure. As such, Principal Component Analysis (PCA) was performed to reduce the dataset's dimensionality, using a concatenated flattened representation of $\{f_r^{00}, f_r^{01}\}$. Scaling factors were applied to the set as $\{f_r^{00}, 26.389f_r^{01}\}$ to balance contributions between auto- and cross-correlations so that neither set dominated the transformation. Overall, Figure 2 highlights the motivation for selecting these particular test cases, with each selected to balance coverage of the property space while simultaneously identifying sparse regions in PC space.

4.1 Al-Si Alloy

After training, samples from the approximate posterior $p(\theta|k^*)$ were drawn from the CNF model for both of the test cases, displayed in Figure 3. The marginal distributions in the log-space of the processing parameters can be seen in Figure 3, where the processing parameter set θ^* associated with the conditioning property set k^* is demarcated with a vertical line. Inspection of the posteriors highlights that in the first case study, larger deviations in θ_1 and θ_2 can be tolerated, but extreme specificity is required in θ_3 , which, notably, was found to be very near to zero. This observation aligns with the fundamental dynamics of the Cahn-Hilliard phase-field model. When the order parameter θ_3 is near zero, signifying an almost equal fraction of both phases in the initial mixture, the system experiences a heightened driving force for phase separation rendering it less sensitive to mobility parameter discrepancies in the early stages of the microstructure evolution. As a result,



Figure 2. Experimental dataset considered in this work with select microstructures identified as test cases. (a) Property set of the low-contrast Al-Si microstructure ensemble, (b) property set of the high-contrast microstructure ensemble, and (c) low-dimensional microstructure representation in the first 4 PC dimensions.



Figure 3. Marginal posterior distributions for the two test cases p_1 and p_2 with the low-contrast constituent property assignment. The first two dimensions of θ are displayed in the log-space. Associated processing parameter sets θ^* to the target property set k^* are displayed as a black dashed line.

even significant variations in the mobility parameters, θ_1 and θ_2 , have a diminished impact on the microstructure evolution. In contrast, the second case study posterior demonstrates significantly more sharpening across the processing parameter domain, indicating that in sparser regions of the microstructure and property spaces, a greater degree of specificity across all processing parameters is necessary to meet the target property set. In each of the marginal posterior plots, the framework was able to recover the latent θ^* associated with the target property set.

Next, we interrogate how well the posterior predictions match the desired target property set. To address this we draw 200 valid samples from the posterior $p(\theta|k^*)$), and apply both the surrogate



Figure 4. Marginal distributions of $\mathcal{H}(p(\boldsymbol{\theta}|\boldsymbol{k}^*))$ (ground truth forward model) for the two lowcontrast test cases p_1 and p_2 shown alongside the validation set of 200 processing parameters sampled from the posteriors. The validation set was evaluated through phase-field and finite element simulations.

and "ground truth" composite forward models ($\hat{\mathcal{H}}, \mathcal{H}$ respectively) on each sample. Posterior samples outside of the validity bounds of the phase-field model were rejected. The results of this can be seen in Figure 4, where the property target falls well within the predicted distribution (for both models). Additionally, the distributions of resultant properties match relatively well between surrogate and true forward models.

4.2 High-Contrast Alloy

The low-contrast Al-Si test cases demonstrated that the framework is capable of adequately identifying the processing parameter sets necessary to meet various target property sets. Due to the higher contrast of the microstructures' constituent properties and increasing nonlinearity of their responses in this case study, we expect less variability in the distributions over processing parameters and latent microstructure statistics. Such intuition is reflected in the resulting posteriors $p(\theta|k^*)$, displayed in Figure 5. p_1 demonstrates a departure from the low-contrast log-uniform, with a preference towards lower mobility values (θ_1 and θ_2), while the posterior p_2 remained roughly equivalent to the prior case study due to its extremal location in the dataset.



Figure 5. Marginal posterior distributions for the two test cases p_1 and p_2 with the high-contrast constituent property assignment. The first two dimensions of θ are displayed in the log-space. Associated processing parameter sets θ^* to the target property set k^* are displayed as a black dashed line.



Figure 6. Marginal distributions of $\mathcal{H}(p(\boldsymbol{\theta}|\boldsymbol{k}^*))$ for the two high-contrast test cases p_1 and p_2 shown alongside the validation set of 200 processing parameters sampled from the posteriors. The validation set was evaluated through phase-field and finite element simulations.

In a similar fashion to the prior case study, we turn towards inspecting the resulting property set predictions of the processing parameter posterior. We apply the same methodology used for Figure 4 for the high-contrast case and present the results in Figure 6. Again, the target property vector is recovered by both the surrogate and exact forward models. Interestingly, the surrogate model over-estimates the variance in predictions k_1 and k_2 compared to the true model. We believe this is caused by a degradation in performance of the SP linkage $\tilde{\mathcal{F}}$ for thermal conductivities near the homogeneous microstructure lower-property limit, as seen in Appendix A. Importantly, even with this degradation in forward property prediction, the framework is capable of identifying promising processing parameter sets in validation.

4.3 Validation Across Property Space

While utilizing these two selected test cases provided the opportunity for validation through the exact forward process, it is limited by the computational cost of evaluating this process. Consequently, the limitation to certain target property sets precludes a complete understanding of the frameworks performance across the entire property space. In order to further explore framework performance, we now turn towards identifying posterior solutions for every property set in the available dataset. In this validation, we restrict our consideration to property values in the hold-out testing dataset from training the forward models. 128 samples are drawn from $p(\theta|k^*)$ for every property value in the dataset, and then each passed through the learned sparse variational multi-output Gaussian process forward models $\mathcal{H}(p(\boldsymbol{\theta}|\boldsymbol{k}^*))$, such that for each target property set there now exists a distribution of forward propagated samples from the corresponding solution posterior. This is practically useful as it provides a method for directly and rapidly comparing the capabilities of the framework, while providing a methodology for inspecting uncertainty in the identified solutions. Figure 7 displays the results of this evaluation for both the low- and high-contrast applications where Figure 7(a) and Figure 7(b) show parity plots colored by the estimated density, highlighting the accurate predictions across the majority of the property space, particularly in the most dense regions. The shape of the estimated cumulative distribution functions for each are overlaid in Figure 7(c) only reinforcing this point. Degraded performance can be observed as we move towards lower-density regions of the property space. Quite naturally, we also correctly observe an increase in uncertainty in such extremal property sets - an early indication uncertainty in the framework is well calibrated.

4.4 Calibration

While the previous case studies indicate that our model captures the correct overall trends, the question remains of how well the uncertainty in the estimated distribution matches that of the true distribution; that is: is our model well-calibrated? The validity of the identified joint distributions $p(\theta, k) = p(k|\theta)p(\theta)$ is explored through recent work by Säilynoja *et al.* [68]. This simulation-based method evaluates the quality of a Bayesian analysis across the entire joint $p(\theta, k)$, sampling



Figure 7. Forward mapping of inverse solutions for all property sets in the available dataset. (a) Parity plot of all target property sets against 128 points propagated from the posterior solution, (b) estimated density of the parity plot, (c) estimated cumulative distribution of Normalized Mean Absolute Error (NMAE) over all propagated property sets with the 95th percentile highlighted.



Figure 8. Empirical cumulative distribution functions to asses uniformity of the samples for both low- and high-contrast cases.

a ground truth from the prior $\hat{\theta} \sim p(\theta)$ and data from the likelihood $\hat{k} \sim p(k|\theta)$. Evaluations with these simulated pairs can then be used in evaluating the discrepancy between the data averaged posterior and the prior through the following expression.

$$p(\boldsymbol{\theta}) = \int p(\boldsymbol{\theta}|\tilde{\boldsymbol{k}}) p(\tilde{\boldsymbol{k}}|\tilde{\boldsymbol{\theta}}) p(\tilde{\boldsymbol{\theta}}) d\tilde{\boldsymbol{\theta}} d\tilde{\boldsymbol{k}}.$$
(3)

The empirical cumulative distribution function (ECDF) graphical test for uniformity involves the probability integral transform in comparing the data averaged posterior to the prior, providing an intuitive methodology for evaluating the quality of a Bayesian analysis. A linear result is desirable. The results of this procedure for both joints from the low- and high-contrast cases can be seen in Figure 8, as well as 95% confidence intervals (based on a binomial distribution). Briefly, this figure indicates that the model is well-calibrated in the low-contrast case, with discrepancies in the fractional rank statistic for θ_3 in the high-contrast posterior.

5 Conclusions

We present a framework for addressing inverse stochastic materials design problems. The framework provides a tool set for the designer to identify *novel* structures and identify distributions of processing routes to *realize* such structures. We exhibit demonstrations of its utility on increasing challenging test cases, and demonstrate that it provides well calibrated posterior predictions of processing parameters. Due to its stochastic nature, this framework also provides a mechanism for Bayesian model calibration, selection, and uncertainty quantification.

6 Author Contributions

AG conceived the project and designed the models with assistance from CK, AR, and MB. GH generated the spinodal decomposition data, and AG the finite-element results. SK ensured funding support. AG wrote the initial manuscript, CK revised, and all authors edited the final version.

7 Acknowledgments

This research acknowledges funding by various sources. Adam P. Generale: Pratt & Whitney; Conlain Kelly: NSF 2027105, NSF Graduate Research Fellowship DGE-1650044, and ONR N00014-18-1-2879; Grayson Harrington: NSF Graduate Research Fellowship DGE-2039655 and Sandia LDRD Contract Agreement #2177713; Andreas E. Robertson: ONR N00014-18-1-2879; M. Buzzy: NSF DMREF-2119640. Surya R. Kalidindi acknowledges funding from all previously listed funding sources. This work utilized computing resources and services provided by the Partnership for an Advanced Computing Environment (PACE) and the Hive computing cluster at the Georgia Institute of Technology, Atlanta, Georgia, USA. A.E. Robertson also acknowledges the continuing support of the Jack Kent Cooke Foundation, and A.P. Generale that of the Alfred P. Sloan Foundation. Finally, the authors wish to thank Rafael Orozco for invaluable conversations, particularly regarding model calibration.



Figure A.1. Parity plot of SV-MOGP forward models performance on the available microstructure ensemble. Predicted $\pm 2.0\sigma$ confidence intervals are displayed alongside mean predictions. (a) PS linkage for first 5 PC scores, (b) SP linkage for Al-Si case, and (c) SP linkage for high-contrast ratio case.

A Appendix: Forward Models

Process-structure (PS) and structure-property (SP) linkages for the Al-Si case were constructed with a sparse variational multi-output Gaussian process (SV-MOGP) [69, 70], where the multi-output covariance matrix was constructed with the Linear Model of Coregionalization (LMC) [71, 72] and a spectral mixture kernel [73]. The intermediate microstructure representation consisted of 5 PC scores due to signal decay and limitations of the PS linkage to accurately predict past this point. The PS linkage was constructed with 800 inducing points, 5 latent processes, and 6 mixtures in the SM kernel, while the SP linkage was defined through 160 inducing points, 5 latent processes, and 6 mixtures in the SM kernel. Each model was trained with 32 bit-precision for 4,000 epochs with a minibatch size of 1024. Optimization of model parameters was performed with the Adam optimizer and cosine annealing from an initial learning rate of 1e-2, ending at 1e-8.

Due to the increasingly complex material response in the high-contrast case, we found improved performance for the SP linkage through the creation of a deep Gaussian process [74,75]. The model consists of 3 layers, each constructed with a Matérn 5/2 kernel and 400 inducing points. Similarly, the model was trained with the Adam optimizer and the same floating point precision, learning rate schedule, and minibatch size for 2,000 epochs.

The available experimental dataset was partitioned into a 80/20 train/test split. Parity plots of each model's performance can be seen in Figure A.1, with corresponding error metrics in Table A.1. The additional challenge of learning the complex nonlinear mapping between structure and property in the high-contrast ratio case is clearly evident.

B Appendix: CNF Architecture

The architecture underpinning the CNF in both the low- and high-contrast cases was identified as the result of an ablation study across 6 various architectures. Relatively simple architectures were considered in this work, although we have no doubt that further refinement may be possible. Due to the low-dimensional microstructure space considered, the architectures considered are significantly more light-weight than similar models considered in other works [23, 24, 26–29], albeit no other models exist which enable inversion of the complete PSP linkage. The networks and training settings considered are displayed in Figure B.1. All models were trained with the Adam optimizer [76] and 32 bit-precision. Specifics regarding the architecture selected can be found in Table B.1. Training

		α_1	α_2	α_3	α_4	α_5
MAE	Train Test	$3.396 {\pm} 8.458 \\ 4.055 {\pm} 12.113$	$\substack{0.377 \pm 0.515 \\ 0.411 \pm 0.661}$	$3.376 {\pm} 4.401$ $3.573 {\pm} 4.636$	$\substack{4.133 \pm 5.727 \\ 4.302 \pm 6.211}$	$4.348{\pm}6.119$ $4.826{\pm}7.087$
NMAE (%)	Train Test	$\substack{1.746 \pm 4.350 \\ 2.086 \pm 5.809}$	$0.853 {\pm} 1.164$ $0.929 {\pm} 1.164$	8.879±11.577 9.400±11.577	$\substack{18.230 \pm 25.258 \\ 18.975 \pm 27.394}$	$\substack{31.317 \pm 44.078 \\ 36.447 \pm 51.054}$
		E_1 (GPa)	E_2 (GPa)	G_{12} (GPa)	k_1 (W/mK)	$k_2 (W/mK)$
MAE	Train Test	$\substack{0.267 \pm 0.341 \\ 0.272 \pm 0.345}$	$\substack{0.272 \pm 0.355 \\ 0.262 \pm 0.336}$	$\substack{0.094 \pm 0.103 \\ 0.094 \pm 0.101}$	$\substack{0.233 \pm 0.310 \\ 0.231 \pm 0.299}$	$\substack{0.234 \pm 0.100 \\ 0.232 \pm 0.304}$
NMAE (%)	Train Test	$\substack{0.247 \pm 0.315 \\ 0.252 \pm 0.319}$	$\substack{0.252 \pm 0.328 \\ 0.242 \pm 0.311}$	$\substack{0.228 \pm 0.249 \\ 0.227 \pm 0.246}$	$\begin{array}{c} 0.074{\pm}0.098\\ 0.073{\pm}0.095\end{array}$	$\substack{0.074 \pm 0.100 \\ 0.073 \pm 0.096}$
MAE	Train Test	$\substack{0.579 \pm 0.957 \\ 0.744 \pm 1.381}$	$\begin{array}{c} 0.566{\pm}0.915\\ 0.777{\pm}1.481\end{array}$	$\substack{0.198 \pm 0.298 \\ 0.264 \pm 0.464}$	$\begin{array}{c} 0.578 {\pm} 1.099 \\ 0.896 {\pm} 2.279 \end{array}$	0.611±1.217 0.838±2.071
NMAE (%)	Train Test	2.990 ± 4.945 3.844 ± 7.134	2.923±4.726 4.010±7.646	2.760 ± 4.159 3.677 ± 6.475	2.241±4.423 3.477±8.844	2.348±4.713 3.246±8.023

Table A.1. Summary error metrics (Mean Absolute Error (MAE) and Normalized Mean Absolute Error (NMAE)) of SV-MOGP forward model performance with reported mean and standard deviation.

Table B.1. Summary of CNF model architectures considered.

Hyperparameter	Arch. 1	Arch. 2	Arch. 3	Arch. 4	Arch. 5	Arch. 6
Depth	3	4	6	3	4	6
Width	128	128	128	256	256	256

was performed for 1000 epochs with a batch size of 1024 (9766 iterations), cosine annealing of the learning rate from 1e - 3 to 1e - 8, an EMA decay rate of 0.9999, and $\sigma_{\min} = 1e - 3$. All probability flow paths were solved for at t = 1 with the adaptive step size dopris solver and tolerances atol = rtol = 1e - 5.

Model performance was evaluated for the low-contrast dataset for the purposes of architecture selection. Posteriors were sampled for each conditioning property set available in the dataset, and the NMAE evaluated across all samples. The threshold for the 95th percentile was also evaluated, with the results of both across the architectures considered presented in Figure C.3. This process is identical to the process laid out in constructing Figure 7. Architecture #5 was selected for all case studies presented in this work, as it was the most light-weight architecture displaying minimal values for the error metrics tracked in Table B.2 and Figure C.3.



Figure B.1. Results of ablation study. (a) NMAE determined through the propagation of 128 posterior samples, conditioned across all available property sets. Propagated posterior means are evaluated directly against the condioning property set. (b) Normalized 95th percentile of properties, as determined through the estimated CDF from all propagated posterior samples.

		Arch. 1	Arch. 2	Arch. 3	Arch. 4	Arch. 5	Arch. 6
E_1 (GPa)	MAE NMAE (%) 95 th Norm. 95 th	$\begin{array}{c} 0.937 {\pm} 0.969 \\ 0.864 {\pm} 0.778 \\ 2.959 \\ 2.738 \end{array}$	$\begin{array}{c} 0.822 {\pm} 0.742 \\ 0.768 {\pm} 0.616 \\ 2.751 \\ 2.546 \end{array}$	$\begin{array}{c} 0.850 {\pm} 0.843 \\ 0.783 {\pm} 0.654 \\ 2.749 \\ 2.544 \end{array}$	$\begin{array}{c} 0.896 {\pm} 0.939 \\ 0.814 {\pm} 0.695 \\ 2.887 \\ 2.672 \end{array}$	$\begin{array}{c} 0.782{\pm}0.813\\ 0.723{\pm}0.633\\ 2.144\\ 1.984\end{array}$	$\begin{array}{c} 0.724 {\pm} 0.740 \\ 0.668 {\pm} 0.564 \\ 2.150 \\ 1.990 \end{array}$
E_2 (GPa)	MAE NMAE (%) 95 th Norm. 95 th	$\begin{array}{c} 0.917{\pm}0.958\\ 0.846{\pm}0.770\\ 2.860\\ 2.647\end{array}$	$\begin{array}{c} 0.810 {\pm} 0.734 \\ 0.757 {\pm} 0.609 \\ 2.616 \\ 2.422 \end{array}$	$\begin{array}{c} 0.777 {\pm} 0.832 \\ 0.718 {\pm} 0.647 \\ 2.009 \\ 1.859 \end{array}$	0.929±0.929 0.846±0.691 2.754 2.549	$\begin{array}{c} 0.809 {\pm} 0.802 \\ 0.751 {\pm} 0.627 \\ 2.103 \\ 1.946 \end{array}$	$\begin{array}{c} 0.718 {\pm} 0.731 \\ 0.666 {\pm} 0.559 \\ 2.047 \\ 1.895 \end{array}$
G ₁₂ (GPa)	MAE NMAE (%) 95 th Norm. 95 th	$\begin{array}{c} 0.345{\pm}367\\ 0.826{\pm}0.768\\ 0.963\\ 2.337\end{array}$	$\begin{array}{c} 0.273 {\pm} 0.288 \\ 0.665 {\pm} 0.621 \\ 0.683 \\ 1.658 \end{array}$	$\begin{array}{c} 0.319{\pm}0.330\\ 0.762{\pm}0.660\\ 0.904\\ 2.193\end{array}$	0.332±0.359 0.792±0.693 0.970 2.353	$\begin{array}{c} 0.279 {\pm} 0.310 \\ 0.674 {\pm} 0.632 \\ 0.743 \\ 1.803 \end{array}$	$\begin{array}{c} 0.265 {\pm} 0.285 \\ 0.639 {\pm} 0.565 \\ 0.711 \\ 1.726 \end{array}$
<i>k</i> ₁ (W/mK)	MAE NMAE (%) 95 th Norm. 95 th	$\begin{array}{c} 1.269{\pm}1.204\\ 0.404{\pm}0.388\\ 3.122\\ 0.988\end{array}$	$\begin{array}{c} 1.036 {\pm} 0.987 \\ 0.332 {\pm} 0.329 \\ 2.685 \\ 0.850 \end{array}$	$\begin{array}{c} 1.134{\pm}1.114\\ 0.359{\pm}0.347\\ 3.326\\ 1.053\end{array}$	$\begin{array}{c} 1.201 \pm 1.149 \\ 0.380 \pm 0.352 \\ 3.514 \\ 1.112 \end{array}$	$\begin{array}{c} 1.007 {\pm} 0.997 \\ 0.321 {\pm} 0.324 \\ 2.543 \\ 0.905 \end{array}$	$\begin{array}{c} 0.920{\pm}0.908\\ 0.292{\pm}0.290\\ 2.732\\ 0.864\end{array}$
k ₂ (W/mK)	MAE NMAE (%) 95 th Norm. 95 th	1.244±1.206 0.396±0.389 3.121 0.988	$\begin{array}{c} 1.106 {\pm} 0.988 \\ 0.326 {\pm} 0.329 \\ 2.746 \\ 0.869 \end{array}$	$\begin{array}{c} 1.048 {\pm} 1.108 \\ 0.332 {\pm} 0.345 \\ 2.695 \\ 0.853 \end{array}$	$\begin{array}{c} 1.241 {\pm} 1.151 \\ 0.393 {\pm} 0.353 \\ 3.558 \\ 1.126 \end{array}$	$\begin{array}{c} 1.042{\pm}0.997\\ 0.333{\pm}0.324\\ 3.136\\ 0.992\end{array}$	$\begin{array}{c} 0.914{\pm}0.907\\ 0.291{\pm}0.290\\ 2.766\\ 0.875\end{array}$

Table B.2. Model architectures and mean error metrics considered across the property space.

C Appendix: Resulting Microstructures



Figure C.1. Heterogeneous microstructures drawn at random from the available dataset.



Figure C.2. Heterogeneous microstructures identified through transforming 25 posterior samples through the phase-field model forward process, $p(m|k^*)$. (a) Al-Si low-contrast ratio microstructures for the first test case, and (b) the second test case.



Figure C.3. Heterogeneous microstructures identified through transforming 25 posterior samples through the phase-field model forward process, $p(m|k^*)$. (a) High-contrast ratio microstructures for the first test case, and (b) the second test case.

D Appendix: Notation

	Tuble D.1. Deminions of common variables used in this work
Variable	Definition
Ω_1	Process Space
Ω_2	Structure Space
Ω_3	Property Space
${\cal F}$	Process-Structure forward mapping (tilde denotes surrogate model)
${\mathcal G}$	Structure-Property forward mapping (tilde denotes surrogate model)
${\cal H}$	Process-Property forward mapping (tilde denotes surrogate model)
m_s^{α}	Discrete microstructure function for state α in voxel s
$f_r^{lphaeta}$	2-point spatial correlations between phases α and β with offset r
θ	Vector of processing parameters
$ heta_1, heta_2$	First two processing parameters for spinodal decomposition (mobilities for each phase)
$ heta_3$	Third processing parameter for spinodal decomposition (initial relative concentration)
$m{k}$	Vector of material properties
E	Young's Modulus
u	Poisson Ratio
κ	Thermal conductivity
$p_n(\boldsymbol{\theta} \boldsymbol{k}^*)$	Posterior distribution of process parameters given a vector of target properties k^*

Table D.1. Definitions of common variables used in this work

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